

1 **The efficacy of a motorized lower-limb prosthetic device: a pilot study**

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24

25 **Abstract**

26 *BACKGROUND* Performing daily activities is challenging for individuals with a transfemoral amputation. Tech-
27 nological advancements in prosthetic prototypes aim at improving functional independence. A state-of-the-art ac-
28 tive device, the CYBERLEGs-gamma (CLs- γ) prosthesis, consisting of powered ankle and knee joints, has been
29 designed and constructed. The control system combines pressure-sensitive insoles and inertial motor units to syn-
30 chronize both joints to work together. To date, the novel device has not been clinically evaluated. Therefore, the
31 objective of this study was to investigate the efficacy of the CLs- γ prosthesis during daily activities compared to
32 current passive and quasi-passive devices.

33 *METHODS* Participants performed a familiarization trial, an experimental trial with the current prosthesis, three
34 adaptation trials and an experimental trial with the CLs- γ prosthesis. Participants completed a stair climbing test,
35 a timed-up & go test, a sit to stand test, a two-minute dual task (i.e. the psychomotor vigilance task during treadmill
36 walking) and a six-minute treadmill walk test at normal speed. Nonparametric Wilcoxon-signed rank tests were
37 conducted with critical alpha set at 0.05.

38 *RESULTS* Eight individuals with a transfemoral amputation (age: 55 ± 15 years, K-level 3) were included. Stride
39 length significantly increased during walking with the CLs- γ prosthesis ($p=0.012$) because of a greater step length
40 of the amputated leg ($p=0.035$). Normal walking speed was significantly slower ($p=0.018$), the net metabolic cost
41 of transport was significantly higher ($p=0.028$) and reaction time significantly worsened ($p=0.012$) when walking
42 with the CLs- γ compared to the current prosthesis. When participants took stairs, they adopted a step-over-step
43 strategy with the CLs- γ prosthesis in contrast to step-by-step wearing the current prosthesis.

44 *CONCLUSIONS* A higher physical effort and cognitive demand were required during activities wearing the novel
45 motorized prosthesis. Although performance outcome measures did not improve, participants had a greater stride
46 length and better simulated able-bodied stair ambulation.

47
48 Trial registration: NCT03376919.

49 Registered 19 December 2017.

51 **Keywords**

52 Transfemoral – Amputation – Powered – Prostheses – Ankle – Knee – Clinical evaluation – Daily activities –
53 Robotics

54 **Background**

55 Performing daily activities can be challenging for individuals with a transfemoral amputation (TFA). For example,
56 a higher metabolic cost and reduced physical performance are shown during walking, ramp ambulation, stair
57 climbing and rising from a chair [1–4]. Moreover, task characteristics differ. People with a TFA often ambulate
58 stairs step-by-step, whereas step-over-step is common for able-bodied individuals [3]. During walking, an
59 asymmetrical pattern is observed and additional attentional effort is required due to the lack of information coming
60 from the proprioceptive system and loss of motor control [5, 6]. These challenges and adaptations lead to the
61 development of secondary complications such as lower-back problems, osteoarthritis and discomfort of other joints
62 [7].

63
64 The amputation of a limb is the leading cause for the aforementioned deficiencies. Current passive and quasi-
65 passive devices can already restore certain daily functions. However, large improvements are possible through
66 technological advancements. For example, active (powered, motorized) prostheses are already on the market, but
67 are yet under-prescribed and under-utilized [8]. The reasons are the large costs related to the use of an active
68 prosthesis and limited reimbursements by the health companies. Moreover, current active prostheses focus on
69 improving walking abilities [9]. Although walking is a common daily activity, people with an amputation feel
70 reduced functionality during many other daily activities. Therefore, the main goal of a novel prosthesis is to restore
71 the loss of function so that individuals regain an independent lifestyle in society, participate in physical activities
72 and thus improve their quality of life.

