

An Aqueous, Electrode-Decoupled Redox-Flow Battery for Long Duration Energy Storage

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Abstract

Redox-flow batteries (RFBs) enable large-scale energy storage at low cost due to the independent scaling of device power and energy, thereby unlocking energy arbitrage opportunities and providing a pathway to grid stability and resiliency. Herein we demonstrate an “electrode-decoupled” redox-flow battery (ED-RFB) with titanium and cerium elemental actives that has a clear pathway to achieve a levelized cost of storage (LCOS) of *ca* \$0.025/kWh-cycle. A key enabling technology is our highly perm-selective modified poly(ether ketone)-based anion exchange membrane (AEM) that ensures long term separation of Ti and Ce species and enables capacity-fade-free cycling over 1300 hours of operation. Further, our Ti-Ce ED-RFB exhibits negligible capacity fade when the actives are charged to 90% state of charge (SOC), stored for close to 100-hours and then discharged, rendering it viable for long duration (load-following) grid-scale energy storage applications. Herein we introduce the Ti-Ce ED-RFB as a novel, low-cost long duration energy storage (LDES) system.

Introduction

The sustained fall in the cost of solar photovoltaic and wind energy has led to a market-driven increase in their deployment in the electricity grid.¹⁻⁴ Ensuring reliability and resiliency of the increasingly renewables-powered grid will require the deployment of suitable energy storage technologies.⁵⁻⁸ Deployment of energy storage resources at scale will in turn drive innovation, expand economies of scale, reduce costs and setup a virtuous cycle of increasing decarbonization.^{4,9-11} Typical batteries (e.g., Li-ion batteries) seldom maintain discharge at peak power for durations sufficient to regulate power output from intermittent sources.¹² On the other hand, redox-flow batteries (RFBs) are excellent candidates for grid-storage applications¹³ wherein the electroactive materials are externally stored and pumped into the electrochemical stack as required, decoupling the energy and power obtainable from a given unit. The energy is a function of the amount of externally stored electroactive material while the power is a function of the stack size, allowing for independent scaling of device energy and power, in turn ensuring sub-linear scaling of the system cost with scale.^{14,15}

Thaler and co-workers at NASA demonstrated the first RFB in the 1970s¹⁶ based on the Fe-Cr¹⁷⁻¹⁹ chemistry. Despite years of effort, this relatively cost-effective system suffers parasitic side-reactions whose mitigation requires complex system-level changes.¹⁹⁻²¹ This has led to the failure of multiple commercial ventures deploying this technology.²² In the 1980s the all-V RFB^{23,24} was developed by Skyllas-Kazacos and co-workers and this chemistry is the farthest along in terms of commercial development. Despite the operational advantages of using the same elemental active on the cathode and anode sides, vanadium is cost-prohibitive, geographically limited in availability (and hence geopolitically constrained) and is not likely to meet system-level cost targets.^{5,15} Numerous other elemental active combinations have been demonstrated in RFBs with some examples being the Zn-Ce²⁵⁻²⁷, all-Fe^{28,29}, Ce-Pb³⁰, V-Ce³¹⁻³³, Zn-V³⁴, Cr-Zn³⁵ chemistries. The challenges in each case have been a combination of high cost, parasitic side reactions (e.g., H₂ evolution), durability, difficulties with phase-change at the

electrode (plating/dissolution), and reactant-cross-over-driven capacity-fade. More recently, aqueous RFBs with organic actives^{36–39} and non-aqueous RFBs^{40–43} have been investigated. Aqueous RFBs featuring organic active species suffer from side-reactions involving the very same electroactive centers in these molecules. A prominent example is the dimerization of methyl viologen based actives.^{44–46} Further, these systems claim cost-effectiveness once the production of the proposed actives are scaled up.^{14,15,47} Currently no economic or market incentives exist for investments in the production of these organic actives, which in turn has to be followed by additional capital investments to manufacture the RFBs at scale. Organic RFBs suffer from significantly higher costs due to the nature of the solvents and actives used.^{14,15} Thus, no commercial RFB systems employing organic actives in aqueous media or organic electrolyte solvents currently exist.

