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Research Article

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Posted Date: April 21st, 2022

DOI: <https://doi.org/10.21203/rs.3.rs-1332587/v1>

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Design and modeling of a D-shaped PCF refractive index sensor based on SPR effect

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Abstract

In this article, we propose and study a D-shaped plasmonic refractive index (RI) sensor. The numerical simulation is performed by the finite-element method (FEM). Results indicate that the proposed RI sensor is particularly proper for sensing in the wavelength range of 0.5 to 0.7 μm . When the analyte RI varies from 1.33 to 1.36, the highest wavelength sensitivity of 9500 nm/RIU and RI resolution of 6.5×10^{-6} RIU are obtained. Besides, the highest amplitude sensitivity of 215 RIU⁻¹ is achieved with a high linearity of 0.99862. These results confirm the capability of the proposed sensor for rapid and accurate detection of RI change in biological and industrial applications.

Keywords: Photonic crystal fiber, SPR, Sensor, refractive index, Sensitivity.

1. Introduction

SPR sensors are very efficient in many sensing applications owing to their privilege sensitivity and simple functionality. Photonic crystal fiber (PCF) can be regarded as an adequate sensing base mainly due to its small dimension and flexibility that provide more premier sensing features unveiled by combination of the surface-plasmon-resonance (SPR) phenomenon [1, 2]. Referring to the structural characteristics of a PCF used to manage light

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transmission, a series of optical parameters including nonlinearity, dispersion, effective mode field area, and mode birefringence, can be engineered practically. Consequently, sensing performance can also become much better. In recent years, D-shaped PCF sensors have been growingly developed and considered owing to the SPR effect. A D-shaped SPR sensor based on an all-solid PCF was introduced by Tian et al. and showed at least 7300 nm/RIU for spectral sensitivity [3]. In another attempt, a D-shaped PCF-SPR sensor with average sensitivity of 7700 nm/RIU and resolution of 1.30×10^{-5} RIU was proposed for RI range of 1.43–1.46 [4]. Wu and coworkers suggested a novel D-shaped sensor with the sensitivity of 31000 nm/RIU in NIR region [5].

Focusing on the visible and NIR region of spectrum, we modeled and simulated a simple D-shaped PCF-SPR sensor and surveyed the structural characteristics that influence the pertinent sensitivity. Regarding the chemical stability and resonance output energy of excitation materials, we considered silver (Ag) as the sensing-layer medium. The effect of the structural parameters on the sensing performance of the modeled sensor was analyzed by the FEM, and investigated the sensing performance to the analyte RI variations.

2. Details of modeling

Fig. 1a shows the cross-section illustration of the proposed sensor. The lattice pitch is $\Lambda=4$ μm , the diameter of air holes are represented by d_1 and d_2 , respectively, and we set $d_1 = 3.2$ μm and $d_2= 1.6$ μm . The thickness of Ag layer (T_{Ag}) is set 40 nm. The background material of the designed PCF is fused silica. The FEM is employed to study the PCF-SPR properties and sensing performance. The FEM discretized mesh is shown in Fig. 1b. The RI of fused silica is given by Sellmeier equation [6]:

$$n(\lambda) = \sqrt{\varepsilon + \frac{A}{\lambda^2} + \frac{B\lambda_1^2}{\lambda^2 - \lambda_1^2}} \quad (1)$$

where λ exhibits a free space wavelength, and $\varepsilon = 11.6858$, $\lambda_1 = 1.1071 \mu\text{m}$, $A = 0.939816 \mu\text{m}^2$, and $B = 8.10461 \times 10^{-3}$. The dielectric parameters of Ag can be determined from the L4 model [7]

$$\varepsilon(\omega) = \varepsilon_\infty + \frac{\sigma/\varepsilon_0}{i\omega} + \sum_{p=1}^4 \frac{C_p}{\omega^2 + A_p\omega + B_p} \quad (2)$$

all constants of Eq. 2 were adopted from Ref [7].

