

Vortex Simulation of Two Cylinders in Tandem Using Overlapping Grid System

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Title page

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ORIGINAL ARTICLE

Vortex Simulation of Two Cylinders in Tandem Using Overlapping Grid System**Wisnu Wardhana¹, Ede M. Wardhana², Meitha Soetardjo³**

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Abstract: To give a considerable time reduction in the calculation of the vortex velocity and in the CPU time, discrete vortex modelling of flows using overlapping grid system for two tandem cylinders is carried out. This simple and time efficient method gives a better scatter of surface vorticity as the vortices around the body are now calculated on grid point. This research is to simulate the loading on structural elements of the structures due to their interaction with anodes or with other members. To show the flow phenomena and interactions involved, the in-line and transverse force coefficients are presented. The comparison of the results with experimental and numerical results and the range for good results is presented.

Keywords: flow simulation • discrete vortex • cylinder • tandem • overlapping grid

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1 Introduction

There are two unusual features of flow in the experiment for two cylinders in tandem with various different gap ratios carried out by [1] that, firstly, the side facing the gap between the cylinders had a very low negative pressure which was almost the same as the corresponding value of the base pressure of the upstream cylinder. This fact is an indication that the flow around the gap is almost stagnant. Secondly, the negative gap pressure in front of the downstream cylinder exceeded that on its downstream face. This means that when the distance is less than a critical gap, the downstream cylinder experiences a negative drag-thrust

force. The vortex reduction scheme is used to simulate the turbulent dissipation in the wake downstream.

2 Basic Formulation

The complex potential $w(z)$ can be formulated where N_b is the number of cylinder, γ_e^b is the strength of vortices at element e of body b , dS_e^b is the length of element e of body b , z_e^b is the position of element e of body b , Γ_e^b is the strength of a vortex v shed by cylinder b , z_v^b is the position of a vortex v shed by cylinder b , as follows,

$$w(z) = u_\infty e^{i\alpha_\infty z} + \frac{i}{2\pi} \sum_{b=1}^{N_b} \sum_{e=1}^{N_e^b} \gamma_e^b dS_e^b \ln(z - z_e^b) + \frac{i}{2\pi} \sum_{b=1}^{N_b} \sum_{v=1}^{N_v^b} \Gamma_v^b \ln(z - z_v^b) \quad (1)$$

In this study an overlapping grid system which has ‘square’ elements is used for individual cylinder to give good pattern of the flow close to the cylinder surface.

The grid node on the cylinder surface provides the control points at which equation (2) above is solved to zero tangential velocity to satisfy Dirichlet boundary condition [10].

The solution procedure for the induced velocity at an element S_n must include the influence of those two cylinders in the fluid domain.

$$-\frac{1}{2} \gamma_m + \oint_{cN_b} k_{mn} \gamma_n dS_n + \vec{u}_\infty \cdot \vec{d}S_m + \sum_{b=1}^{N_b} \sum_{v=1}^{N_v} l_{mv} \Gamma_v^b = 0 \quad (2)$$

3 Methodology

Equation (2) must satisfy the Dirichlet boundary condition as follow,

$$\begin{aligned} & -\frac{\gamma_m^p}{2} + \sum_{q=1}^{N_b} \sum_{n=1}^{N_n^q} \frac{\Delta S_n^q}{2\pi} \Re \left(\frac{i \gamma_n^q e^{i \beta_m^p}}{z_m^p - z_n^q} \right) + \Re \left(u_\infty e^{-i(\alpha_\infty - \beta_m^p)} \right) + \\ & \sum_{q=1}^{N_b} \sum_{v=1}^{N_v} \frac{\Gamma_v^q}{2\pi} \Re \left(\frac{i e^{i \beta_m^p}}{z_m^p - z_v^q} \right) = 0 \end{aligned} \quad (3)$$

The equation can be written as follows

$$\sum_{q=1}^{N_b} \sum_{n=1}^{N_e^q} K_{mn}^{pq} + \Re \left(u_\infty e^{-i(\alpha_\infty - \beta_m^p)} \right) + \sum_{q=1}^{N_b} \sum_{v=1}^{N_v} \frac{\Gamma_v^q}{2\pi} \Re \left(\frac{ie^{i\beta_m^p}}{z_m^p - z_v^q} \right) = 0 \quad (4)$$

In matrix form it can be written as

$$\begin{pmatrix} k_{mn}^{11} & k_{mn}^{12} \\ k_{mn}^{21} & k_{mn}^{22} \end{pmatrix} = \begin{pmatrix} RHS^1 \\ RHS^2 \end{pmatrix} \quad (5)$$

The RHS means the right-hand side of equation (6). The procedure can be seen as in the flowchart Fig. 1 below.