We posit that viable RFB alternatives to mass-produced energy storage systems such as Li-ion batteries (that linearly scale in terms of cost due to coupling of energy and power) should utilize electrolyte precursors that are already produced at scale and require minimal processing. Further, any RFB system should meet the overall DOE / ARPA-E cost targets that have been documented to have any chance at a viable pathway to commercialization.^{5,48,49} In this paper, we: **a)** identify the characteristics of such an ideal RFB system, **b)** identify Ti and Ce as abundantly available electroactive species satisfying these criteria, **c)** elucidate their electrochemistry, **d)** develop a Ti-Ce electrode-decoupled RFB (ED-RFB) employing our unique and highly perm-selective anion exchange membrane (AEM) separator that permits the use of dis-similar actives at either electrode without irreversible capacity-fade, **e)** test the ED-RFB over a long time frame (1300 hours) employing long-duration (24-hr) cycles that mimic real world usage, and **f)** show through detailed techno-economic analyses that our ED-RFB system can comfortably attain a levelized cost of storage (LCOS) of <\$0.05/kWh-cycle when deployed at scale, thereby being cheaper than established DOE targets for grid-storage applications.

The development and utilization of our highly perm-selective AEM separator is particularly noteworthy as it permits electrode-decoupled operation with minimal to no intermixing of the cations in the catholyte and the anolyte, thereby doubling the usable capacity of the cell.^{31,50,51} The electrode-decoupled operation greatly expanded the chemical design space available for the choice of actives, resulting in the development of the aqueous Ti-Ce ED-RFB.

Results And Discussions

The desired design characteristics of an ideal redox-flow battery (enumerated below and expanded upon in Supporting Materials section S1) were determined after taking into consideration the problems and challenges identified in existing systems^{13,52,53} and with the aim of keeping the overall cost under \$100/kWh^{5,15,49}:

1. High coulombic efficiency: Minimal parasitic side-reactions or gas-evolution (H₂ or O₂) reactions during operation.

2. Nominal operating cell voltage $\geq 1V$ and low equivalent weight of active materials to reduce cost/kWh.
3. No reactions involving phase change at either electrode: Multiple (soluble) oxidation states needed for the electroactive species.
4. Low cost: Aqueous electrolytes combined with low-cost and currently mass-produced electro-actives with good solubility.
5. Benign (non-toxic, no side reactions).

By examining various electroactive species soluble in aqueous electrolytes (Supplementary Materials **Fig. S1**), several possible combinations that could constitute cells with $\geq 1V$ were identified. Unfortunately, the cells with the highest nominal voltages, namely the Zn-Ce and Zn-Br systems do not meet the phase change criterion, with Zn dendrite mitigation being a perennial problem.^{25,54} The Fe-Cr system, with a nominal voltage of 1.19V suffers from irreversible side reactions and H₂ evolution at the Cr electrode.¹⁹ The methyl viologen and ferrocenium based actives (from the work of Aziz and co-workers³⁷ and representative of the class of similar organic actives) do form $\geq 1V$ cells in combination with elemental actives at the other electrode but their long-term stability and cost-effective production at scale has not been demonstrated. And while the all-V system is outstanding in many respects, the cost of vanadium is such that the cost of actives alone would exceed the DOE cost target for the RFB system.^{5,48,49}

The elemental actives were next examined in the context of their abundance in the Earth's crust as well as their broad availability, and hence their potential for meeting large-scale deployment on the worldwide electric grid. Figure 1 **(a)** depicts the abundances of some of the electroactive elements that satisfy one or more of the criteria outlined above.⁵⁵ Ti was found to be 20x as abundant as V and hence would be an excellent replacement for V-based RFBs. Given that the E⁰ of the TiO²⁺/Ti³⁺ couple is 0.19V vs. SHE, it has to be paired with the Ce³⁺/Ce⁴⁺ couple to produce a cell with a nominal voltage $\geq 1V$. Despite being a so called "rare earth" element, Ce is as abundant as Pb (found in lead-acid batteries used in every internal combustion gasoline vehicle on the road today) and is almost 2x as abundant as Co, which is critical to Li-ion batteries. The existing proven reserves depicted in Fig. 1 **(b)** can enable Ti-Ce RFBs to store over 300 times the entire world electricity production (25,000 TWh/year) (see production data in Fig. 2) even based on the limiting species, Ce. Figure 1 **(c)** and **(d)** identify the countries with the top 5 proven reserves of Ti and Ce. The existence of reserves does not necessarily indicate the level of development or exploitation of those reserves, but the wide geographical spread of these reserves could make Ti and Ce supply immune to geopolitical shifts. Thus, the combination of Ti and Ce satisfied all of our technical criteria and also offered several economic and geopolitical advantages and hence was chosen for further study.

