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A new scheme for calculating soil thermal diffusivity

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Declarations

Conflict of interest The authors declare that they have no competing interest.

23

Abstract

24 Land-atmosphere interaction is one of the important causes of climate change. The accurate
25 characterization of physical mechanism of the soil layer can help us better understand the land-
26 atmosphere interaction. As one of the important thermal properties of soil, soil thermal
27 diffusivity is an important parameter reflecting soil thermal conductivity and a necessary
28 condition for simulating soil thermodynamic environment. Based on the comparison of several
29 methods for calculating soil thermal diffusivity (amplitude method, phase method, logarithmic
30 method, arctangent method, Laplace method and numerical methods), this paper develops a new
31 soil thermal diffusivity model (Thermal conduction-convection method based on Fourier series
32 boundary condition for calculating soil thermal diffusivity, TCCMF) and compares the results of
33 the new model with other methods. The results show that: (1) The accuracy of the results
34 obtained by the amplitude method, phase method, logarithmic method, and arctangent method is
35 not high enough; the Laplace method can better solve the effects of extreme weather or non-
36 periodic changes in soil temperature. (2) When the numerical methods are used to solve the
37 thermal conduction equation, the Crank-Nicholson-Sch format is unconditionally stable, the data
38 utilization rate is higher, the obtained soil thermal diffusivity is less discrete, and the result is
39 more accurate. (3) The new model (TCCMF) uses the Fourier series method, which is easy to
40 calculate, and has more complete physical process and more flexible precision control. The
41 simulation results of soil temperature using this method show that this method (TCCMF) has
42 better simulation accuracy, indicating that it has potential value in simulating soil
43 thermodynamic characteristics and land-atmosphere interaction.

44 **Keywords** Land-atmosphere interaction · land surface process · Soil temperature · Soil thermal
45 diffusivity · Thermal conductivity-convection equation

46 1 Introduction

47 The interaction of earth sphere layers is a prominent feature of contemporary earth science
48 thought. Climate change is the result of the interaction of earth sphere layers. Surface processes
49 are various physical, chemical, and biological processes that occur at the earth-air interface, and
50 are the embodiment of the interaction between the pedosphere, hydrosphere, atmosphere, and
51 biosphere. Humans live on land, and the land-atmosphere interaction (mass and energy

52 exchange) profoundly affects the living environment of human beings. A lot of studies have been
53 done on land-atmosphere interaction and its climate effects. For example, the land-atmosphere
54 interaction increases the climate variability in Central and Eastern Europe, and the increase in
55 summer temperature is also due to the feedback effect between the surface and the atmosphere
56 (Seneviratne et al. 2006). The Global Energy and Water Cycle Experiment (GEWEX)
57 Continental –Scale International Project (GCIP) improved the accuracy and sophistication of
58 land-surface schemes in many national models, defined water budgets for the central United
59 States and provided a new understanding of dynamics of regional energy and water budgets
60 (Lawford 1999). The First International Satellite Land Surface Climatology Project (ISLSCP)
61 studied surface forcing of planetary boundary layer circulations, surface flux modeling-
62 parameterization–retrieval methods, biotic effects on boundary layer processes, remote sensing
63 of surface properties, and so on (Smith 1998; Williams et al. 2019). NOPEX (a Northern
64 Hemisphere Climate Processes Land Surface Experiment) pointed out the importance of the
65 boreal forests and studied surface-atmosphere interactions in forest-dominated landscapes in
66 northern Europe (Halldin et al. 1998). Heihe River Basin Field Experiment (HEIFE) pointed out
67 that the land-atmosphere interaction is realized through the exchange of energy and mass on the
68 earth's surface, the exchange of mass and energy between the land surface and atmosphere is
69 realized through the planetary boundary layer process (Hu and Gao 1994; Hu et al. 1994). Soil
70 layers are important in land-atmosphere interactions. The mass and energy exchange between
71 land and atmosphere is realized through the soil layer. The understanding of the physical and
72 chemical properties of the soil layer directly determines our grasp of the land-atmosphere
73 interaction. Due to the large spatial heterogeneity of soils, we still have insufficient
74 understanding of the spatial heterogeneity of soils and their temporal changes. Thermal
75 properties are one of the important properties of soils, which control the transfer and storage of
76 heat in soils. Soil thermal diffusivity is an important parameter to characterize soil thermal
77 properties, it represents the propagation speed of temperature waves in soil (Zhang et al. 2011).
78 Together with the soil temperature gradient, it also controls the magnitude of soil heat flow.
79 Therefore, the accurate inversion of soil thermal diffusivity is of great significance for
80 understanding soil thermodynamic-dynamic processes and land-atmosphere interactions.

81 The soil thermal diffusivity is usually defined as $k = \lambda/C_g$, which is determined by the
82 volumetric heat capacity of the soil C_g (unit: $J \cdot cm^{-3} \cdot K^{-1}$) and the soil thermal conductivity λ

83 (unit: $W \cdot m^{-1} \cdot K^{-1}$). It is difficult to directly observe the soil thermal diffusivity, so it is
84 generally obtained by inversion. The thermal diffusivity can be determined based on the
85 observed soil temperature in a variety of ways, most of which are based on the assumption that
86 soil is a semiunbounded medium with a constant thermal diffusivity and that the upper thermal
87 boundary can be expressed by a harmonic function (Li et al. 2015; Zheng and Liu 2013). In
88 terms of the thermal conduction equation for soil temperature (SCM), the common calculation
89 methods include the amplitude method, phase method, arctangent method, logarithmic method,
90 numerical method, harmonic method, Laplace method, and modified Laplace method
91 (Bhumralkar 1975). The amplitude method, phase method, arctangent method, logarithm
92 method, and harmonic method assume that the soil temperature at the boundary is in the form of
93 a sine function or Fourier series. Evaluation of these methods shows that the Fourier series is the
94 most reliable one. For the non-periodic soil temperature, the boundary conditions of the soil
95 temperature obtained by the Laplace method and the improved Laplace method are closer to the
96 real soil thermal conduction process, but the two methods are very complicated in calculation
97 (Liu et al. 2014).

98 There are three ways of heat transfer, namely conduction, convection and radiation. Under
99 actual soil conditions, the vertical water vapor flux will also affect the soil temperature through
100 convection, so the thermal conduction-convection equation (SCCM) will make the calculation
101 results more accurate. Studies have shown that, compared with the thermal conduction equation
102 (SCM), the difference between the soil thermal diffusivity calculated using the thermal
103 conduction-convection equation (SCCM) and the measured one is smaller (Goto et al. 2005;
104 Kane et al. 2001). Fan and Tang (1994) derived the expression of the thermal conduction-
105 convection equation, solved the soil thermal diffusivity and heat flux according to its physical
106 mechanism, and analyzed the relationship between heat flux and earthquake. Gao et al. (2005)
107 solved the analytical solution of the thermal conduction-convection equation by mathematical
108 methods, and obtained the same expression as Fan and Tang (1994). However, the previous
109 scholars assumed that the soil temperature at the boundary is a sine function when doing the
110 derivation, which may not be accurate enough in the process of describing the soil temperature
111 and solving the soil thermal diffusivity.

112 Since the 20th century, scholars have proposed many methods for calculating the thermal
113 diffusivity of soil. Whether based on SCMs, SCCMs, or different soil thermodynamic properties,

114 these methods have their own applicable conditions, advantages and disadvantages. Previous
115 work led to important contributions, although the horizontal comparison of various methods was
116 relatively insufficient. Therefore, the objectives of the present study were to (1) transversely
117 compare the results of soil thermal diffusivity obtained from different boundary conditions under
118 the SCM; (2) derive a method of solving the SCCM under the condition of a Fourier boundary
119 and obtain the thermal diffusivity; (3) compare the measured soil temperature with the soil
120 temperature obtained by solving the SCCM under the Fourier boundary condition. The research
121 not only provides a more accurate simulation of soil temperature and a useful tool for calculating
122 soil thermal diffusivity, but also partially analyzes the thermal fluctuations in the soil. It helps to
123 understand the changes in soil thermal properties and thermal movement, as well as the land-
124 atmosphere interaction under the background of climate change.