73
74 Engineers from the Vrije Universiteit Brussel recently designed, developed and constructed the CYBERLEGS-
75 gamma (CLs- γ) prosthesis (Figure 1), the successor of the beta-version[10]. The novel prototype (technology
76 readiness level: 5) consists of an integrated controller in the knee and ankle joints [11]. At the ankle joint, an
77 actuator provides torque by compressing or decompressing series elastic springs, whereas a parallel spring system
78 acts between the shank and the foot to reduce energy consumption by storing potential and kinetic energy during
79 dorsiflexion and releasing it during plantarflexion [12]. At the knee joint, the actuator provides resistance, similar
80 to eccentric muscle power, during the weight acceptance phase and is activated right before heel strike. Afterwards,
81 the controller provides active torque, similar to concentric muscle power, during the stance phase when the knee
82 is extending. The motion is constrained to the sagittal plane, i.e. flexion and extension. The CLs- γ prosthesis
83 comprises the control system and electronics in the leg structure and still requires an external power source (battery

84 pack) to be placed on the pelvis. Electronics of the system are custom made boards to control not only the
85 prosthesis, but also act as interface between the pressure-sensitive insoles that are instrumented in the shoes of
86 both feet and the inertial motor units that are attached to the trunk and lower limbs [13]. A more detailed
87 mechatronic description is available in literature [14].

88

89 [Insert figure 1]

90 **Figure 1.** The CYBERLEGs-gamma prosthesis. The knee actuator consists of the motor, gearbox and spindle, and
91 the springs in series, acting on the knee joint through metal beams. The wearable apparatus consists of a motor
92 moving the spring in and out of place. The ankle actuator consists of the motor, gearbox, and series and parallel
93 springs acting on the ankle joint. The ankle and knee are clamped together, allowing a change in distance between
94 the joints.

95

96 Evaluation of a prosthetic prototype is key in the iterative process of design and development of an innovative
97 medical device. While prototype efficacy could provide valuable information for the engineers, the iterative
98 evaluation process could be optimized by using a holistic approach which includes psychophysiological,
99 biomechanical and physical performance outcome measures [9, 15]. Walking trials are frequently investigated,
100 however, other daily activities, such as rising from a chair, taking turns and stair climbing are also important to
101 improve the ecological validity of the experiment [16].

102

103 The aim of this study was to evaluate the CLs- γ prosthesis during daily activities. We hypothesized improved
104 physical performance during stair climbing, sit to stand and walking with the CLs- γ compared to the current
105 prosthesis. It was also hypothesized that walking with the CLs- γ restored a more symmetrical walking pattern (e.g.
106 step length and width, stance and swing phases, and heel pressure), and decreased physical (e.g. metabolic cost,
107 heart rate and rating of perceived exertion) and cognitive (e.g. reaction time) effort compared to the current
108 prosthesis.

109

110 **Methods**

111 *Recruitment*

112 Nine participants with a transfemoral amputation (K-level > 2) were enrolled in the study [17]. The recruitment
113 process was performed by the physiotherapist of an orthopaedic centre (VIGO, Wetteren, Belgium), where

114 experiments took place. Medicare Functional Classification level was subjectively determined by two independent
115 physiotherapists (JG and PVDV) and in case of disagreement a medical doctor was contacted. The study was
116 approved by the institutional medical ethics committee of UZ Brussel and Vrije Universiteit Brussel (Belgium,
117 B.U.N. 143201732970) and the Federal Agency for Medicines and Health Products (FAMHP reference number:
118 80M0725). All participants were provided written and verbal information about the experimental protocol,
119 potential risks and benefits before giving informed consent to participate in the study.