The new locations of the vortices can be calculated as follows

$$z_v^{(t+\Delta t)} = z_{v(t)} + \delta z_v^{rw} + \delta t u_v^{(t)}(z_v) \quad (6)$$

where: $z_{v(t)}$ is the initial position and the other is the shift of vortices

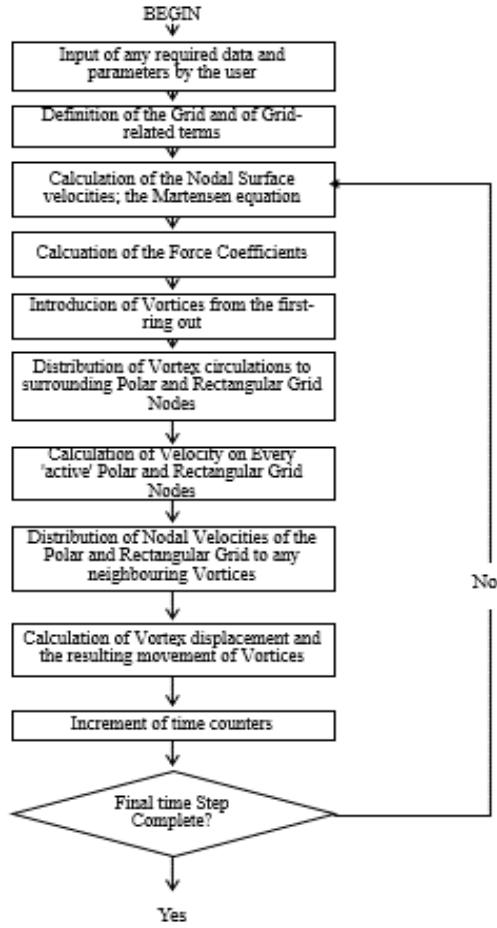


Figure 1 Flowchart of the Algorithm

The new position of each vortex is referenced to both polar and rectangular grid systems. Each vortex has two base nodes from which its relative position at every time step is measured and renewed.

A numerical expression for the change in surface pressure over the element n during the discrete time step Δt can then be obtained as

$$\Delta p_n = -\rho \frac{\gamma_n \Delta S_n}{\Delta t} = -\rho \frac{\Gamma_n}{\Delta t} \quad (7)$$

The difference of pressure Δp_n is measured from the stagnation pressure $p_s = \frac{1}{2} \rho u_\infty^2$ at the stagnation point S_s . Hence, the pressure at element m will be

$$p_n = p_s - \frac{\rho}{\Delta t} \sum_{n=1}^m \Gamma_n \quad (8)$$

The other force that contributes to drag and lift forces is the one due to the skin friction (viscous drag) on the surface of the cylinder, as follow

$$\tau_n = \mu \omega_n = \mu \frac{\gamma_n d S_n}{d A_n} \quad (9)$$

where μ is the dynamic viscosity. The form drag, lift and skin friction coefficients can be calculated as follows,

$$C_D = \frac{D}{\frac{1}{2} \rho u_\infty^2 d} = \frac{2}{\rho u_\infty^2 d} \sum_{n=1}^m (\bar{p}_n \sin \beta_n \Delta S_n + \bar{t}_n \cos \beta_n \Delta S_n) \quad (10)$$

$$C_L = \frac{L}{\frac{1}{2} \rho u_\infty^2 d} = -\frac{2}{\rho u_\infty^2 d} \sum_{n=1}^m (\bar{p}_n \cos \beta_n \Delta S_n - \bar{t}_n \sin \beta_n \Delta S_n) \quad (11)$$

where d is the diameter of the cylinder and β the tangent angle of the element. The basic procedure is based on the integration of the elemental pressure around a cylinder. The pressure around the cylinder can then be integrated numerically to get the value of the force coefficients.

Methods of enhancement as used in [10] also applied in this research such as Correction for close proximity, Vorticity Reduction Scheme and the Curvature Corrections.

4 RESULTS

The results of the numerical experiments for G/D ratio of 0.5, 1, 1.5 and 2 for $Re = 100000$ are presented in Fig. 9, 10, 11 and 12 below.

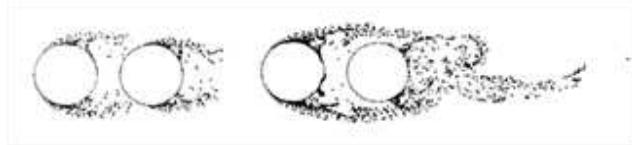


Figure 2 The Flow Pattern at $G/D=1.5$, $t=1$ and 5

It is seen from Fig. 2 above that for $G/D = 1.5$ at $t = 1$ and 5, the two cylinders shed the vortices almost identically even though no asymmetric enforcement was imposed. The flow pattern at higher t can be seen in Fig. 3 below



Figure 3 The Flow Pattern at $G/D = 1.5$

which shows that the random diffusion and also the accumulation of numerical errors was found to be sufficient to trigger asymmetric shedding from the downstream cylinder.

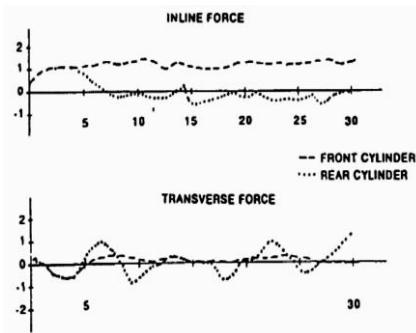


Figure 4 The Flow Patterns and Forces at $G/D = 2$ [12]

The comparison of the present results to those of [12], shows a. good agreement between the flow patterns and also the force coefficients at $G/D = 1.5$ as shown in Fig. 9 below. They used a, three level curvilinear grids generated from a solution of the Laplace equation. Close to the cylinder, a finer grid system was introduced which then overlapped with two coarser grids for the transport of the wake far from the cylinders.