125

126 **2 Field experiments**

127 The observation site is located in Golmud. Golmud is composed of two unconnected parts: the
128 central and southern parts of the Qaidam Basin and Tanggula Mountain. The average
129 temperature in Golmud is 5.3 °C, the precipitation is 42.1 mm, the relative humidity is 32%, the
130 cumulative number of sunshine events is 3096.3 h, and the accumulated annual evaporation is
131 2504.1 mm. It belongs to the continental plateau climate and presents less rain, wind and
132 drought. The annual average sunshine hours in the region are 3200~3600 h, and the annual total
133 solar radiation is 6618~7356 MJ/m². It is the second largest high-value solar radiation area in
134 China after the Qinghai-Tibet Plateau (Yang et al. 2017). The soil temperature used in this study
135 was recorded every 10 minutes by CR1000 produced by Campbell Corporation of the United
136 States at 6 depth layers of 5 cm, 10 cm, 20 cm, 40 cm, 80 cm, and 180 cm for the period from
137 October 2012 to July 2013. The data were quality controlled (Gao et al. 2016).

138 3 Method

139 3.1 Thermal conduction equation for soil temperature (SCM)

140 The volumetric heat capacity C_g ($J \cdot cm^{-3} \cdot K^{-1}$) and the soil thermal conductivity λ ($W \cdot$
141 $m^{-1} \cdot K^{-1}$) are assumed to remain consistent with depth based on the classical thermal diffusion
142 equation in a one-dimensional semiunbounded medium:

$$143 \quad \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial z^2} \quad (1)$$

144 where $k = \lambda/C_g$ (unit: m^2s) is the thermal diffusivity.

145 The boundary condition at z_1 is given by the following equation (Van Wijk and de Vries,
146 1963):

$$147 \quad T|_{z=z_1} = \bar{T}_1 + A_1 \sin(\omega t - \Phi_1), t \geq 0 \quad (2)$$

148 where \bar{T}_1 ($^{\circ}C$) is the average value of soil temperature at depth z_1 , A_1 ($^{\circ}C$) is the amplitude,
149 $\omega=2\pi/p$ (rad/s) is the daily change period, p is the period of the change, and Φ_1 is the initial soil
150 temperature (primary phase) (rad) at depth z_1 , which is obtained by least squares fitting.

151 According to Eq. (1) and Eq. (2), the soil temperature at depth z_2 is expressed as follows:

$$152 \quad T_{z=z_2} = \bar{T}_2 + A_1 \exp[(z_1 - z_2)\alpha] \sin[\omega t - \Phi_1 - (z_2 - z_1)\alpha] \quad (3)$$

153 where $\alpha = \sqrt{\omega/2k}$. The amplitude A_2 and initial phase Φ_2 at depth z_2 are as follows:

$$154 \quad A_2 = A_1 \exp[-(z_2 - z_1)\alpha]$$

$$155 \quad \Phi_2 = \Phi_1 + (z_2 - z_1)\alpha$$

156 According to Eq. (1) to Eq. (3), the thermal diffusivity k can be expressed with the amplitude
157 and phase:

$$158 \quad k_p = (z_1 - z_2)^2 \omega / [2(\Phi_1 - \Phi_2)^2] \quad (4)$$

$$159 \quad k_A = (z_1 - z_2)^2 \omega / [2\ln^2(A_1/A_2)] \quad (5)$$

160 3.1.1 Arctangent method and logarithmic method

161 Soil temperatures can be simulated with a series of sinusoidal terms. Observations of soil
162 temperature at a certain depth can be expressed in Fourier series:

$$163 \quad T(t) = \bar{T} \cdot \sum_{n=1}^2 [A_n \cos(n\omega t) + B_n \sin(n\omega t)] \quad (6)$$

164 where \bar{T} (°C) is the average value of soil temperature and A_n and B_n (°C) are amplitudes. Eight
 165 soil temperature observations were performed at two depths per day. The phase method is shown
 166 in Eq. (4):

$$167 \quad k = \omega(z_1 - z_2)^2 \cdot \{2\{\arctan$$

$$168 \quad \left[\frac{(T_1(z_1) - T_3(z_1))(T_2(z_2) - T_4(z_2)) - (T_2(z_1) - T_4(z_1))(T_1(z_2) - T_3(z_2))}{(T_1(z_1) - T_3(z_1))(T_1(z_2) - T_3(z_2)) + (T_2(z_2) - T_4(z_1))(T_2(z_2) - T_4(z_2))} \right]\}^2\}^{-1} \quad (7)$$

169 where $T_1(z_1)$, $T_2(z_1)$, $T_3(z_1)$, $T_4(z_1)$ and $T_1(z_2)$, $T_2(z_2)$, $T_3(z_2)$, $T_4(z_2)$ are four soil
 170 temperature observations at z_1 and z_2 .

171 The amplitude method is shown in Eq. (5):

$$172 \quad k = \frac{\omega}{2} \times \frac{z_2 - z_1}{\left\{ \ln \left[\frac{(T_1(z_1) - T_3(z_1))^2 + (T_2(z_1) - T_4(z_1))^2}{((T_1(z_2) - T_3(z_2)))^2 + (T_2(z_2) - T_4(z_2))^2)} \right] \right\}^2} \quad (8)$$

173 Eq. (7) is an arctangent method, and Eq. (8) is a logarithmic method, which was developed
 174 early without automatic recording equipment. Compared with the phase method in Eq. (4) and
 175 amplitude method in Eq. (5), the arctangent method and the logarithmic method do not need to
 176 fit the amplitude and phase; thus, they are simpler and more convenient to use and have the
 177 ability to reflect the possible nonsinusoidal changes (Liu et al.,1991). However, the temperature
 178 sampling data at intervals of 6 h will inevitably lead to the absence of short-period signals. When
 179 the heat transfer model is established, there are no high-order harmonic components with
 180 boundary conditions, which leads to further errors in the simulation results (Liu et al. 2014).

181 3.1.2 Laplace transformation based method (LTM)

182 In Section (3.1.1), the prerequisite for the four methods is to assume a stable cyclical change
 183 in soil temperature. In actual circumstances, if there is a sudden change in weather conditions,
 184 such as heavy precipitation, cold waves, blizzards, etc., then the stability cycle will fail.
 185 Therefore, the model with stable period change as the boundary condition will not be applicable
 186 when simulating soil temperature change and obtaining thermal diffusivity (Liu et al. 2014). To
 187 better simulate the nonperiodic changes in soil temperature and make the boundary conditions of
 188 the model closer to the soil heat transfer process, the Laplace transform is a good choice.

189 The solution of Eq. (1) with initial and boundary conditions is given as follows:

$$190 \quad T(z, 0) = T_0 \quad (9a)$$

$$191 \quad T(0, t) = \Phi(t), t > 0 \quad (9b)$$

192 Then, the Laplace transformation can be performed (Carslaw and Jaeger, 1959):

193
$$T(z,t) = T_0 + \frac{z}{2\sqrt{\pi k}} \int_0^t \Phi(\tau) \frac{\exp\left(\frac{-z^2}{4k(t-\tau)}\right)}{(t-\tau)^{3/2}} d\tau \quad (10)$$

194 Eq. (10) applies to a semi-infinite medium whose upper boundary condition is given by $\Phi(t)$, a
195 continuous function of time. It is an impulse response equation that is useful for sudden changes
196 in temperature input signals (such as in rainy or cold front transit). A limitation of using this
197 equation is that the initial temperature profile must be uniform. The soil thermal diffusivity can
198 be obtained by fitting Eq. (10) (de Silans et al. 1996).