120

121 *Experimental protocol*

122 Each participant visited the laboratory six times for a familiarization session, an experimental trial with their
123 current prosthesis, three adaptation trials and an experimental trial with the CLs- γ prosthesis (Figure 2). The total
124 duration of this experiment (within subject design) was eight months. The environmental humidity, pressure and
125 temperature of the laboratory was set at $48 \pm 6\%$, 764 ± 8 mmHg and 24.5 ± 1.6 °C; respectively. All appointments
126 took place in the morning at the same hour and at least 24 hours between each session was planned to counteract
127 fatigue. The familiarization trial aimed to accustom participants to the experimental protocol, to get used to the
128 measurement devices and to determine the participants' normal walking speed. Normal walking speed was
129 determined through verbal feedback from the participant. The investigator altered the walking speed until the
130 participant confirmed the speed is consistent with the normal walking speed [18]. The recorded walking speed was
131 kept constant during the experimental treadmill trials to enable comparisons between conditions. Furthermore, a
132 duplicate of the participants' current socket was made to optimise fitting and alignment of the novel prosthesis.
133 Participants were fitted to the novel device by a certified prosthetist and instructed during the different tasks by a
134 physiotherapist.

135

136 [Insert Figure 2]

137 **Figure 2.** Experimental protocol including a familiarization trial – an experimental trial with the current prosthesis
138 (passive or quasi-passive device) – three adaptation sessions to the novel prosthesis (i.e. the CYBERLEGS-gamma
139 (CLs- γ) prosthesis) – an experimental trial with the CLs- γ prosthesis. The five tasks were a stair climbing test, a
140 timed-up & go test, a sit to stand test, a two-minute dual task and six-minute treadmill walk test.

141

142 The main experimental trials with the current and CLs- γ prosthesis consisted of five consecutive tasks with ten
143 minutes of rest between each task: the stair climbing test (SCT), the timed-up & go test (TUG), the sit to stand test

144 (STS), a two-minute dual task (i.e. the psychomotor vigilance task during treadmill walking) and a six-minute
145 treadmill walk test (6MWT) [16, 19–23]. Description of each task can be found in aforementioned references. The
146 walking tests were carried out at normal walking speed. Remark that during the psychomotor vigilance task
147 participants had to respond by pushing a button with the index finger of their dominant hand. Earplugs were
148 required during the task to reduce distraction related to sound. The visual stimulus, displayed as a red dot, was
149 visualized on a computer screen with a random time interval between 1000 and 10000 ms. The interval stimulus-
150 response onset was set at 500 ms and the distance to the screen was approximately one meter.

151
152 Between the experimental trials with the current and CLs- γ prosthesis, participants underwent three adaptation
153 trials. The focus of adaptation differed among each trial: (i) socket fit and walking, (ii) alignment and SCT, (iii)
154 STS and TUG. Participants were fitted and aligned to the novel device by a certified prosthetist and instructed
155 during the different tasks by a physiotherapist. During each adaptation session, participants also performed hallway
156 walking for ten minutes. Participants were free to move at their own pace and if needed crutches were allowed.

157

158 *Dependent measures*

159 Physical performance determinants were gathered in terms of duration (s) of the SCT and TUG, number of cycles
160 during the STS, reaction time (ms) during the psychomotor vigilance task, normal walking speed ($\text{m}\cdot\text{s}^{-1}$) and
161 cadence ($\text{steps}\cdot\text{min}^{-1}$) during the 6MWT. Biomechanical outcome measures (spatiotemporal and kinetics data)
162 were recorded during walking. Cadence ($\text{steps}\cdot\text{min}^{-1}$), maximum heel pressure ($\text{N}\cdot[\text{cm}^2]^{-1}$), stance and swing phase
163 (% of gait cycle), step width (cm) and stride length (cm) were reported. Physiological outcome measures
164 (cardiovascular and respiratory) were collected in terms of heart rate (bpm) and session rating of perceived exertion
165 (score between 0-10) after each experimental test. Oxygen uptake ($\text{mL}\cdot[\text{min}\cdot\text{kg}]^{-1}$), ventilation ($\text{L}\cdot\text{min}^{-1}$) and
166 metabolic equivalents were gathered during the 6MWT. Psychological outcome measures like the visual analogue
167 scale (score on 100) for fatigue were collected after the five tests [24]. The EuroQol-5D (score on 100) was filled
168 in before the test with the CLs- γ and current prosthesis [25]. Other questionnaires were completed during the
169 familiarization, i.e. the prosthetic evaluation questionnaire and the system usability scale.