As the vortices shed from the upstream cylinder approach the downstream cylinder, the drag coefficient of the downstream cylinder gradually declines until it settles and oscillates around a negative value of -0.2, which is close to the experimental results. Numerically, this effect is due to the presence of the vortices shed by the upstream cylinder approaching the upstream face of the downstream cylinder and interacting with the newly created vortices there so as to interfere with the normal relative contributions to the pressure distribution made by the upstream and downstream parts of the cylinder.

The force coefficients of the upstream cylinder experience a relatively small oscillating drag and lift coefficient as, at this gap ratio, the downstream cylinder acts as a splitter plate which suppress the regular oscillatory shedding of vortices from the upstream cylinder. The drag coefficient reduces from that of the isolated cylinder to be around 0.8 and the oscillating lift coefficient has a zero mean which is also close to the experimental results.

The lift coefficient of the downstream cylinder has a Strouhal number of around 0.16 and a maximum value of 0.5. This is quite close to the Strouhal number of the original experimental graph shown in Fig. 5 below.

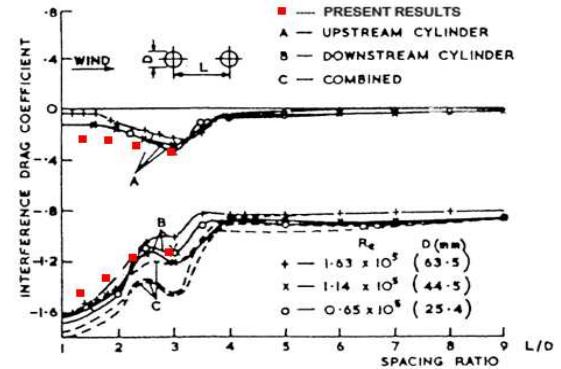


Figure 5 Interference Drag Coefficient

At a gap ratio 1, it is shown that the larger gap between the cylinders creates more space in the formation region of the upstream cylinder for the development of an oscillating wake. This influences the symmetrical properties of the reattachment position of the vortices shed from the upstream cylinder on the downstream cylinder.

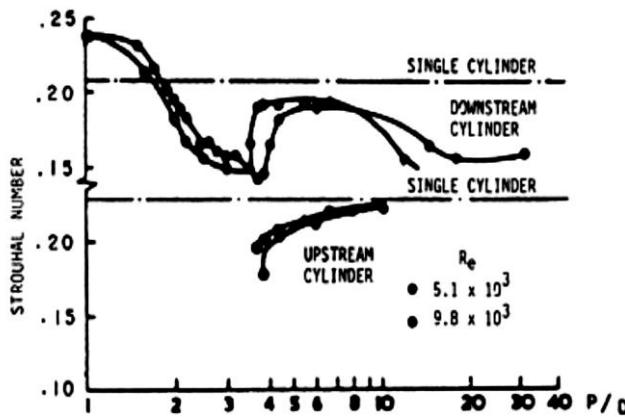


Figure 6 The Strouhal Number Behind Cylinder in Tandem from [1]

The oscillatory reattachment of the shear layers from the upstream cylinder causes an asymmetric vorticity distribution around the downstream cylinder. This phenomenon is reflected in the graphs of the force coefficients for the downstream cylinder, in which both the drag coefficient C_D and the lift coefficient C_L are oscillatory in nature. The lift coefficient is more oscillatory at a mean peak value 0.9 which is slightly higher than before, while the drag coefficient continues to oscillate about a zero mean, as shown in Fig. 8.

For gap ratio of $G/D = 1.5$, the larger gap causes the drag and lift coefficients of the downstream cylinder to oscillate more regularly about the zero mean, but there are no significant changes to the force coefficients of the upstream cylinder. This then creates a more regular Von Karman vortex street behind the downstream cylinder, similar to that of a single cylinder in isolation.

As the gap ratio of G/D is increased to 2, oscillation of the lift coefficient of the upstream cylinder begins to appear. This shows that the upstream cylinder is just on the verge of shedding vortices as is shown also in the flow visualisation in Fig. 10 below in which the shape of the formation region of the upstream cylinder is regularly asymmetric relative to the downstream cylinder position. In turn, this influences the behaviour of the force coefficients of the downstream cylinder which become less regular and for which the mean value of the peak lift and drag coefficients are 0.5 and 0.8 respectively.

This behaviour is in line with the experimental results as described by [1] for which at around this gap ratio, a sudden jump in the Strouhal number occurs for the downstream cylinder. Regular vortex shedding was first detected behind

the upstream cylinder, as shown in the Strouhal number curve illustrated in Fig. 6 above.

In a numerical experiment using the Finite Element method [13] at a low Reynolds number of 100, found that a similar trend occurred at around this gap ratio and they divided the flow into Vortex Suppression and Vortex

Formation regimes at gap ratios of 1.5 and 3.5. In the vortex suppression regime, as in the previous case, the gap ratio is less than the critical spacing. The shear layers separating from the upstream cylinder reattach to the downstream cylinder so that vortices do not have sufficient room to grow, to develop or to be shed. Since the downstream flow is in the attached vortex region of the upstream cylinder, the oncoming stream to the downstream cylinder is quite weak. When the gap ratio is greater than its critical value, as in the present case, a vortex formation regime begins to appear from behind both cylinders. The occurrence of vortex shedding between the two cylinders creates an oscillatory oncoming flow upstream of the downstream cylinder and this leads to a stronger oscillatory flow behind the downstream cylinder.