199 3.1.3 Numerical method

200 For homogeneous soils, the heat transfer equation can be approximated by a difference
201 equation. Commonly used differential formats are as follows (Liu et al. 1991):

202 (1) Dufeat-Frankel-Sch (format 1)

203
$$\frac{T_j^{n+1} - T_j^n}{2} = \frac{k\Delta t}{\Delta z^2} (T_{j+1}^n + T_{j-1}^n - T_j^{n+1} - T_j^{n-1}) \quad (11)$$

204 This format is stable.

205 (2) Crank-Nicholson-Sch (format 2)

206
$$T_j^{n+1} - T_j^n = \frac{k\Delta t}{2\Delta z^2} [(T_{j+1}^{n+1} - 2T_j^{n+1} + T_{j-1}^{n+1}) + (T_{j+1}^n - 2T_j^n + T_{j-1}^n)] \quad (12)$$

207 This format is unconditionally stable. In Eq. (11)-(12), j represents a spatial interval and n
208 represents a time interval.

209 3.2 Thermal conduction-convection equation for soil temperature (SCCM)

210 Eq. (1) assumes that the soil is vertically uniform. However, some scholars (Gao et al. 2003)
211 believe that the difference between day and night temperature and solar radiation will trigger the
212 vertical movement of soil water, which affects the temperature distribution in soil. To reflect the
213 influence of this part, thermal conduction was combined with convection to establish a soil
214 thermal conduction-convection model:

215
$$\frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial z^2} - \frac{C_w}{C_g} w\theta \frac{\partial T}{\partial z} \quad (13)$$

216 where w (m/s) is the liquid flow rate (downward positive), θ is the volumetric water content of
 217 the soil, and C_W ($J^\circ C^{-1}m^{-3}$) is the specific heat capacity of the water. Assume that these
 218 quantities are independent of z and $-\frac{C_W}{C_g}w\theta$ is the liquid water flux density. Let $W =$
 219 $-\frac{C_W}{C_g}w\theta \frac{\partial T}{\partial z}$, then:

$$220 \quad \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial z^2} + W \frac{\partial T}{\partial z} \quad (14)$$

221 *3.2.1 Boundary condition as a superposition of a sine wave on the constant temperature field*

222 Given the following boundary condition:

$$223 \quad T|_{z=0} = \bar{T} + A \sin \omega t \quad (t \geq 0)$$

224 The solution of Eq. (14) is as follows:

$$225 \quad T(z, t) = T_0 + A \exp\left[\left(\frac{-W - \alpha}{2k}\right)z\right] \sin\left(\omega t - \Phi_1 - \frac{\beta}{2k}z\right) \quad (15)$$

226 where

$$227 \quad \alpha = \sqrt{\frac{W^2 + \sqrt{W^4 + 16k^2\omega^2}}{2}}, \quad \beta = \frac{2\sqrt{2}k\omega}{\sqrt{W^2 + \sqrt{W^4 + 16k^2\omega^2}}} \quad (16)$$

228 Therefore, the soil temperature (T) at depth z_2 can be calculated using the following equation:

$$229 \quad T_{z=z_2} = \bar{T}_2 + A_1 \exp[(z_1 - z_2)\alpha M] \sin[\omega t - \Phi_1 - (z_2 - z_1)\alpha N] \quad (17)$$

230 In Eq. (17), M and N can be expressed as follows:

$$231 \quad M = \frac{\alpha}{\omega} \left\{ W + \frac{1}{\sqrt{2}} \left[W^2 + \left(W^4 + \frac{4\omega^4}{\alpha^4} \right)^{1/2} \right]^{1/2} \right\}$$

$$232 \quad N = \sqrt{2} \frac{\omega}{\alpha} \left[W^2 + \left(W^4 + \frac{4\omega^4}{\alpha^4} \right)^{1/2} \right]^{-1/2}$$

233 Assuming that $z_1 < z_2$, $A_1 > A_2$, $\Phi_1 < \Phi_2$, the following equations are derived (Gao, 2005):

$$234 \quad k = -\frac{(z_2 - z_1)^2 \omega \ln(A_2/A_1)}{(\Phi_2 - \Phi_1)[(\Phi_2 - \Phi_1)^2 + \ln^2(A_2/A_1)]} \quad (18)$$

$$235 \quad W = \frac{\omega(z_2 - z_1)}{\Phi_2 - \Phi_1} \left[\frac{-(\Phi_2 - \Phi_1)^2 + \ln^2(A_2/A_1)}{(\Phi_2 - \Phi_1)^2 + \ln^2(A_2/A_1)} \right] = \frac{\omega(z_2 - z_1)}{\Phi_2 - \Phi_1} \left[\frac{2\ln^2(A_2/A_1)}{(\Phi_2 - \Phi_1)^2 + \ln^2(A_2/A_1)} - 1 \right] \quad (19)$$

236 The above is the thermal conduction-convection method.

237 3.2.2 Boundary condition as the form of Fourier series

238 Hu et al. (2015) derived the thermal conduction-convection equation for the Fourier series
 239 boundary of soil temperature (FCCM). Given the following boundary condition:

$$240 \quad T(0, t) = T_0 + \sum_{n=1}^N A_n \sin(n\omega t - \Phi_n), n = 1, 2, \dots, N \quad (20)$$

241 where n is the number of harmonics.

242 The solution of Eq. (15) is as follows:

$$243 \quad T(z, t) = T_0 + \sum_{n=1}^N A_n \times \exp\left[-\frac{W}{2k} - \frac{\sqrt{2}}{4k} X_n z\right] \sin\left(n\omega t - \frac{\sqrt{2}\omega}{nX_n} z\right) \quad (21)$$

244 where

$$245 \quad \alpha_n = \sqrt{\frac{W_n^2 + \sqrt{W_n^4 + 16k_n^2 \omega^2}}{2}}, \quad \beta_n = \frac{2\sqrt{2}k_n \omega}{\sqrt{W_n^2 + \sqrt{W_n^4 + 16k_n^2 \omega^2}}}$$

246 Therefore, the soil temperature (T) at depth z_2 can be calculated using the following equation:

$$247 \quad T_{z=z_2} = \bar{T}_2 + \sum_{n=1}^N A_n \exp\left[\left(\frac{-W - \alpha_n}{2k}\right)(z_2 - z_1)\right] \times \sin\left[n\omega t - \Phi_n - (z_2 - z_1) \frac{\beta_n}{2k}\right] \quad (22)$$

248 3.2.3 Soil thermal diffusivity under Fourier boundary conditions(k_n , TCCMF)

249 The detailed derivation of k_n is in the appendix.

$$250 \quad W_n = \frac{\omega(z_1 - z_2)}{n(\Phi_n^1 - \Phi_n^2)} \left[\frac{2\ln^2\left(\frac{A_n^1}{A_n^2}\right)}{n^2(\Phi_n^1 - \Phi_n^2)^2 + \ln^2\left(\frac{A_n^1}{A_n^2}\right)} - 1 \right] \quad (23)$$