170

171 *Measurement devices and data analysis*

172 Spatiotemporal and kinetics data were collected with the Zebris software (Medical GmbH, Isny, Germany).
173 Ground reaction force time-series were automatically reduced to zero-dimensional maxima under the forefoot,

174 midfoot and heel. Cadence, stance and swing phases, step width, step and stride length were continuously
175 determined. Gait variability, expressed as the coefficient of variation, was calculated for step width, and step and
176 stride length from the standard deviation dividing by the mean [26]. Ergospirometrical data were continuously
177 gathered during the 6MWT using a portable system (Cosmed K5[®], Cosmed, Rome, Italy). Preceding each test, a
178 calibration (volume, ambient air and reference gas) was performed after a system warm-up period of thirty minutes.
179 The setting mixing chamber was used, and data was continuously transferred to the program Omnia (Cosmed).
180 The device was mounted on the back of the participant with a harness. The net metabolic cost of transport
181 ($\text{mL} \cdot [\text{m} \cdot \text{kg}]^{-1}$) was calculated from dividing the relative oxygen uptake ($\text{mL} \cdot [\text{min} \cdot \text{kg}]^{-1}$) by the product of the
182 duration of the test (min), the weight (kg) of the participant and the distance (m) covered during the test [27].
183 Heart rate was measured at the end of each task with an elastic belt strapped around the chest (Polar M400[®], H7-
184 sensor, Kempele, Finland). The performance outcome measure of the psychomotor vigilance task was reaction
185 times, measured with E-prime 3.0 (Psychology Software Tools, Sharpsburg, USA).

186

187 *Statistical analysis*

188 Data are presented as mean (standard deviation). SPSS version 25.0 (International Business Machines Corporation,
189 New York, USA) was used for statistical analyses. Shapiro Wilk normality tests showed that most datasets were
190 not normally distributed. Therefore, nonparametric Wilcoxon-signed rank tests were conducted. The critical alpha
191 for all analyses was set at 0.05. Effect sizes were calculated from dividing the absolute standard test statistics by
192 the square root of the number of observations [28].

193

194 **Results**

195 One participant withdrew after the first trial for reasons not related to the study. Therefore, data analysis was
196 performed on eight participants (one female and seven males; age: 55 ± 15 years; height: 174 ± 5 cm; weight: 81
197 ± 11 kg; table 1). An equal number of participants had an amputation of the right or left lower limb. Four
198 participants' current prosthesis was passive, while the other half of the participants wore a quasi-passive device
199 (microprocessor-controlled). Years since amputation varied among participants (22 ± 14 years), but they were all
200 familiar with their current prosthesis for a minimum duration of three months.

201

202 **Table 1.** Participants' characteristics: demographic data, prosthetic components and normal walking speed.

Participant (gender)	Age (yrs)	Body weight (kg)	Body length (cm)	AMP side	Length stump (cm)	Suspension mechanism	Current prosthetic knee and ankle joint	Years since amputation	Speed (m.s ⁻¹) current	Speed (m.s ⁻¹) CLS- γ
1 (M)	65	72	172	L	28	Vacuum	Össur Total knee® Össur Flex walk®	41	0.83	0.83
2 (M)	34	76	178	R	36	Liner	Otto Bock C-leg® Otto Bock Taleo®	9	1.25	0.56
3 (M)	35	75	176	L	35	Vacuum	Össur Total Knee® Össur Variflex®	19	0.88	0.56
4 (M)	72	90	172	L	38	Strap	Otto Bock Genium® Otto Bock Taleo®	7	0.83	0.33
5 (M)	63	98	178	R	28	Vacuum	Össur Mauch® Össur Variflex®	29	0.44	0.33
6 (F)	55	83	165	R	30	Strap	Össur Total knee® Össur Flex walk®	34	0.61	0.44
7 (M)	56	90	179	L	35	Vacuum	Otto Bock C-leg® Otto Bock C-walk®	5	0.56	0.56
8 (M)	61	63	170	R	35	Liner	Otto Bock C-leg® Otto Bock C-walk®	30	0.83	0.56

210 All participants were indicated as Medicare Functional Classification Level K3 ambulators and had their current prosthesis for at
 211 least one month. Abbreviations: **AMP** amputated **CLS- γ** CYBERLEGS-gamma, **F** female, **L** left, **M** male, **R** right.