Experimental evidence, and also the results presented in Fig. 10, show that for a gap ratio greater than 2, the general trend of the flow visualisations and the associated force coefficients of the upstream cylinder behaves more and more like an isolated cylinder with the interference drag coefficient approaching to zero. The drag coefficient of the downstream cylinder, however, shows a consistently lower value than that of an isolated cylinder and settles at a value of around 0.5, which is slightly higher than the experimental values. The lift coefficient oscillates with Strouhal number 0.18 which is slightly less than that of the isolated cylinder.

For higher gap ratios, however, the present model failed to simulate the flow phenomena. This is because the formation region of the upstream cylinder imposes a strong unstable asymmetric distribution of newly created vorticity upon the downstream cylinder which develops to create all unrealistic flow pattern and corresponding force coefficients for both cylinders.

The results for the drag coefficient for the gap ratio G/D less than 2 have been compiled and are displayed in Fig. 8. The above results have also been represented in terms of the interference drag coefficient by deducting a drag for the isolated cylinder of 1.1. It is found that fairly good results are achieved for this particular range of the gap ratios.

Table 1. The CPU time percentage of each section of the Algorithm

Section Number	Purpose of Action	CPU Time
1	Input/ Output	0.03
2	Define Grid	0.00
3	Calculate Nodal Velocity	86.0
4	Calculate Vortex Velocity	0.33
5	Vortex Displacement	3.07
6	Distribute Circulation	0.37
7	Calculate Surface Velocity	9.61
8	Calculate Forces	0.01

The percentage CPU time used in calculating each intermediate stage of the computation is displayed in Table 1 above. The figures are based on a period of 400 time steps with around 570 active nodes for each cylinder polar grid and around 11200 vortices shed by each cylinder. In other word, there are about 1140 active nodes and about 22400 vortices in the flow.

5. CONCLUSIONS

This method can directly be applied for multi-cylinder cases with different dimensions at any configurations, as seen in the basic formulation and the methodology above. By using certain mathematical transformation, this method can also be developed further for predicting the flows about any two-dimensional shapes. One of the main difficulties in the flow around two cylinders in an infinite fluid implementing the present model has been in achieving results within practical time limits. As has been mentioned already, the algorithm does not include explicitly a turbulence model. Results resembling experimental results have been achieved over a wide range, but inevitably there are flow configurations for which turbulence effects will not allow representation of the flow in this manner.

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Availability of data and materials

The datasets supporting the conclusions of this article are included within the article.

Authors' contributions

All authors contribute to the whole manuscript

Competing interests

The authors declare no competing financial interests.

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Consent for publication

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Ethics approval and consent to participate

Not applicable

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Biographical notes

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Appendix

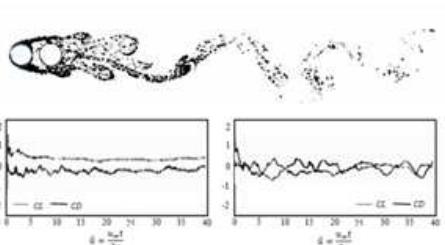


Figure 7 The Flow Pattern for G/D = 0.5, and the Force Coefficients for Re = 100000

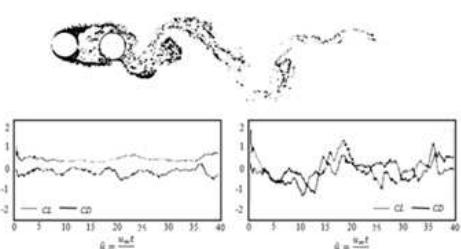


Figure 8 The Flow Pattern for G/D = 1, and the Force Coefficients for Re = 100000

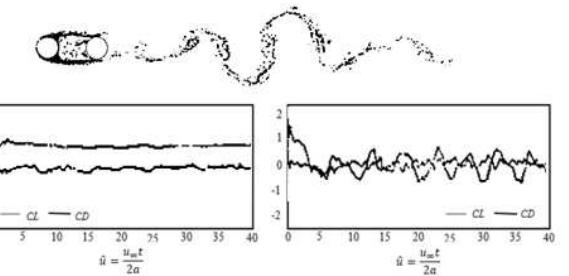


Figure 9 The Flow Pattern for G/D = 1.5, and the Force Coefficients for Re = 100000

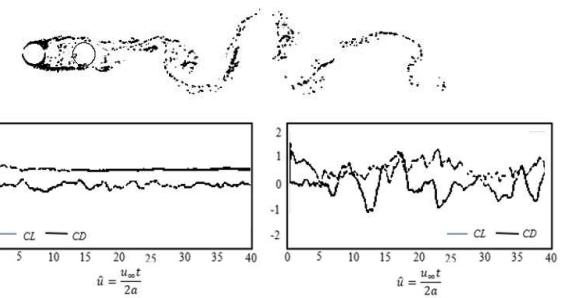


Figure 10 The Flow Pattern for G/D = 2, and the Force Coefficients for Re = 100000