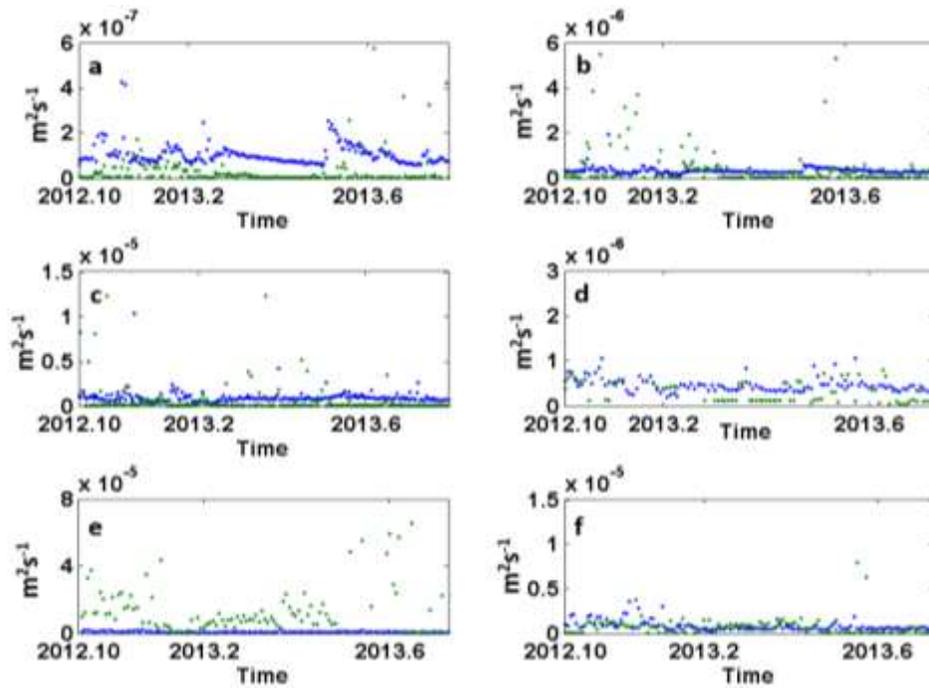
$$251 \quad k_n = -\frac{(z_1 - z_2)^2 \omega \ln\left(\frac{A_n^1}{A_n^2}\right)}{n(\Phi_n^1 - \Phi_n^2) \left[n^2(\Phi_n^1 - \Phi_n^2)^2 + \ln^2\left(\frac{A_n^1}{A_n^2}\right) \right]} \quad (24)$$

252 **4 Result**

253 4.1 Comparison of five methods for the thermal conduction equation in the shallow soil layer

254 The soil thermal diffusivities at six depths (5-10 cm, 5-20 cm, 5-40 cm, 10-20 cm, 10-40 cm,
 255 and 20-40 cm) in the shallow soil of the photovoltaic power station were calculated by the

256 amplitude method, phase method, arctangent method, logarithm method and Laplace method.
257 The boundary condition of the amplitude method and the phase method is that a constant sine
258 wave is superimposed on the constant temperature field. Selecting the parts of the fitting result
259 whose judgment coefficients are greater than 0.8 (Wang et al. 2019), Fig. 1c, e and f show that
260 there are fewer data with coefficients of determination greater than 0.8 at 40 cm and the fitting
261 result is not good. Fig. 1 shows that the results obtained by the amplitude method at the four
262 levels of 5-10 cm, 5-20 cm, 5-40 cm, and 10-20 cm are generally larger than that of the phase
263 method. Compared with the amplitude method, the phase method can partially reflect the
264 extreme values of the thermal diffusivity. Fig. 2 shows that the arctangent method is derived
265 from the phase method. In addition, 0, 8, 16 and 24 (Beijing time) points are selected every day
266 and the obtained soil thermal diffusivity results are more uniform. Compared with the phase
267 method, it does not reflect some extreme conditions. The logarithm method is derived from the
268 formula of the amplitude method. The time of selection was based on 0, 8, 16 and 24 (Beijing
269 time) points. The results obtained by the logarithm method are similar to those obtained by the
270 amplitude method. However, some extreme values reflected by the amplitude method are not
271 reflected in the logarithmic method. At depths of 5-40 cm, the soil thermal diffusivity obtained
272 by the amplitude method, the phase method, the arctangent method and the logarithm method
273 have large differences. The Laplace method does not have a formula for the established
274 boundary conditions. Fig. 3 shows that the method is effective in reflecting the influence of
275 some extreme conditions and nonperiodic weather changes on the thermal diffusivity. The above
276 results are basically consistent with the results obtained by Liu et al. (1991). The amplitude
277 method and phase method are based on a single temperature sine wave, which is used to describe
278 the general soil, and the accuracy is not high enough, especially when there are multiple extreme
279 temperature values. The arctangent method and logarithmic method require less measured data
280 and present more convenient data acquisition, which is one of the main reasons for their lack of
281 precision, and they also inherit some of the disadvantages of the amplitude method and phase
282 method. The Laplace method has no fixed boundary condition function, and it has outstanding
283 advantages in dealing with actual weather conditions, such as sudden weather, heavy
284 precipitation, cold waves, blizzards and other nonperiodic weather changes.

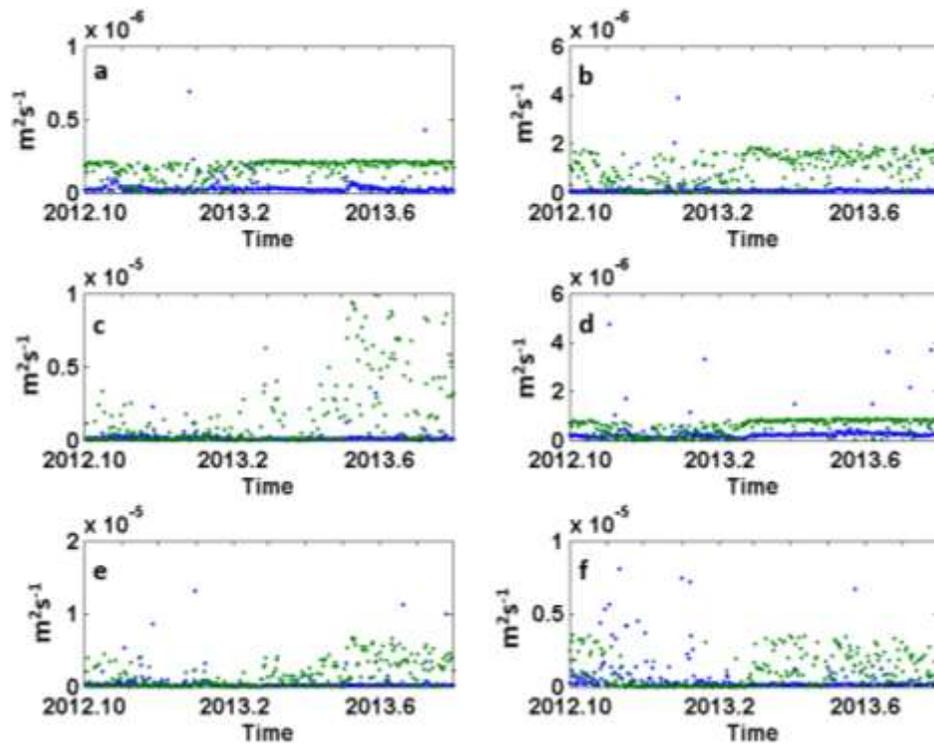


285

286 **Fig. 1** Soil thermal diffusivities at six different depths calculated by the amplitude method and
 287 phase method. **a.** 5-10 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.** 10-20 cm, **e.** 10-40 cm, and **f.** 20-40 cm.