212

213 *Gait biomechanics*

214 Stride length significantly increased when walking with the CLS- γ compared to the current prosthesis ($17 \pm 10 \%$,
 215 $p = 0.012$; Table 2, Figure 3A). The increased stride length was due to a greater step length of the amputated leg
 216 ($22 \pm 20 \%$, $p = 0.035$; Table 2, Figure 3B). No significant difference in step length of the non-amputated leg was
 217 reported (Figure 3B). Step width did not significantly change while walking with the current and CLS- γ prosthesis.
 218 Coefficients of variation did not differ between both prostheses for stride length, step width, and step length of the
 219 amputated and non-amputated leg. The percentage duration of stance phases of the amputated and non-amputated
 220 leg did not vary between walking with the current and CLS- γ prosthesis. Additionally, swing phase did not differ
 221 between both prostheses. Maximum heel pressure of the amputated and non-amputated leg did not change while
 222 walking with the current compared to the CLS- γ prosthesis.

223

224 **Table 2.** Dependent variables are presented as mean and standard deviation, their corresponding p-value, absolute standard test
 225 value (Z) and effect size.

Variables	Current	CLS- γ	p-value	Z	Effect size	Variables	Current	CLS- γ	p-value	Z	Effect size
Stride length (cm)	84.75 (7.57)	99.38 (10.74)	0.012	2.52	0.63	Ventilation (L.min ⁻¹)	31.46 (7.83)	29.61 (7.33)	0.398	0.85	0.28
Step length AMP leg (cm)	41.38 (4.60)	50.63 (8.55)	0.035	2.10	0.53	Metabolic equivalents	4.15 (1.13)	3.86 (1.20)	0.271	1.10	0.28
Step length N-AMP leg (cm)	43.63 (6.63)	48.75 (7.96)	0.231	1.26	0.32	Net metabolic cost (mL.[m.kg ⁻¹] ⁻¹)	0.35 (0.13)	0.56 (0.16)	0.028	2.97	0.74
Step width (cm)	16.13 (5.00)	15.75 (3.06)	0.733	0.34	0.09	RPE SCT	2.00 (0.76)	2.50 (1.07)	0.334	0.97	0.42

CV stride length	0.06	0.03	0.075	1.78	0.45	RPE TUG	1.90 (1.00)	1.75 (0.46)	0.739	0.33	226 0.08
CV step width	0.13	0.09	0.235	1.19	0.30	RPE STS	3.00 (0.93)	2.63 (1.19)	0.180	1.34	227 0.34
CV step length AMP leg	0.07	0.06	0.443	0.77	0.19	RPE 6MWT	3.25 (1.04)	3.38 (1.30)	0.480	0.71	228 0.18
CV step length N-AMP leg	0.09	0.05	0.674	0.41	0.11	VAS SCT	2.09 (1.41)	3.48 (2.00)	0.093	1.68	229 0.29
Stance phase AMP leg (%)	63.71 (3.19)	60.81 (9.00)	0.327	0.98	0.25	VAS TUG	2.00 (2.02)	2.03 (1.90)	0.672	0.42	230
Stance phase N-AMP leg (%)	73.76 (4.08)	76.88 (7.74)	0.263	1.12	0.28	VAS STS	3.73 (2.15)	3.34 (2.08)	0.553	0.57	231
Swing phase AMP leg (%)	35.26 (5.16)	34.89 (10.50)	0.327	0.98	0.25	VAS 6MWT	3.48 (3.04)	3.63 (2.36)	0.735	0.34	232
Swing phase N-AMP leg (%)	27.26 (2.04)	27.43 (10.10)	0.207	1.26	0.32	EQ-5D	84.38 (9.43)	87.89 (9.05)	0.059	1.89	233
Heel pressure AMP leg (N.cm ²)	18.99 (4.75)	24.19 (5.41)	0.063	1.86	0.46	Speed (m.s ⁻¹)	0.77 (0.25)	0.45 (0.12)	0.018	2.37	234 0.59
Heel pressure N-AMP leg (N.cm ²)	19.68 (6.17)	22.04 (3.91)	0.575	0.56	0.14	Cadence (steps.min ⁻¹)	71 (13)	60 (9)	0.012	2.52	235
Heart rate SCT (bpm)	102 (18)	106 (17)	0.611	0.51	0.13	Reaction time (msec)	337 (56)	398 (65)	0.012	2.52	236 0.63
Heart rate TUG (bpm)	100 (16)	100 (17)	0.533	0.59	0.15	Duration SCT (sec)	16 (8)	36 (13)	0.012	2.52	237 0.63
Heart rate STS (bpm)	108 (18)	104 (17)	0.204	1.27	0.32	Duration TUG (sec)	15 (6)	20 (6)	0.012	2.52	238 0.63
Heart rate 6MWT (bpm)	120 (25)	113 (18)	0.893	0.41	0.10	Number of stands	8.00 (3.00)	7.80 (3.28)	0.671	0.43	239 0.11
Oxygen consumption (mL.[min.kg] ⁻¹)	14.15 (4.01)	14.10 (3.80)	0.499	0.68	0.17						240