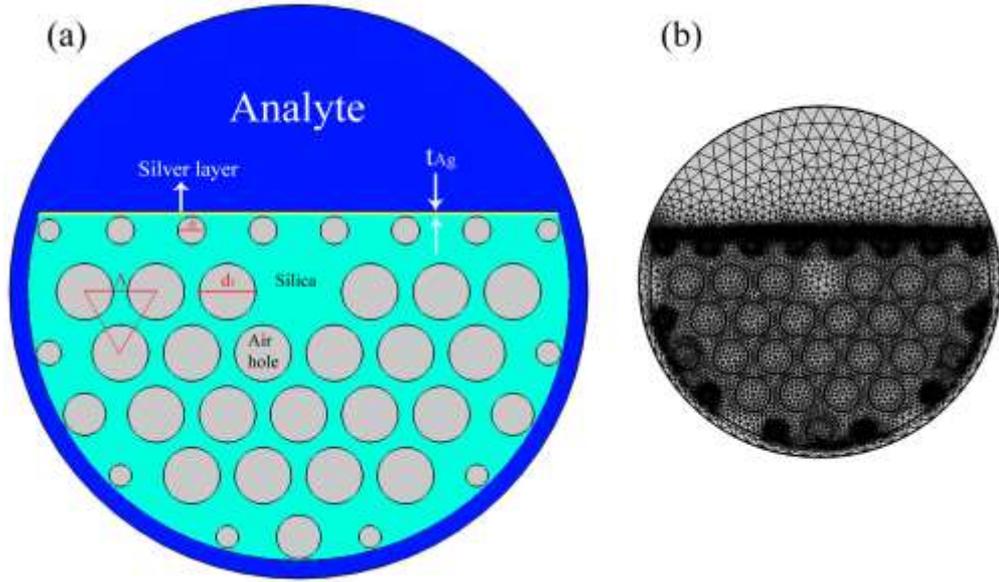


Fig.1. (a) cross-section view of the proposed sensor and (b) FEM discretized mesh.

The modes will couple, when their effective refractive index (n_{eff}) are equal. To investigate the coupling properties of the designed sensor, we display the n_{eff} curve and E-field distributions along with the loss spectra of the pertinent modes in Fig. 2. The confinement loss of the sensor can be characterized by using the following formula [7]

$$\alpha_{\text{Loss}} (\text{dB/cm}) = 8.686 \times \left(\frac{2\pi}{\lambda} \right) \times \text{Im}(n_{\text{eff}}) \times 10^4 \quad (3)$$

The sensitivity of the sensor of the RI unit (RIU) can be defined as [8]

$$S_n (\mu m / RIU) = \frac{\Delta \lambda_{peak}}{\Delta n_{Anl.}} \quad (4)$$

where $\Delta \lambda_{peak}$ denotes the shift of the resonance peak.

Since no spectral manipulation is required, it is more cost effective to utilize the amplitude interrogation technique (AIT) to investigate the performance of the sensor. The amplitude sensitivity can be calculated by [9]

$$S_{Amp.} (RIU^{-1}) = -\frac{1}{\alpha(\lambda, n_{Anl.})} \times \frac{\Delta \alpha(\lambda, n_{Anl.})}{\Delta n_{Anl.}} \quad (5)$$

where α , $\Delta \alpha$ and $\Delta n_{Anl.}$ stand for loss, loss difference and variation of the analyte RI, respectively.

3. Results and Discussion

In the simulated structure, (a) x-polarization core fundamental mode (FM) (Fig. 2a), (b) y-polarization core FM (Fig. 2b), and (c) SPP mode in the sensing layer (Fig. 2c) are analyzed. When light interacts with Ag layer on the Ag-analyte interface, both x and y-polarization FMs appear in the core, but only x-polarization FM can stimulate the surface plasmons.

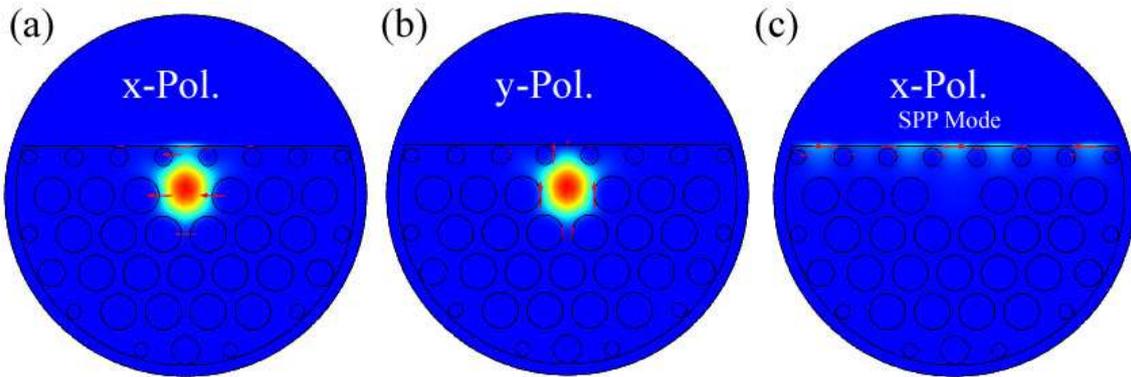


Fig. 2. Mode pattern of (a) x-polarization core (b) y-polarization core and (c) SPP fundamental mode.