288 Blue represents the amplitude method, and green represents the phase method.

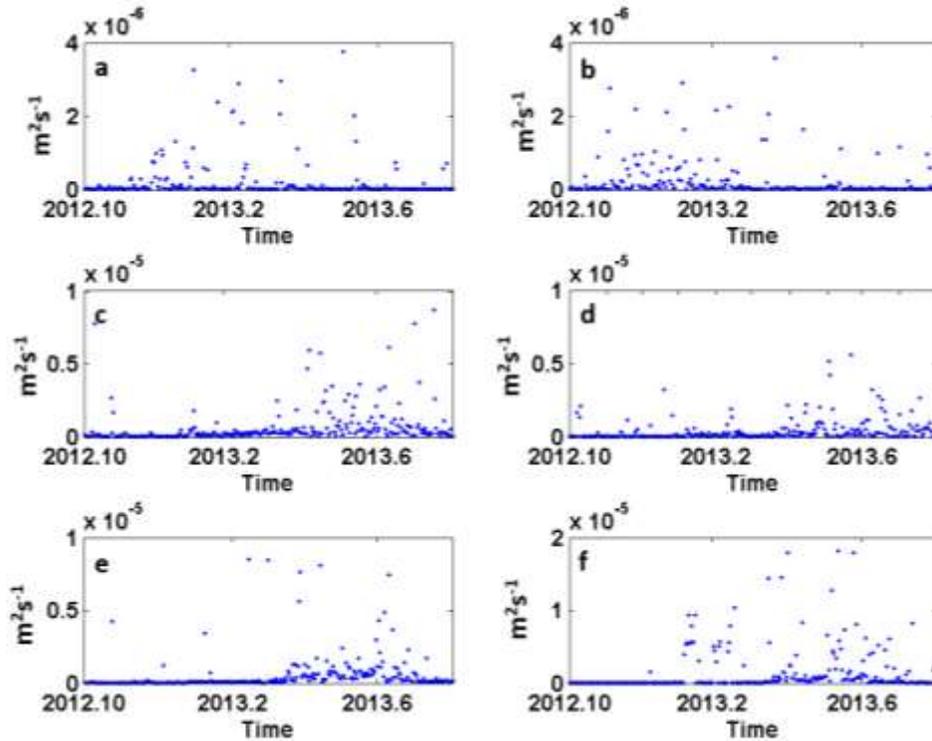
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290

291 **Fig. 2** Soil thermal diffusivities at six different depths calculated by the logarithmic method and
 292 arctangent method. **a.** 5-10 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.** 10-20 cm, **e.** 10-40 cm, and **f.** 20-40
 293 cm. Blue stands for arctangent, and green stands for logarithm

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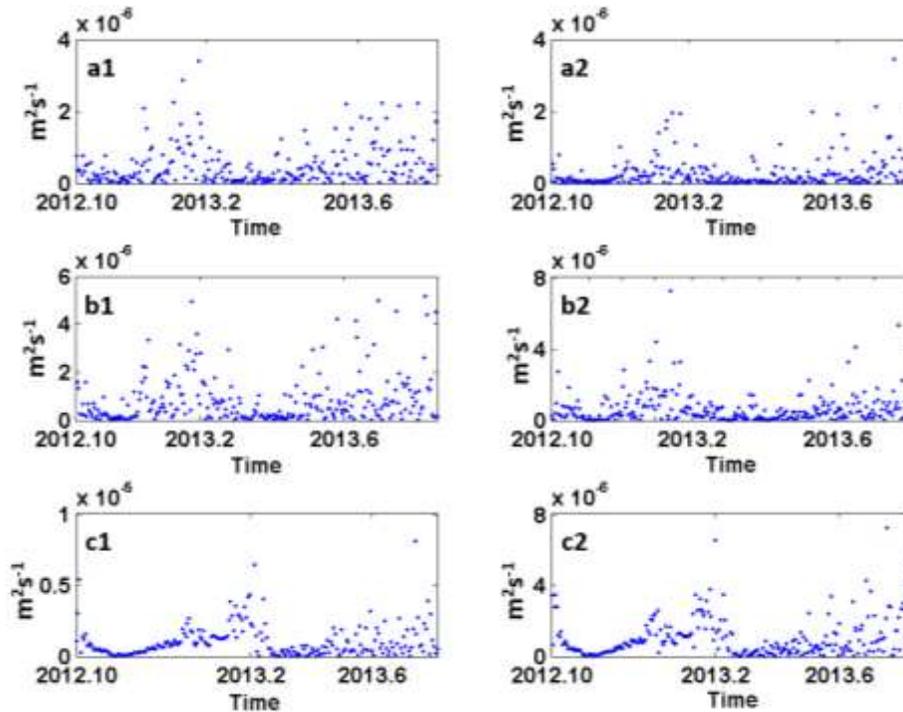
295

296 **Fig. 3** Soil thermal diffusivities at six different depths calculated by the Laplace method. **a.** 5-10
 297 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.** 10-20 cm, **e.** 10-40 cm, and **f.** 20-40 cm.

298 4.2 Analysis of numerical methods for the thermal conduction equation

299 Two differential formats are used, namely, format 1 (Dufeat-Frankel-Sch) and format 2
 300 (Crank- Nicholson-Sch), and the heat transfer equation is solved in 10-minute steps. The results
 301 are shown in Fig. 4. The three different depths (5-20 cm, 5-40 cm, 10-40 cm) of soil thermal
 302 diffusivity obtained by the two methods in Fig. 4 have two peaks between December 2012 and
 303 June 2013. The thermal diffusivity changes obtained in the two formats are generally the same,
 304 but the dispersion of k values in the second format is small. Between the two, although format 1
 305 is stable, the data utilization is less than that of format 2 and the precision is lower. The second
 306 format is unconditionally stable, and the data utilization rate is high; therefore, the degree of
 307 dispersion is small, and the precision is higher. Liu et al. (1991) pointed out that on a sunny day
 308 with few clouds, the numerical method needs to measure 12 data points from 3 depths; and when
 309 the weather is cloudy, it is necessary to measure 24 data points from 3 depths with high
 310 precision. In the case of a shortened time interval, the relative bias will also decrease; in both

311 formats, format 2 has higher precision and neither of them needs to reduce Δz or Δt to ensure
312 stability.



313

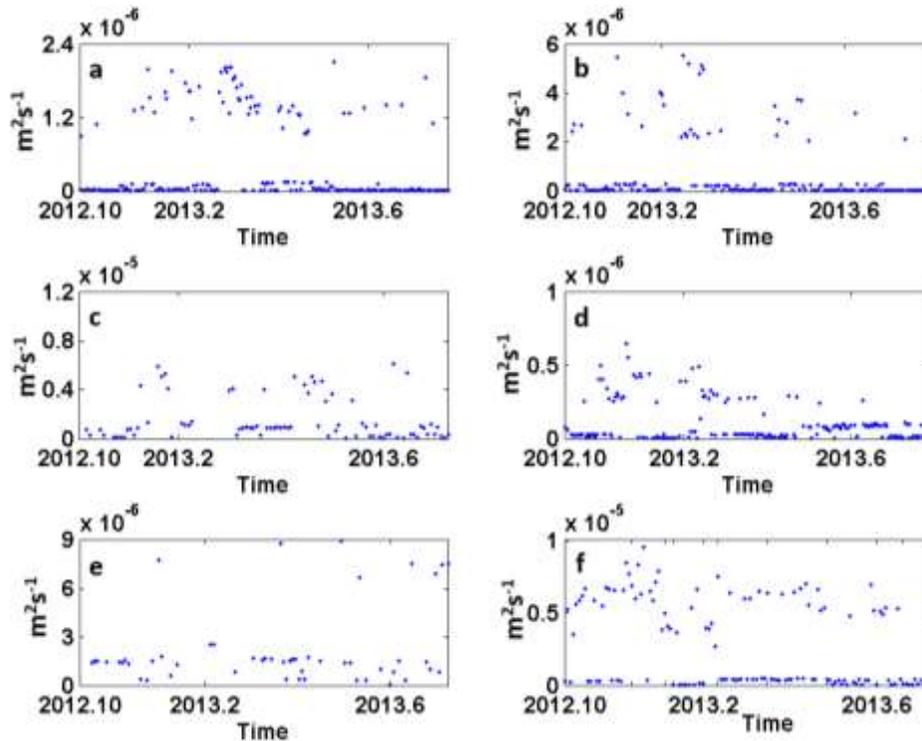
314 **Fig. 4** Soil thermal diffusivities at three different depths calculated by format 1 (Dufeat-Frankel-
315 Sch) and format 2 (Crank-Nicholson-Sch). **a1, a2.** 5-20 cm; **b1, b2.** 5-40 cm; and **c1, c2.** 10-40
316 cm.