241 Abbreviations: **AMP** amputated, **CLS- γ** CYBERLEGS-gamma, **CV** coefficient of variation, **EQ-5D** EuroQol-5D, **N-AMP** non-
242 amputated, **RPE** rating of perceived exertion, **SCT** stair climbing test, **STS** sit to stand test, **TUG** timed-up & go test, **VAS** visual
243 analogue scale, **6MWT** six-minute walk test.

244

245 [Insert Figure 3]

246 **Figure 3.** Mean and standard deviation for stride (A) and- step length (B) are presented while walking with the
247 current compared to the CYBERLEGS-gamma (CLS- γ) prosthesis. Abbreviations: **AMP** amputated leg, **N-AMP**
248 non-amputated leg.

249

250 *Physiological measures*

251 Heart rate at the end of each task did not change when wearing the current compared to the CLS- γ prosthesis. The
252 amount of oxygen consumption, ventilation and metabolic equivalents did not vary between walking with both
253 prostheses. However, the net metabolic cost of transport significantly increased 61 ± 47 % when wearing the CLS-
254 γ compared to the current prosthesis during the 6MWT ($p = 0.028$; Table 2, Figure 4).

255

256 [Insert Figure 4]

257 **Figure 4.** Representation of the net metabolic cost per meter during the six-minute treadmill walk test with the
258 current compared to the CYBERLEGs-gamma (CLs- γ) prosthesis.

259

260 *Subjective workload*

261 No differences in session rating of perceived exertion and the visual analogue scale for fatigue were reported
262 during the different tests between the current and CLs- γ prosthesis. The self-reported scores on the EuroQol-5D
263 did not significantly change between both prostheses.

264

265 *Task performance*

266 Figure 5 shows that the normal walking speed was significantly lower with the CLs- γ compared to the current
267 prosthesis (42 ± 21 % decrease, $p = 0.018$; Table 2). Cadence significantly decreased 12 ± 8 % while walking with
268 the CLs- γ compared to the current prosthesis ($p = 0.012$; Table 2). It took participants significantly longer to
269 respond to the stimulus on the psychomotor vigilance task while walking with the CLs- γ compared to the current
270 prosthesis (19 ± 12 % increase, $p = 0.012$; Table 2). Participants significantly needed more time to complete the
271 SCT and TUG with the CLs- γ compared to the current prosthesis (125 ± 75 % increase, $p = 0.012$ and 33 ± 21 %
272 increase, $p = 0.012$, respectively; Table 2). Number of stands during the STS did not differ between both
273 prostheses.