Figures

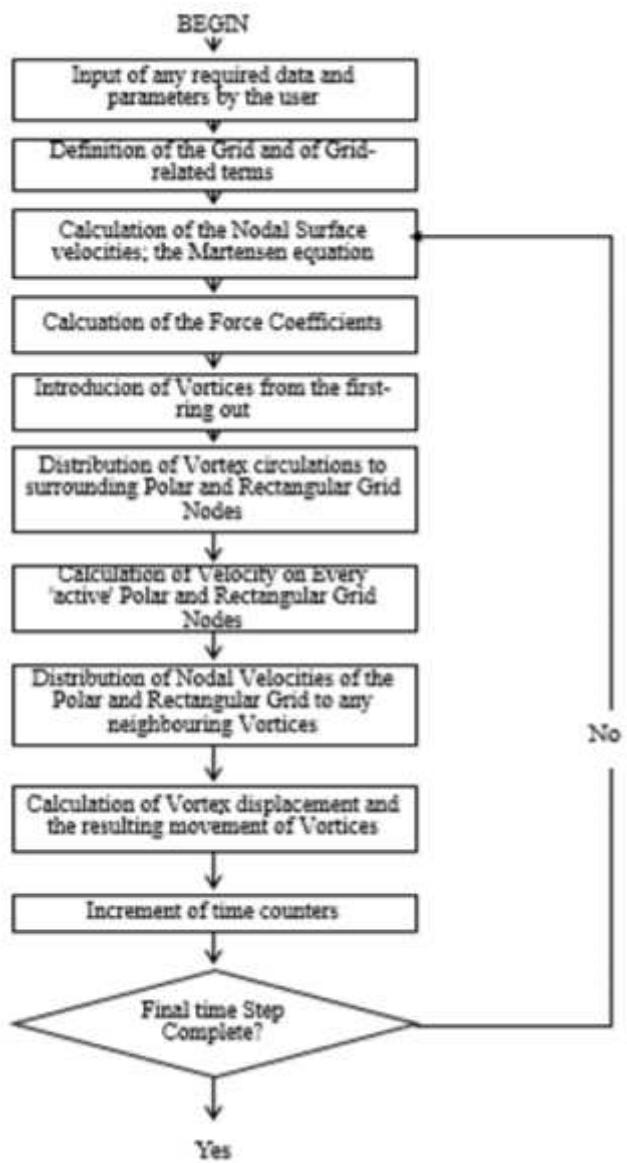


Figure 1

Flowchart of the Algorithm



Figure 2

The Flow Pattern at $G/D=1.5$, $t=1$ and 5



Figure 3

The Flow Pattern at $G/D = 1.5$

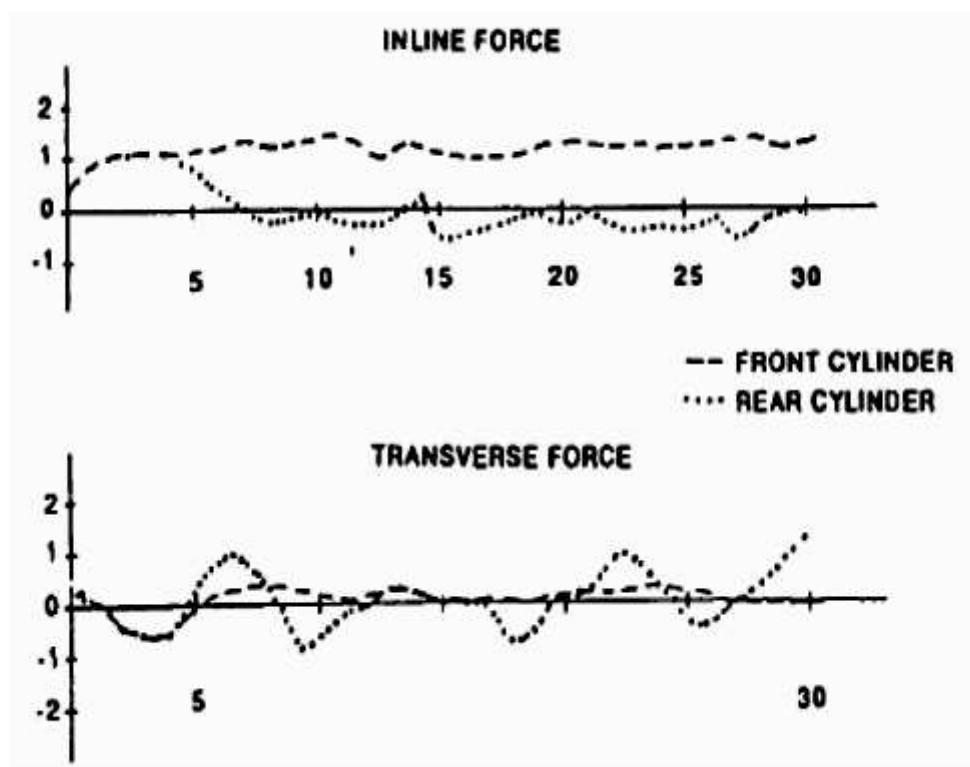


Figure 4

The Flow Patterns and Forces at $G/D = 2$ [12]