317 4.3 Analysis of the results of the thermal conduction-convection equation under Fourier series
318 boundary conditions

319 4.3.1 First-order Fourier series (thermal conduction-convection)

320 In Fig. 5, the thermal conduction-convection method is a special case (first-order) of the
321 thermal conduction-convection equation under the Fourier boundary condition. Traditional
322 algorithms assume that the soil is vertically uniform and only consider heat transfer; the thermal
323 conduction-convection equation considers the vertical heterogeneity in the soil and combines the
324 effects of upward thermal convection (water transport) on soil temperature. Comparing the
325 results of the thermal conduction-convection method with the previous methods, the thermal
326 conduction-convection method is more sensitive to the change in soil thermal diffusivity and can
327 better reflect the change in soil thermal diffusivity with weather. The main disadvantage of the

328 traditional thermal conduction equation is that when the vertical gradient of soil thermal
329 diffusivity is relatively large, it overestimates the amplitude and phase of the soil temperature;
330 therefore, it is only suitable for estimating the actual soil temperature of vertically uniform dry
331 soil (Gao 2005).



332

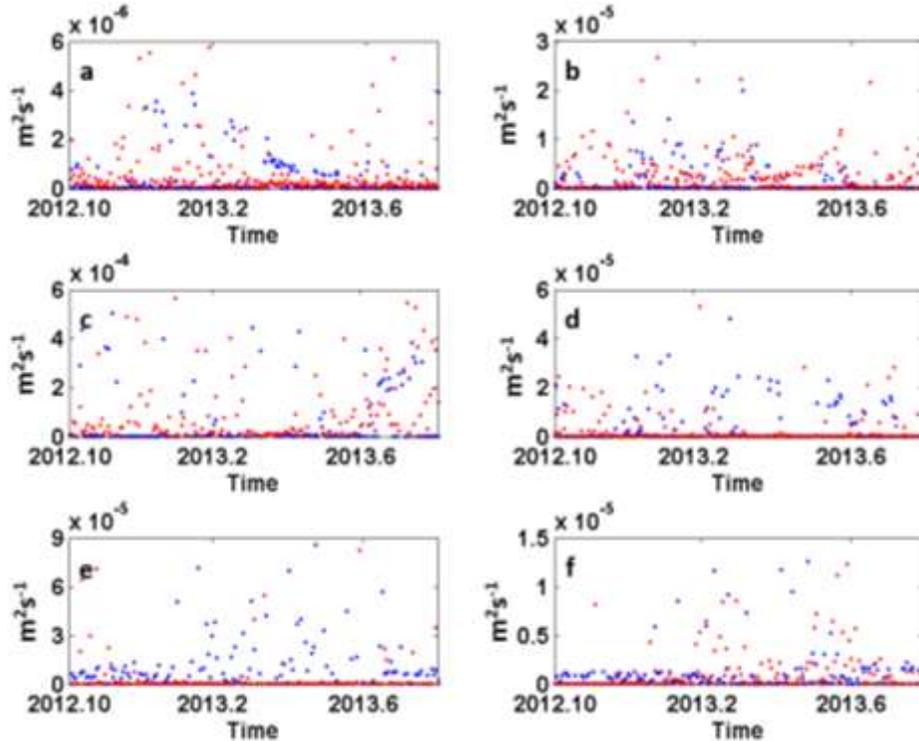
333 **Fig. 5** Soil thermal diffusivities of six different depths on the surface calculated by the first-order
334 Fourier series (thermal conduction-convection method). **a.** 5-10 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.**
335 10-20 cm, **e.** 10-40 cm, and **f.** 20-40 cm.

336 4.3.2 Second-order, third-order and fourth-order Fourier series

337 In Fig. 6, Fig. 7 and Fig. 8, the Fourier series, which is a special case of the Fourier integral, is
338 one of the classical methods for analyzing the continuity of periodic signals. When performing
339 Fourier series decomposition on a computer, the continuous signal is sampled and then
340 decomposed according to the discrete Fourier series. Any periodic continuous signal can be
341 decomposed into a set of rotation vectors according to the Fourier series (Ahmed and Rao 1975;
342 Liang 1982). The soil thermal diffusivity is difficult to change, and it has a certain periodicity
343 most of the time; therefore, it is reasonable to use the Fourier series. Fourier decomposition is
344 essentially a filtering process (Duan et al. 2016). The fitted n th-order phase Φ_n and the

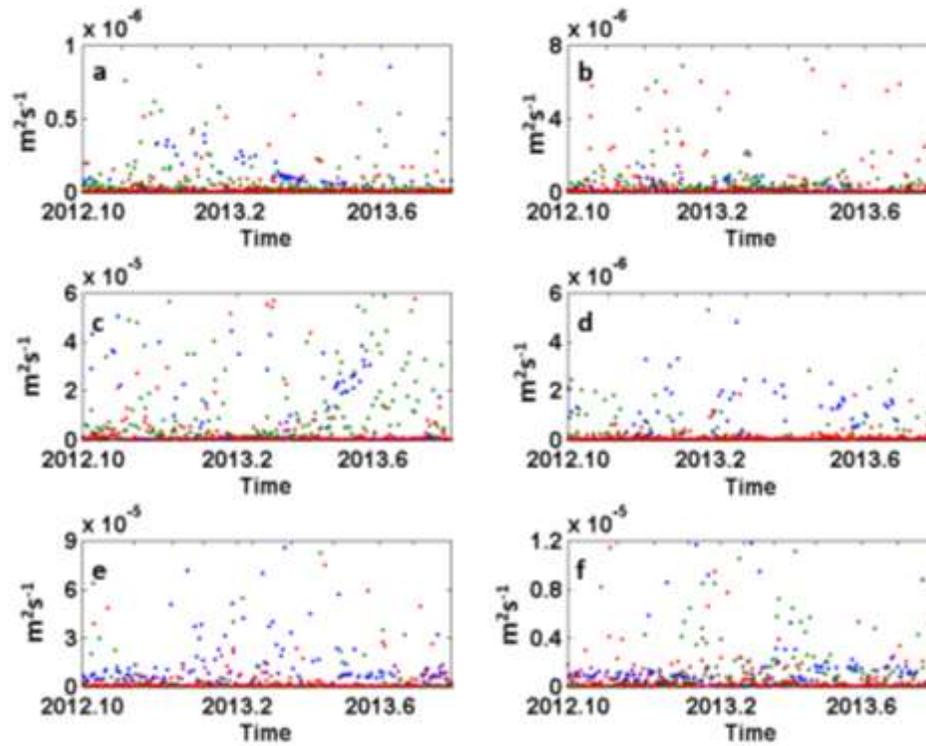
345 amplitude A_n are substituted into Eq. (32) to obtain the value of k_n , which is the contribution of
346 different wave components to the soil thermal diffusivity k . These soil thermal diffusivity
347 components k_n can be superimposed to obtain a more accurate change in the soil thermal
348 diffusivity k . As the order n becomes larger, the simulated soil thermal diffusivity k will be more
349 accurate.

350 **Second-order:**



351
352 **Fig. 6** Soil thermal diffusivities of six different depths on the surface calculated by second-order
353 Fourier series. **a.** 5-10 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.** 10-20 cm, **e.** 10-40 cm, and **f.** 20-40 cm.
354 Blue for k_1 , and red for k_2 .