Based on the dispersion relations of the x-polarization FM and plasmonic mode in Fig. 3, a detectable loss signal at the intersection (phase matching point) of the two RI curves is quite evident. At the mode-resonance conditions, the evanescent field in the fiber is remarkably boosted, and a strong loss peak rises. In our study, only x-polarization FM can resonate with SPP mode at $\lambda = 500$ nm. Therefore, only one loss peak at the intersection of the two curves rises that is very proper to be utilized in the sensing field. Owing to the uniqueness of resonance peak in the sensor, the accurate detection of the analyte RI can be gained.

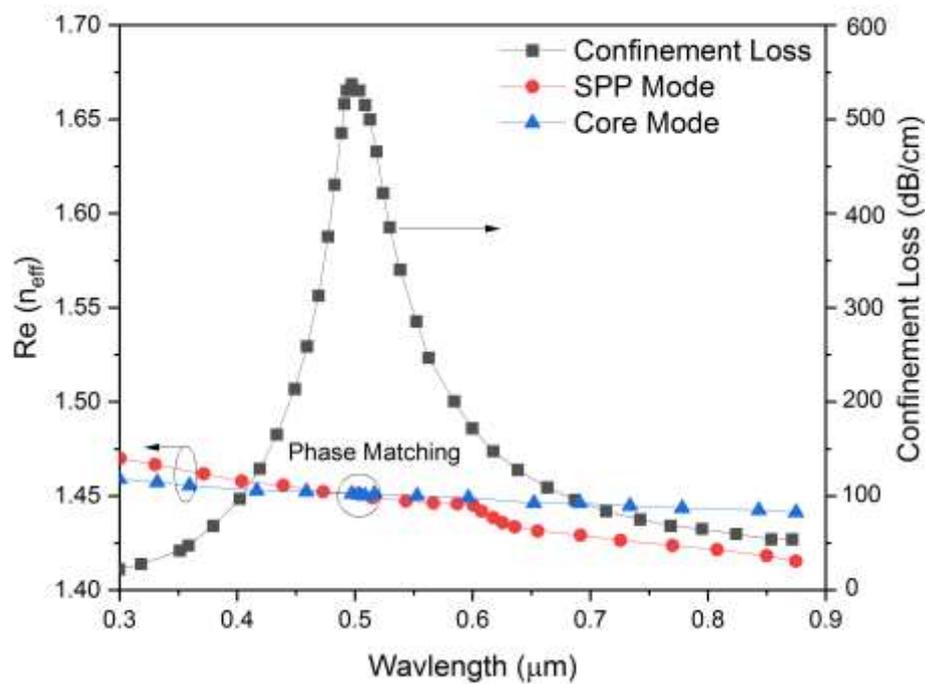


Fig. 3. The relation of radiation between the fundamental core-guided mode and SPP mode with $n_{\text{Anl}} = 1.33$.

The effect of the PCF structural parameters on the sensing characteristics of the proposed sensor is also investigated. Fig. 4 illustrates the loss spectra for different d_1 values with $n_{\text{Anl}} = 1.33$. As it is obvious, the position of resonance peak is red-shifted as d_1 increases. At the same time, the intensity of resonance signal also changes; particularly in the case of $d_1 = 4.2 \mu\text{m}$, the sharpness of the signal is reduced and widened. This coincides with decrement in

the core area which made it difficult to keep good single-mode transmission of the PCF, so x-polarization FM cannot produce a strong mode-coupling effect with the SPP mode.