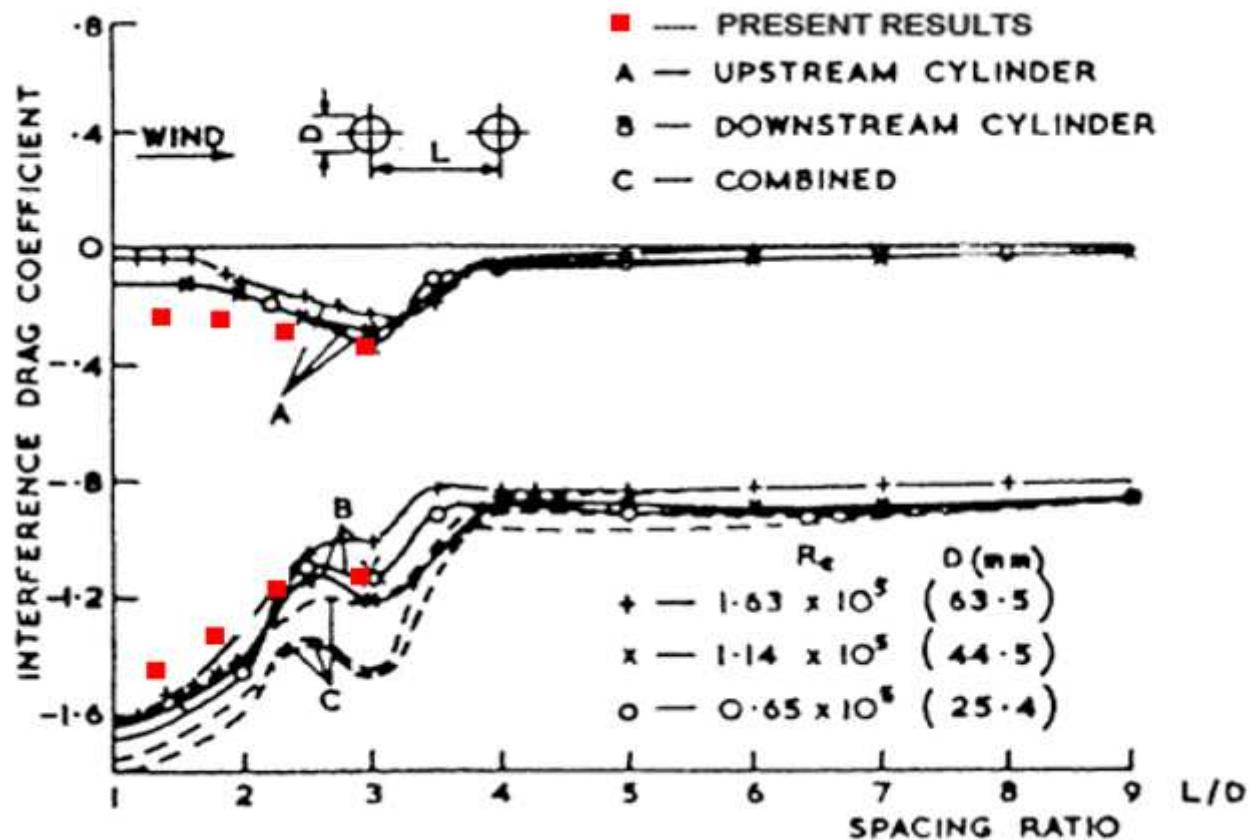


Figure 5

Interference Drag Coefficient

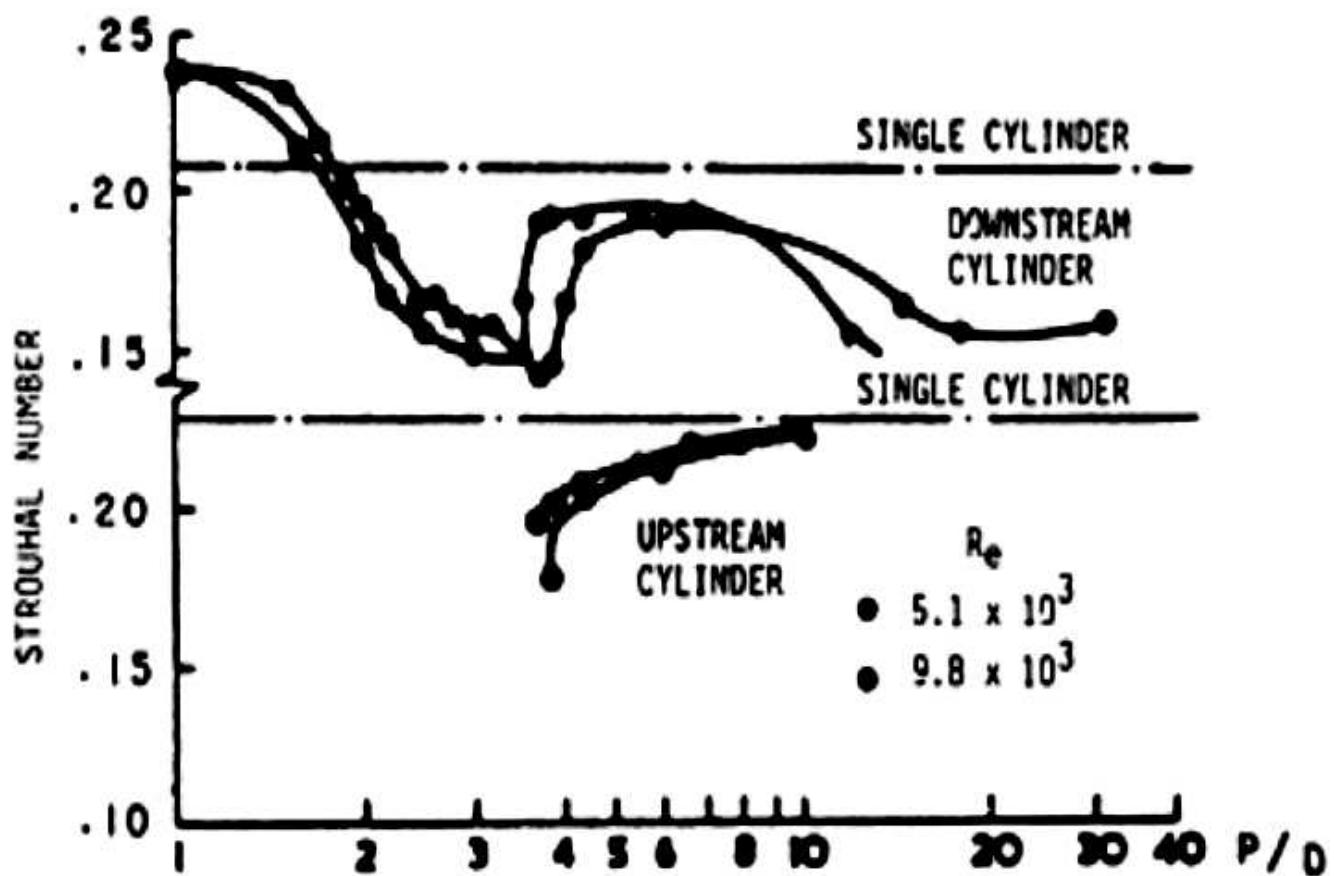


Figure 6

The Strouhal Number Behind Cylinder in Tandem from [1]