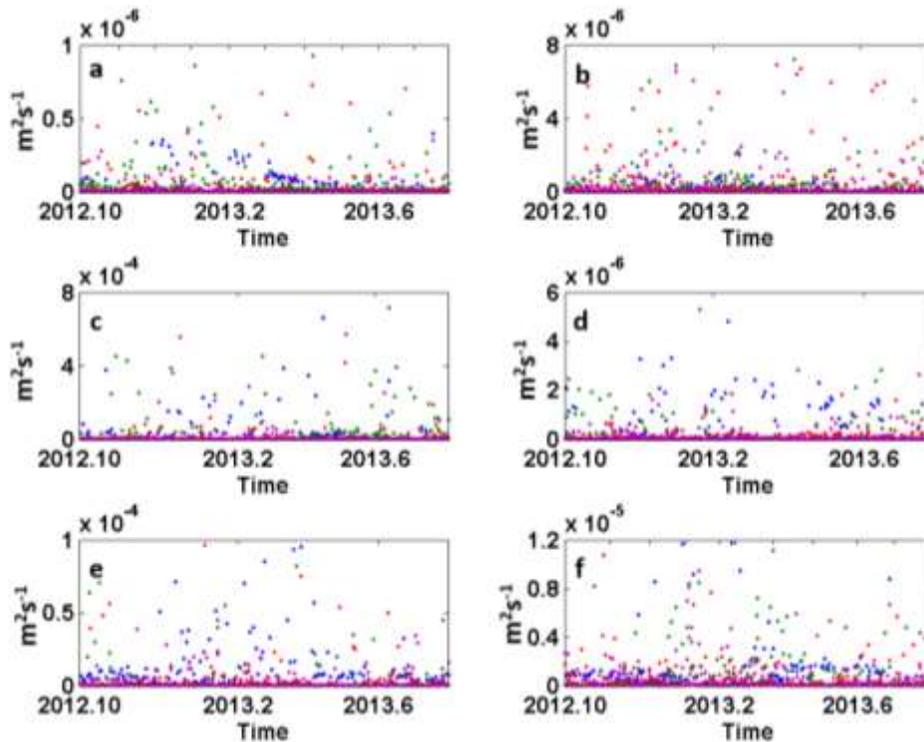
355 **Third-order:**



356

357 **Fig. 7** Soil thermal diffusivities of six different depths on the surface calculated by third-order
 358 Fourier series. **a.** 5-10 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.** 10-20 cm, **e.** 10-40 cm, and **f.** 20-40 cm.
 359 Blue for k1, red for k2, and green for k3.

360 **Fourth-order:**



361

362 **Fig. 8** Soil thermal diffusivities of six different depths on the surface calculated by fourth-order
 363 Fourier series. **a.** 5-10 cm, **b.** 5-20 cm, **c.** 5-40 cm, **d.** 10-20 cm, **e.** 10-40 cm, and **f.** 20-40 cm.
 364 Blue for k1, red for k2, green for k3, and purple for k4

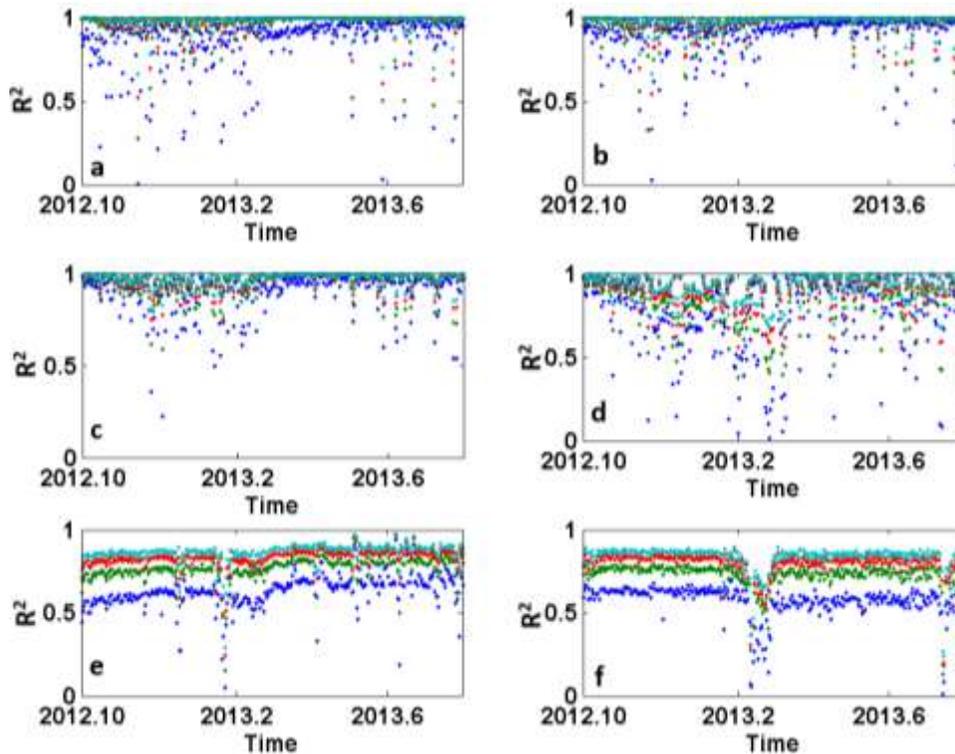
365 4.4 Bias analysis of fitting soil temperature under Fourier series

366 Soil temperature changes are complex and affected by many factors. Soil convective heat
 367 exchanges have a significant contribution to soil temperature oscillations. Therefore, using the
 368 Fourier series to accurately describe the diurnal variation in shallow soil can reduce the bias
 369 caused by assuming that the temperature of the soil surface follows a single sine wave (Wang et
 370 al. 2010). In this section, the soil temperature fitted by the 1st-, 2nd-, 3rd-, and 4th-order Fourier
 371 series is compared with the measured soil temperature. The goodness of fit of different
 372 regression models is usually determined using the coefficient of determination (R^2) (Wang et al.
 373 2019). The coefficient of determination, also known as the determination coefficient, and the
 374 decision index represent the amount by which the independent variable explains the percentage
 375 change of the dependent variable. Therefore, the larger the coefficient of determination, the
 376 better the regression effect of the model. R^2 can be expressed as follows:

377

$$R^2 = 1 - \frac{\sum(y - \hat{y})^2}{\sum(y - \bar{y})^2}$$

378 In Fig. 9, several sets of data at the same depth (a1, b1, c1, d1; a2, b2, c2, d2; a3, b3, c3, d3;
379 a4, b4, c4, d4; a5, b5, c5, d5; a6, b6, c6, d6) are used for comparison. In the six sets of data, the
380 R^2 value is ordered as follows fourth-order > third-order > second-order > first-order. In
381 addition, the fourth-order Fourier series is used to fit the soil temperature to depths of 5 cm, 10
382 cm, and 20 cm, R^2 is above 0.96, and the highest is 0.9999. The minimum value of the fitting
383 result with respect to the first-order Fourier series is less than 0.5, indicating that the fitting result
384 also improves as the fitting order increases. At depths of 80 cm and 180 cm, the soil change was
385 close to a linear change due to the layered soil (Fig. 10); therefore, the results obtained by the
386 Fourier series were weaker than that at other levels. Moreover, studies have shown that using the
387 fifth-order Fourier series to simulate the daily variation in the soil temperature field is quite
388 accurate (Liu et al. 1991). Too many harmonics will cause oscillations, which are not only
389 difficult to calculate but also reduce the accuracy.



390

391 **Fig. 9** Bias for soil temperature fitted by Fourier series. Results at **a.** 5 cm; **b.** 10 cm; **c.** 20 cm; **d.**
392 40 cm; **e.** 80 cm; and **f.** 180 cm. Dark blue for the 1st order, green for the 2nd order, red for the
393 3rd order, and light blue for the fourth order.

394



395

396 **Fig. 10** Soil layer structure.