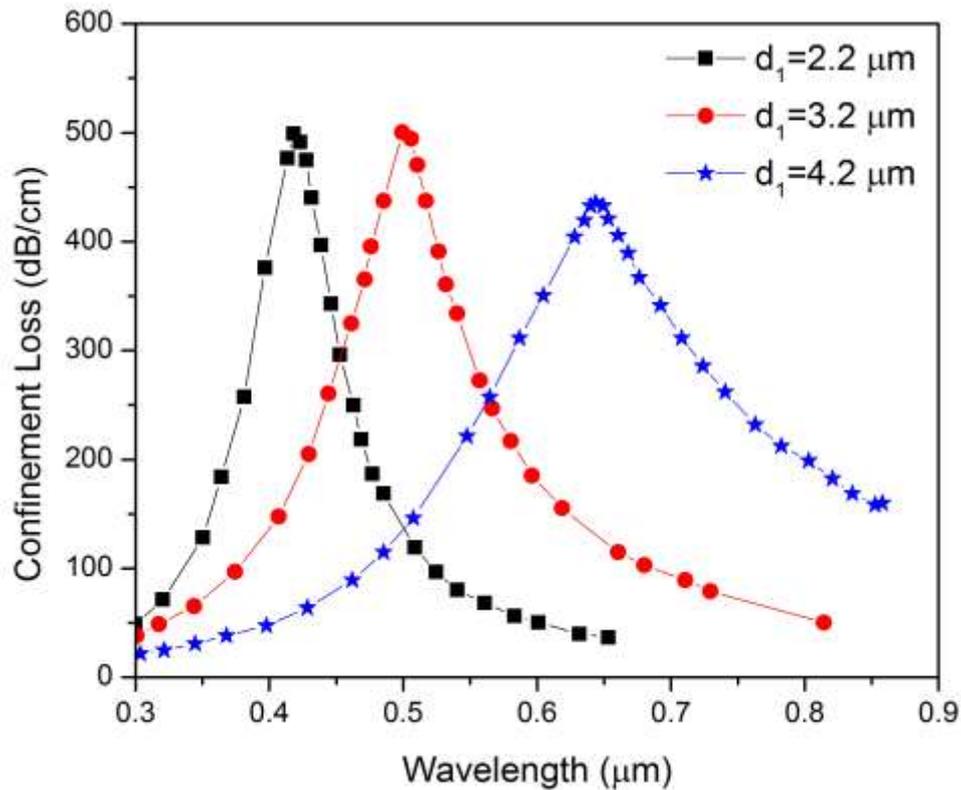


Fig. 4. Variation of the confinement loss spectra for different d_1 values.

For $d_1 = 2.2$ and $3.2 \mu\text{m}$, the energy generated by the latter is also slightly larger than that of the former; if more loss energy is generated, the peak will be easier to detect, hence the case of $d_1 = 3.2 \mu\text{m}$ is opted for the next step of analysis.

The effect of different silver-layer thicknesses (T_{Ag}) on the sensor performance is also studied and shown in Fig.5. As the T_{Ag} increases, the confinement loss is blue-shifted, and the pertinent intensity decreases. That is why the thinner thickness of the silver layer causes more light-matter interaction that leads to more free oscillation of surface plasmon. This event also boosts the evanescent field near the dielectric interface. Hence, $T_{Ag} = 20 \text{ nm}$ is selected as the optimum thickness for the next stage of simulation.

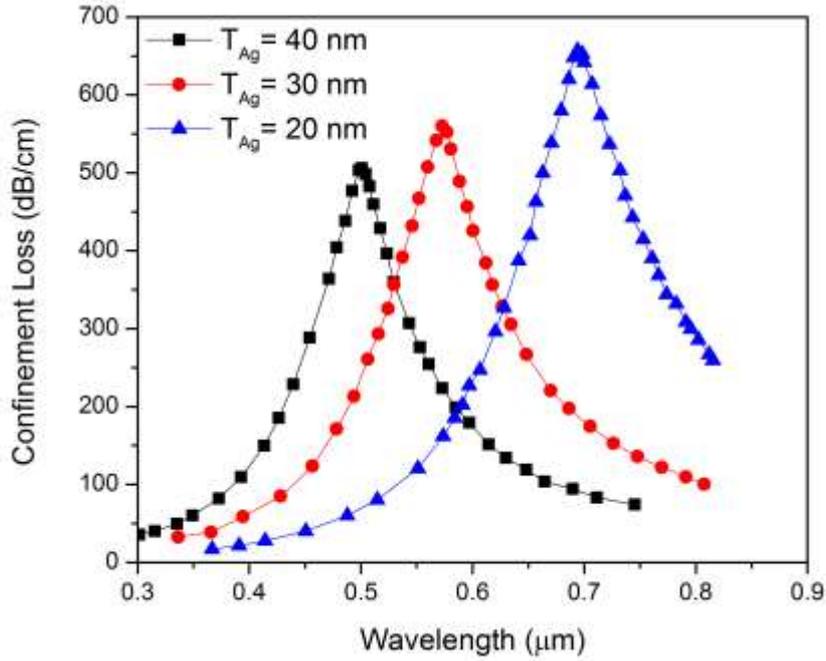


Fig. 5. Variation of the core mode confinement loss spectra of the proposed RI sensor for different thickness of silver layer.