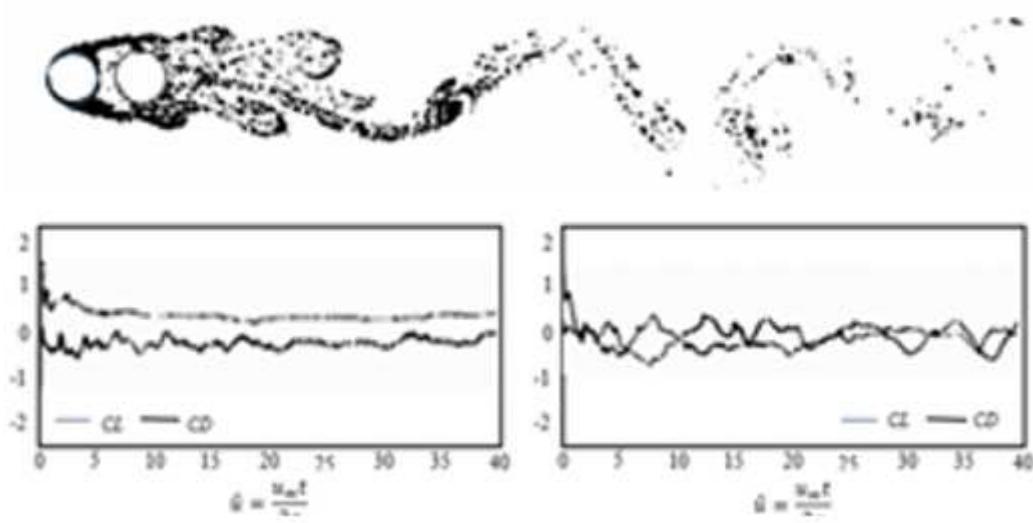


Figure 7

The Flow Pattern for $G/D = 0.5$, and the Force Coefficients for $Re = 100000$

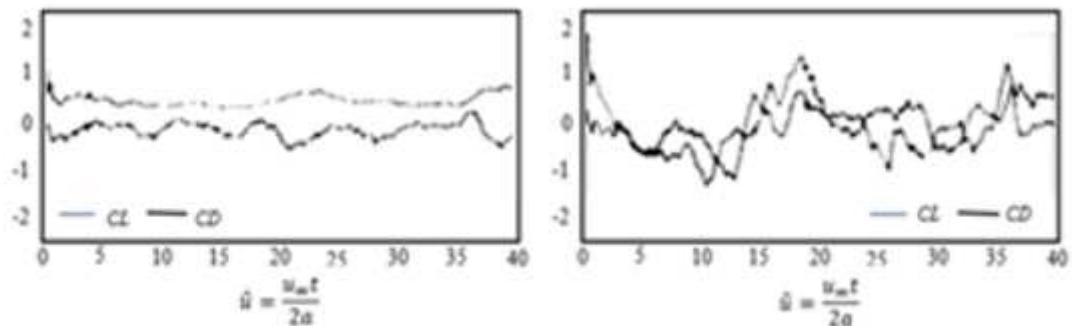


Figure 8

The Flow Pattern for $G/D = 1$, and the Force Coefficients for $Re = 100000$