397 **5 Conclusions**

398 In this paper, the results of soil thermal diffusivities obtained from different boundary
399 conditions under the thermal conduction equation are compared horizontally. A new model for
400 solving the thermal diffusivity of the thermal conduction-convection equation under the Fourier
401 boundary condition is proposed, and the results of soil temperature simulations with different
402 order Fourier series are compared. The results show that (1) the amplitude method and phase
403 method are based on a single temperature sine wave, which is used to describe the general soil;
404 however, the accuracy is not high enough and the disadvantages are especially obvious when
405 encountering multiple temperature extreme values. The logarithmic method and the arctangent
406 method are performed four times a day, which can partially reflect the nonperiodic change of soil
407 temperature; however, the data utilization rate is not high enough and the accuracy of the

408 obtained results is also low. The Laplace method does not have a clear soil temperature boundary
409 function and thus can better address extreme weather effects or nonperiodic changes in soil
410 temperature. (2) When solving the thermal conduction equation by a numerical method, format 2
411 (Crank-Nicholson-Sch format) is unconditionally stable and the data utilization rate is higher.
412 The obtained soil thermal diffusivity is less discrete, and the result is more accurate. (3) When
413 the thermal conduction-convection equation is used to solve the soil thermal diffusivity under the
414 Fourier series boundary condition, the n-order soil thermal diffusivity k_n represents the influence
415 of different fluctuations of soil temperature on the total soil thermal diffusivity and its
416 contribution; when the soil temperature is simulated by the Fourier series, the result becomes
417 more accurate as the order n becomes larger than the measured soil temperature. In addition, the
418 Fourier series performs well in simulating and solving soil thermal properties. The model for
419 solving the soil thermal diffusivity by the thermal conduction-convection equation under the
420 Fourier boundary condition proposed in this paper has certain significance in solving the
421 problem of thermal diffusivity calculation. However, it assumes that soil temperature changes
422 have a certain periodicity, which may cause some problems when addressing nonperiodic
423 changes in soil. According to the previous test, the Laplace method of the thermal conduction
424 equation performs well in response to nonperiodic changes in soil temperature. However, the
425 Laplace transform process is more difficult and the solution is more complicated. Therefore, this
426 method should be applied to the thermal conduction-convection equation in a more convenient
427 and feasible way, and it is expected to further contribute to the solution of soil thermal
428 diffusivity.

429 Heat transport into active layer soils is important to understanding potential responses to
430 changes in surface energy balance, particularly in the context of changing climate. Soil thermal
431 properties are key parameters controlling the energy and water cycles. At the same time, with the
432 global warming, near-surface air temperature acts as an external forcing of soil temperature, and
433 its changes have a great impact on the thermal effects of soil fluctuations of different
434 frequencies. Therefore, it is also necessary to analyze the thermal properties of soil fluctuations
435 at different frequencies. This work starts with the improvement of soil thermal diffusivity, which
436 is one of the thermal properties of soil. It helps to understand the changes in soil thermal
437 properties and thermal movement, as well as the land-atmosphere interaction under the
438 background of climate change.

439 **Appendix**

440 *Derivation of k_n under Fourier series boundary condition (TCCMF)*

441 According to the derivation of the conduction convection method by Gao (2005), we can
442 derive the solution of the soil thermal diffusivity under Fourier series boundary conditions.

443 A_n^1, Φ_n^1 and A_n^2, Φ_n^2 under the Fourier series boundary condition can be expressed as follows:

444
$$A_n^1 = A_n \times z_1 e^{(-\frac{W}{2k} - \frac{\sqrt{2}}{4k} X_n)} \quad (1'a)$$

445
$$\Phi_n^1 = \frac{\sqrt{2}\omega z_1}{nX_n} \quad (1'b)$$

446
$$A_n^2 = A_n \times z_2 e^{(-\frac{W}{2k} - \frac{\sqrt{2}}{4k} X_n)} \quad (1'c)$$

447
$$\Phi_n^2 = \frac{\sqrt{2}\omega z_2}{nX_n} \quad (1'd)$$

448 where A_n^1, Φ_n^1 and A_n^2, Φ_n^2 are the amplitude and phase of the nth term of the Fourier series at

449 depths z_1 and z_2 , respectively; and $X_n = \sqrt{W_n^2 + \sqrt{W_n^4 + 16k_n^2\omega^2}}$.

450 Assuming that $z_1 > z_2$ (that is, $A_n^1 < A_n^2, \Phi_n^1 > \Phi_n^2$), the following is obtained:

451
$$\frac{\ln(A_n^1/A_n^2)}{z_1 - z_2} = \left(-\frac{W}{2k} - \frac{\sqrt{2}}{4k} X_n \right) \quad (2')$$

452 From Eq. (1'b) and Eq. (1'd), the following can be concluded:

453
$$X_n = \frac{\sqrt{2}\omega(z_1 - z_2)}{n(\Phi_n^1 - \Phi_n^2)} \quad (3')$$

454 Combining Eq. (2') with Eq.(3'), the following is obtained:

455
$$k_n^2 = \frac{(z_1 - z_2)^2 \cdot [W_n + \omega \cdot \frac{z_1 - z_2}{n(\Phi_n^1 - \Phi_n^2)}]^2}{4\ln^2(A_n^1/A_n^2)} = \frac{(z_1 - z_2)^2 \cdot [nW_n(\Phi_n^1 - \Phi_n^2) + \omega(z_1 - z_2)^2]}{4n^2(\Phi_n^1 - \Phi_n^2)^2 \ln^2(A_n^1/A_n^2)} \quad (4')$$

456 Eq. (4') can be rewritten as follows:

457
$$k_n^2 = \frac{(z_1 - z_2)^2}{4n^2(\Phi_n^1 - \Phi_n^2)^2} \left[\frac{\omega^2(z_1 - z_2)^2}{n^2(\Phi_n^1 - \Phi_n^2)^2} - W^2 \right] \quad (5')$$

458 Eq. (4') and Eq. (5') are combined to eliminate k_n and obtain an equation for W_n :

459
$$[nW_n(\Phi_n^1 - \Phi_n^2) + \omega(z_1 - z_2)]^2 = \ln^2\left(\frac{A_n^1}{A_n^2}\right) \left[\frac{\omega^2(z_1 - z_2)^2}{n^2(\Phi_n^1 - \Phi_n^2)^2} - W_n^2 \right] \quad (6')$$

460 Eq. (6') can be rewritten as follows:

461
$$aW_n^2 + bW_n + c = 0 \quad (7')$$

462 where

463
$$\begin{cases} a = n^4(\Phi_n^1 - \Phi_n^2)^4 + n^2(\Phi_n^1 - \Phi_n^2)^2 \cdot \ln^2(A_n^1/A_n^2) \\ b = 2n^3\omega(\Phi_n^1 - \Phi_n^2)^3(z_1 - z_2) \\ c = \omega^2(z_1 - z_2)[n^2(\Phi_n^1 - \Phi_n^2)^2 - \ln^2(A_n^1/A_n^2)] \end{cases} \quad (8')$$

464 According to Eq. (7'), the value of W_n is not always negative:

465
$$W_n = \frac{\omega(z_1 - z_2)}{n(\Phi_n^1 - \Phi_n^2)} \left[\frac{2\ln^2\left(\frac{A_n^1}{A_n^2}\right)}{n^2(\Phi_n^1 - \Phi_n^2)^2 + \ln^2\left(\frac{A_n^1}{A_n^2}\right)} - 1 \right] \quad (9')$$

466
$$k_n = - \frac{(z_1 - z_2)^2 \omega \ln\left(\frac{A_n^1}{A_n^2}\right)}{n(\Phi_n^1 - \Phi_n^2) \left[n^2(\Phi_n^1 - \Phi_n^2)^2 + \ln^2\left(\frac{A_n^1}{A_n^2}\right) \right]} \quad (10')$$

467

468

469 **Data availability statement**

470 Datasets for this research are included in this paper (and its supplementary information files):

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