The influence of different lengths of the lattice pitch on the confinement loss spectra of the proposed RI sensor is also investigated. Fig. 6 depicts the calculated confinement loss spectra for three different values of Λ . It is clear from the figure that, with the increase of Λ , the loss peak shifts towards the shorter wavelengths and the related intensity increases. The reason behind this behavior is that, as the Λ increases, the light in the core penetrates more into the cladding, and the evanescent electromagnetic field increases which leads to loss enhancement.

It is well known that the performance of the RI plasmonic PCF sensor relies on the shift of the position of the resonance peak associated with the change of the detected analyte RI. Owing to the uniform distribution of the loss spectra and the single peak in the investigated band, the proposed sensor seems very proper for sensing applications. Fig. 7 displays the confinement loss spectra for different analyte RIs from 1.33 to 1.36. Using the wavelength–interrogation–method, when the RI varies from 1.33 to 1.36, the corresponding resonance wavelength can be tuned from 0.5 to 0.7 μm . Results reveals that the average $\Delta\lambda_{\text{peak}}$ is about

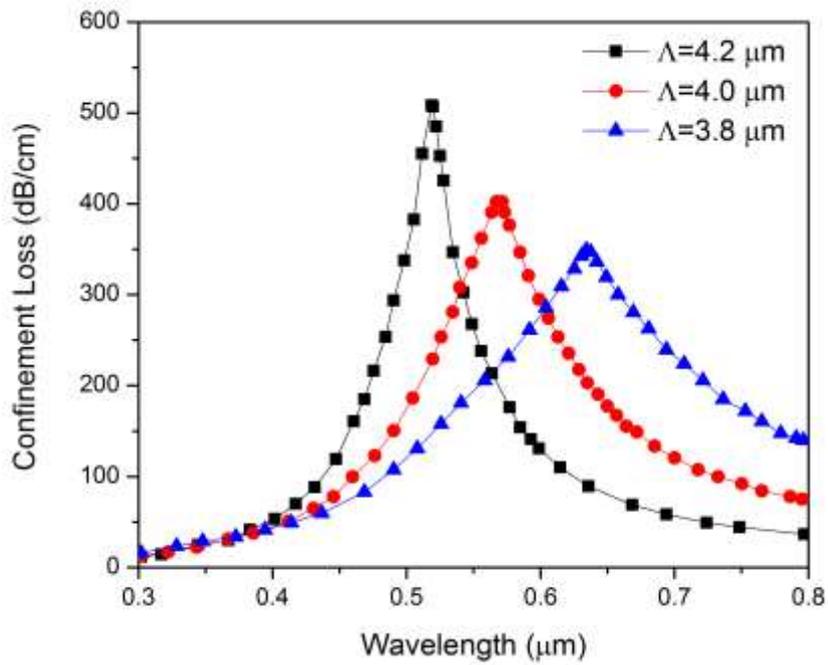


Fig. 6. Variation of the core mode confinement loss spectra of the proposed RI sensor for different values of the lattice pitch Λ .