274

275 [Insert Figure 5]

276 **Figure 5.** Individual (1-8) and group average (MEAN) normal walking speed (mean and standard deviation) with
277 the current (\diamond) versus the CYBERLEGs-gamma (CLs- γ) (\square) prosthesis are displayed.

278

279 **Discussion**

280 The aim of this study was to investigate the effectiveness of a novel prosthesis, consisting of powered ankle and
281 knee joints, during daily activities. The main finding was that the CLs- γ prosthesis reduced walking symmetry,
282 and physical and cognitive effort during daily activities compared to current devices. Worth mentioning is that
283 although performance outcome measures were not improved, participants wearing the novel prosthesis were able
284 to conduct the step-over-step during stair climbing instead of the step-by-step strategy with their current prosthesis.

285

286 Little is known about powered ankle and knee joints incorporated in one prosthetic device. The approach of
287 configuring both joints working together is a major challenge, which is reflected in the few studies that have
288 already been conducted with other prototypes [29–32]. Previous research did not report improved functioning with
289 the synchronized joints and the impedance or kinematic control-based mechanism. The CLs- γ prosthesis differs
290 from previous prototypes since the finite state controller relies on pressure-sensitive insoles in the shoes and inertial
291 motor units attached to the trunk and lower limbs. These novel mechanisms of the CLs- γ prosthesis showed to
292 partially restore the capacity to exert some tasks that could not be performed with their current prosthesis. The
293 most notable change was observed during stair ascending and descending where participants conducted the step-
294 over-step instead of the step-by-step strategy. This reciprocal stair ambulation shows the possible functional
295 capacity of motorized lower limb prostheses. Moreover, we assume that more able-bodied functioning would
296 reduce the risk of overuse injuries and secondary complications.

297
298 Although stride length significantly increased with the novel prosthesis, the greater stride length did not approach
299 values of able-bodied walking (CLs- γ : 99 ± 11 cm vs. able-bodied: 157 ± 5 cm) [33]. Stride length mainly increased
300 as a result from a larger step length of the amputated leg. This exacerbated the asymmetrical walking pattern and
301 did not contribute to a higher symmetry between the amputated and non-amputated leg. Also, gait variability of
302 stride length, a measure for gait symmetry, did not significantly differ between the the CLs- γ and current
303 prosthesis, an asymmetrical walking pattern remains present [26].

304
305 Walking with the CLs- γ prosthesis significantly increased oxygen consumption. A weight reduction of the next
306 prototype would most likely decrease the net metabolic cost since it directly influences oxygen uptake. Second,
307 the control system and interface need further development, which apparently affected gait and walking efficiency.
308 This was recently observed in a study wherein the authors outlined that the controller parameters (passive and
309 active loops) could influence the metabolic cost [34]. For example, torque-angle or torque-time optimization would
310 benefit biological measures [35]. This obviously highlights the need of developing more sophisticated and user-
311 specific controllers in future prototype development.

312
313 Some studies investigated the reaction time on an auditive stimulus during stepping and standing posture in people
314 with a TFA [36]. In the current study, a longer reaction time on a visual stimulus was observed during treadmill
315 walking when wearing the CLs- γ prosthesis. Therefore, to reduce the cognitive effort during gait, and to cope with

316 the increased physiological demand, participants' normal walking speed was slower with the CLs- γ compared to
317 the current prosthesis. This means that walking with the novel device interferes with the individual's ability to
318 focus on other tasks [6]. We suppose it may be possible that the increased cognitive demand was driven by lack
319 of adaptation period to the novel device. The duration of an adaptation period varies among different studies, i.e.
320 between a few hours, up to three weeks and even three months [37]. One study reported that after a few hours of
321 adaptation all participants with a TFA were already able to properly perform daily activities with clinically relevant
322 results for further development of the prototype [30]. Therefore, in the current study we implemented three
323 adaptation sessions of in total approximately three hours to prepare them for the experimental trials. We assume it
324 may be possible that the adaption was enough to gather relevant outcomes for the development process, but
325 apparently not sufficient to obtain an automatized gait pattern, and thus participants were unable to conduct an
326 additional task.