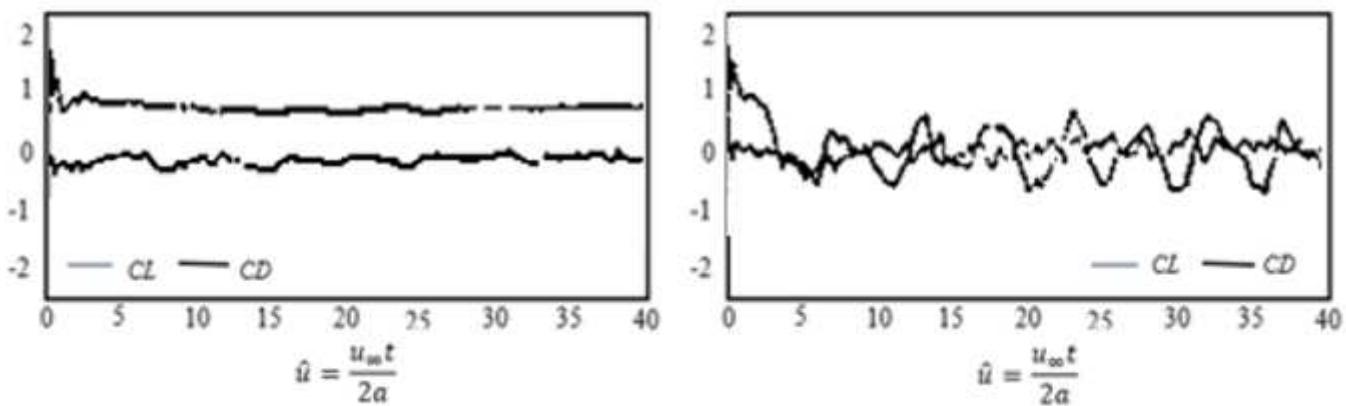


Figure 9

The Flow Pattern for $G/D = 1.5$, and the Force Coefficients for $Re = 100000$

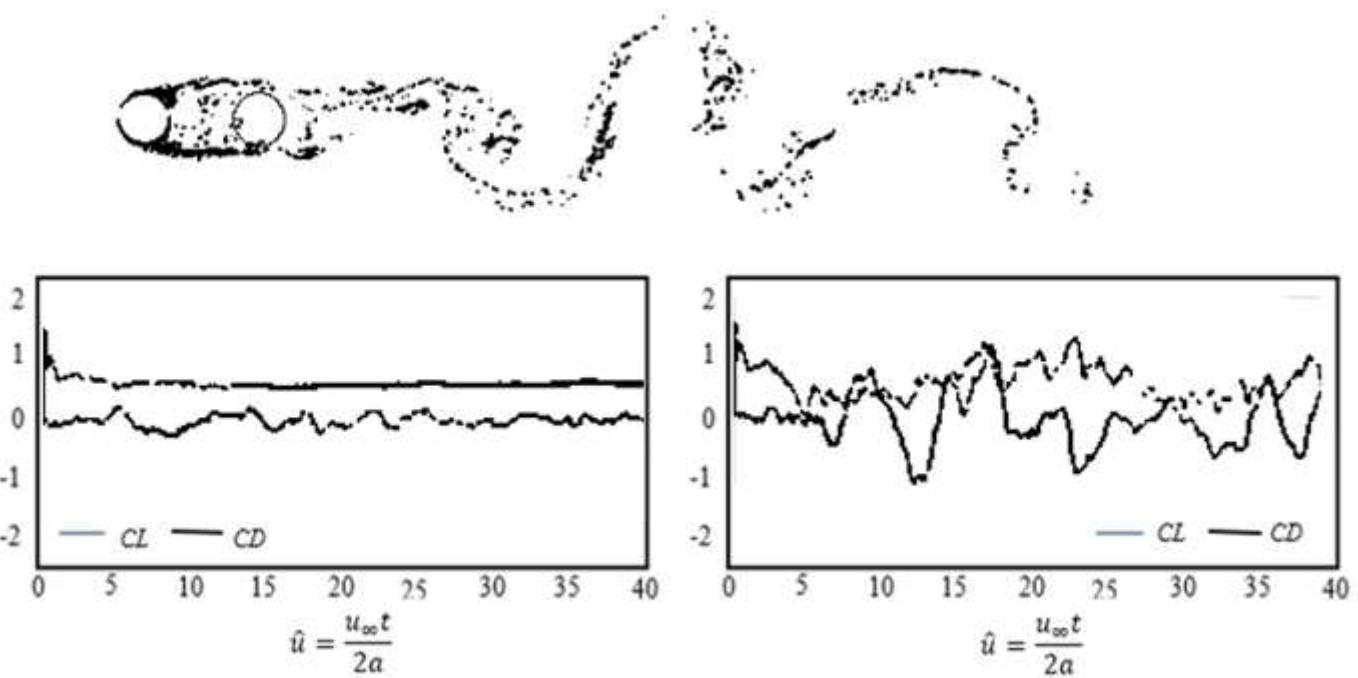


Figure 10

The Flow Pattern for $G/D = 2$, and the Force Coefficients for $Re = 100000$