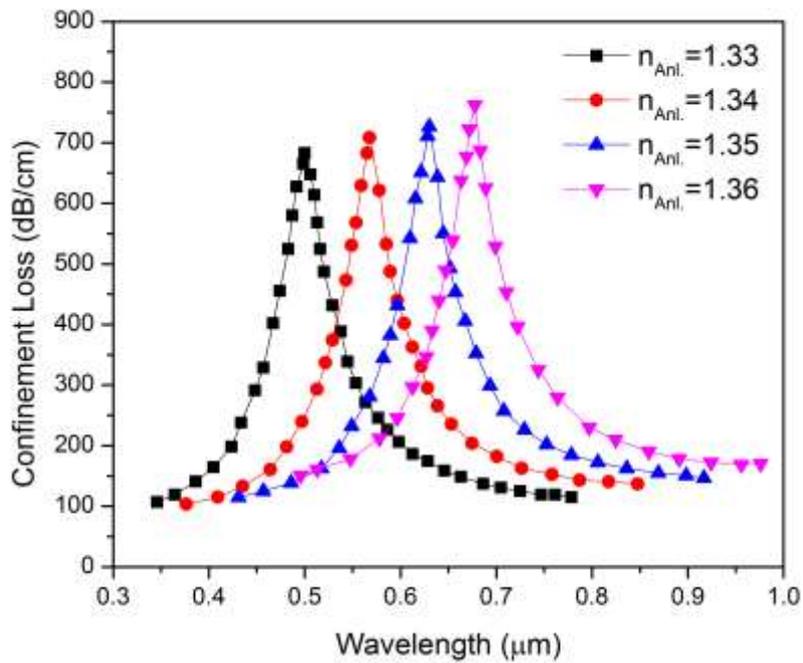


Fig. 7. Variation of the confinement loss spectra of the proposed RI sensor for different values of analyte RI.

77 nm; thus, the average wavelength sensitivity (S_n) (Eq. 4) is 7700 nm/RIU in this sensor. The maximum S_n occurs as the analyte RI varies from 1.33 to 1.34. The maximum sensitivity reaches 9500 nm/RIU, and the corresponding RI resolution is 6.5×10^{-6} RIU. Fig. 8 exhibits the amplitude sensitivity with different analyte RIs calculated by AIM. We observe that the corresponding peak intensity decreases as RI changes from 1.33 to 1.36, and maximum amplitude sensitivity reaches 215 RIU^{-1} when $n_{\text{Anl.}}$ is 1.33.

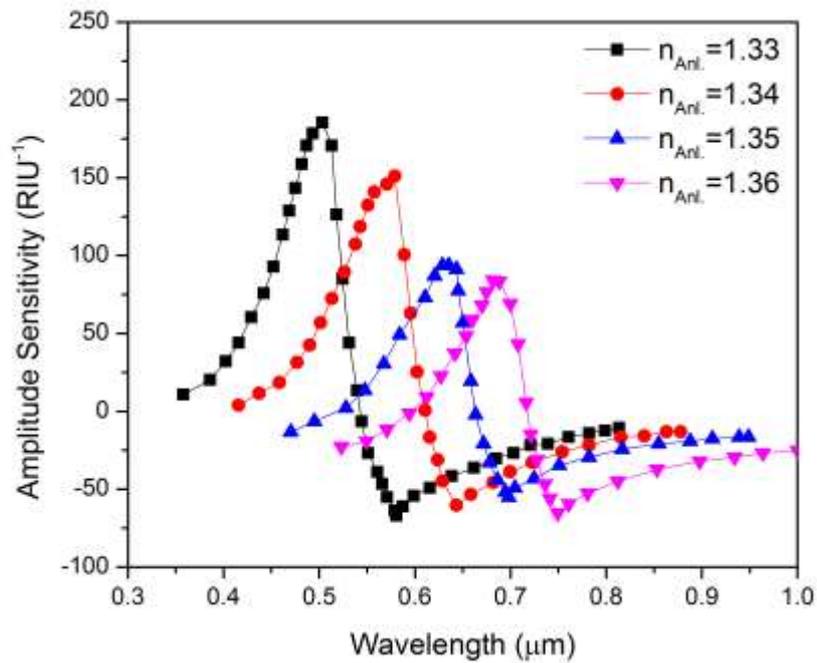


Fig. 8. The calculated amplitude sensitivity of the proposed sensor for different analyte RIs.

Finally, we analyzed the linearity of the proposed sensor by fitting the values of the resonance wavelengths versus analyte RIs (Fig. 9):

$$\lambda_{\text{Peak}} = 6.6n_{\text{Anl.}} - 8.3 \quad (6)$$

The adjusted residual-square (R^2) of 0.99862 was found for the fitting equation indicating a highly linear correlation degree between $n_{\text{Anl.}}$ and λ_{Peak} .