327

328 A limitation of this study is that the 6MWT was performed on a treadmill, while – according to the standardized
329 procedure – it should be conducted in a hallway [16]. It is been proven though that the treadmill 6MWT showed a
330 high test-retest reliability [23]. The treadmill 6MWT was chosen for safety of the participants, since the CLs- γ
331 prosthesis reached technology readiness level 5, whereas the hallway 6MWT is recommended for more developed
332 prototypes. We also did not record kinematics during walking and the results are only relevant for individuals with
333 a TFA, classified as MFC level K3. A bigger sample size (average 10 [9]) is also recommended in future research
334 since the current study demonstrated for several parameters (maximum heel pressure, step width, stride length,
335 swing phase and step length of the non-amputated side and heart rate during STS) moderate effect. In a next step,
336 it is advised to include an adaptation period of three months at a higher technology readiness level (≥ 6 , i.e. 'model
337 or prototype demonstration in a relevant environment') to map long-term adaptation of the novel prosthesis [11].

338

339 **Conclusion**

340 The CYBERLEGS-gamma prosthesis consists of powered ankle and knee joints meant to replace a human ankle-
341 knee system for various tasks including walking, sit to stand, and stair climbing. A higher physical and cognitive
342 effort were required during walking with the novel prosthesis compared to current devices. Overall, our hypotheses
343 were rejected, meaning that technological advancements in lower limb prosthetics are required to enable
344 synchronized and powered ankle and knee joints. Although performance outcome measures were not improved,

345 participants wearing the novel prosthesis better simulated able-bodied stair ambulation. All participants were able
346 to conduct stairs with the step-over-step instead of the step-by-step strategy.

347

348 **List of Abbreviations**

349 **AMP** amputated

350 **CLs- γ** CYBERLEGS-gamma

351 **CV** coefficient of variation

352 **EQ-5D** EuroQol-5D

353 **F** female

354 **L** left

355 **M** male

356 **N-AMP** non-amputated leg

357 **R** right

358 **RPE** rating of perceived exertion

359 **SCT** stair climbing test

360 **STS** sit to stand test

361 **TFA** transfemoral amputation

362 **TUG** timed-up & go test

363 **VAS** visual analogue scale

364 **6MWT** six-minute treadmill walk test

365

366 **Declarations**

367 *Ethics approval and consent to participate*

368 The study was approved by the institutional medical ethics committee of UZ Brussel and Vrije Universiteit Brussel
369 (Belgium, B.U.N. 143201732970) and the Federal Agency for Medicines and Health Products (FAMHP reference
370 number: 80M0725). All participants were provided written and verbal information about the experimental
371 protocol, potential risks and benefits before giving informed consent to participate in the study.

372

373 *Consent for publication*

374 Consent for publication of results is obtained from all participants.

375

376 *Availability of data and materials*

377 All data generated or analysed during this study are included in this published article.

378

379 *Competing interests*

380 The authors declare that they have no competing interests.

381

382 *Funding*

383 This research received funding by ‘the CYBERnetic LowEr-Limb CoGnitive Ortho-prosthesis Plus project
384 (CYBERLEGs++) [H2020-ICT-2015 Grant Agreement #731931].

385

386 *Authors' contributions*

387 JGH substantially contributed to the conception of the methods used, participant recruitment, data acquisition,
388 interpretation and analysis, and writing the manuscript. JGE and LF made substantial contributions to the
389 conception of the methods used, participant recruitment, and data acquisition, interpretation and analysis. SDB,
390 RG, KDP and BR made substantial contributions to conception, design and writing the manuscript. SC, NV, RM
391 and DL were involved in the conception of the methods used, data interpretation and writing the manuscript. All
392 authors read and approved the final manuscript.

393

394 *Acknowledgements*

395 We would like to thank Patrick Van De Vaerd and colleagues of V!GO (9230 Wetteren, Belgium) for their
396 assistance during the experimental trials. We would also like to thank the company V!GO for providing their
397 laboratory.

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