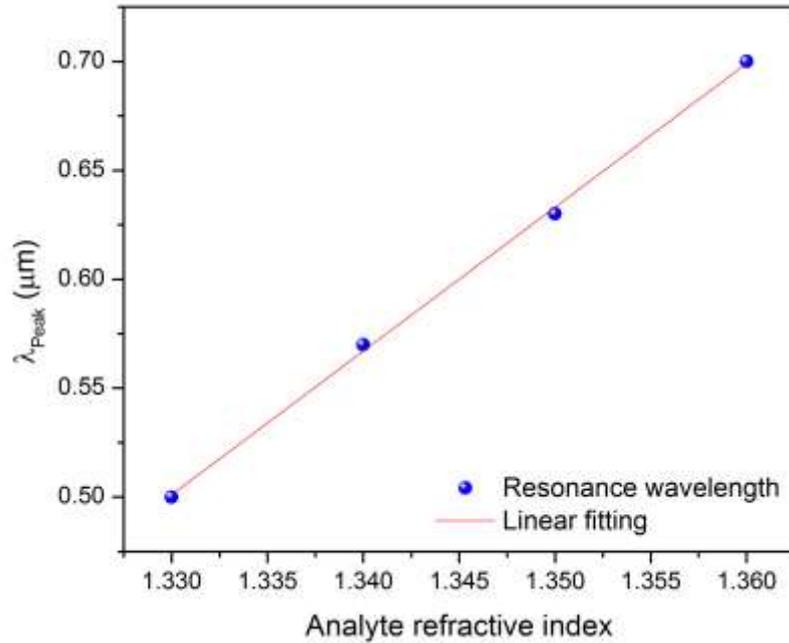


Fig. 9. The analysis of linearity degree between the resonance wavelength and analyte RI.

Compare to the other structures [10–12], the convenient design and high sensitivity of the proposed sensor, make it suitable for many applications.

4. Conclusion

In brief, we numerically analyzed the sensing properties of a high-performance visible D-shaped PCF–SPR RI sensor. The finite element method was used to investigate the sensing performance. The effect of the structural characteristics, and the relation between the resonance wavelengths and analyte refractive index were also studied. Using the wavelength interrogation method, an average wavelength sensitivity of 7700 nm/RIU and an average RI resolution of 1.08×10^{-5} RIU were attained. Also, the maximum wavelength sensitivity and RI resolution of 9500 nm/RIU and 6.5×10^{-6} RIU were achieved, respectively, for the analyte RI between 1.33 and 1.34. Furthermore, the amplitude sensitivity of 215 RIU^{-1} at $n_{\text{Anl.}}=1.33$ was observed from the calculations.

Funding declaration

This study didn't use any fund.

Author declaration

[Instructions: Please check all applicable boxes and provide additional information as requested.]

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We wish to draw the attention of the Editor to the following facts, which may be considered as potential conflicts of interest, and to significant financial contributions to this work:

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No conflict of interest exists.

We wish to confirm that there are no known conflicts of interest associated with this publication and there has been no significant financial support for this work that could have influenced its outcome.

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Funding was received for this work.

All of the sources of funding for the work described in this publication are acknowledged below:

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Availability of data and material

All data are available whenever were asked.

Code availability

The code will be available whenever is asked.

Authors' contributions

- 1- Amin Sayyad Tondro performed the calculations.
- 2- Mojtaba Sadeghi analyzed the results and prepared the figures.
- 3- Abbas Kamaly contributed in writing the text.
- 4- Zahra Adelpour contributed in discussions.
- 5- Ali Emamghorashi contributed in analysis and discussion.

Ethics approval

I, Mojtaba Sadeghi, corresponding author of the manuscript, am enclosing herewith a manuscript entitled “Modeling and analysis of D-shaped plasmonic refractive index and temperature sensor using photonic crystal fiber” submitted to Journal of Computational Electronics for possible evaluation. With the submission of this manuscript I would like to undertake that the above mentioned manuscript has not been published elsewhere, accepted for publication elsewhere or under editorial review for publication elsewhere; and that my Institute’s Islamic Azad University, Shiraz branch representative is fully aware of this submission.

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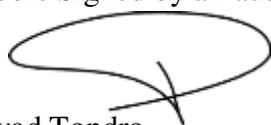
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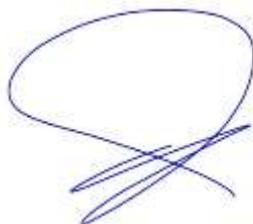
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I, the undersigned, give my consent for the publication of identifiable details, which can include photographs and details within the text to be published in the above Journal and Article.

Dr. Mojtaba Sadeghi**Corresponding Author**

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