A schematic for our Ti-Ce ED-RFB is depicted in Fig. 2 **(a)**. The highly permselective AEM ensures that ion conduction across the separator occurs primarily by the transport of anions as depicted in Fig. 2 **(b)**. The corresponding electrode half-cell reactions are as follows –



$\text{Ce}^{4+} + \text{e}^- \leftrightarrow \text{Ce}^{3+}$ ($E^0 = 1.61\text{V}$ vs. SHE) – Positive Electrode

The Ti and Ce electrolytes were formulated with a variety of supporting electrolytes that are stable across the voltage window of these redox couples (Supplementary Materials **Section S2**). Only acidic supporting electrolytes were examined, as the soluble oxidation states desired as per the half reactions presented above occur only at low pH (see Pourbaix diagrams in Supplementary Materials **Fig. S2**). Given the highly oxidizing nature of Ce^{4+} , side-reactions with the supporting electrolyte is a concern (Supplementary Materials **Fig. S3**). The down-selection of suitable supporting electrolytes (from amongst HCl, H_2SO_4 , HNO_3 and $\text{CH}_3\text{SO}_3\text{H}$) is detailed in Supplementary Materials **Section S2**. Both H_2SO_4 and $\text{CH}_3\text{SO}_3\text{H}$ -supported electrolyte formulations were identified as the only stable combinations; the side-reactions encountered with HCl and HNO_3 are discussed in Supplementary Materials **Section S2**. The choice of supporting electrolytes was found to significantly affect the E^0 value of the $\text{Ce}^{3+}/\text{Ce}^{4+}$ redox couple, with a 120mV difference between H_2SO_4 and $\text{CH}_3\text{SO}_3\text{H}$ supported electrolytes in line with earlier reports.⁵⁶ Ce^{3+} and Ce^{4+} exhibit diametrically opposite solubility behavior with increasing acid concentration with Ce^{3+} solubility decreasing while Ce^{4+} solubility increases (Supplementary Materials **Fig. S4**).⁵⁷ The maximum achievable solubility where both species stay in solution is 0.5M in H_2SO_4 and 0.9M in $\text{CH}_3\text{SO}_3\text{H}$ and hence these concentrations were used at the positive electrode.

Unlike the constraints on the Ce electrolyte, TiOSO_4 was found to be highly soluble in H_2SO_4 and solutions of up to 10M have been prepared and characterized as shown in Supplementary Materials **Fig. S6**. Ti is much less readily soluble in $\text{CH}_3\text{SO}_3\text{H}$ with concentrations of 6M resulting in precipitation of the Ti salt as seen in **Fig. S6**. Nevertheless, Ce is by far the limiting species, and achieving sufficient Ti concentration at the negative electrolyte is not an issue.

Cyclic voltammograms (CVs) with Ti and Ce electrolytes indicated that a mixed supporting electrolyte consisting of H_2SO_4 and $\text{CH}_3\text{SO}_3\text{H}$ is ideal in terms of reversibility (inferred from the CV peak separation ΔE_p) and energy efficiency (directly proportional to the voltage efficiency, which is a function of reversibility) of the system (see Supplementary Materials **Fig. S7**). However, issues with variable and inversely correlated solubility of the Ce^{3+} and Ce^{4+} ion led us to avoid using these mixed systems pending further fundamental studies.⁵⁷ The CVs depicting the Ce and Ti half-cell reactions with H_2SO_4 as the supporting electrolyte are depicted in **Fig. 2(d)**. The Ce redox peaks show a separation of 0.76V while the Ti peaks are separated by 1.53V. Similarly, CVs depicting the Ce and Ti half-cell reactions with $\text{CH}_3\text{SO}_3\text{H}$ as the supporting electrolyte are depicted in **Fig. 2(e)**. The Ce redox peaks show a separation of 0.67V while the Ti peaks are separated by 1V. Given the $> 59\text{mV}$ peak separation, both half-reactions are not reversible.⁵⁸ This resultant differences between the average charge and discharge voltages for the Ti-Ce ED-RFB can be mitigated by suitable surface treatment of the RFB electrodes.⁵⁹ This will in turn influence the voltage efficiency and hence energy efficiency of the RFB. Despite the differences in ΔE_p , the differences in formal potentials $E_{form} = (E_{cathodic} + E_{anodic})/2$ ensures that the theoretical open circuit potential (OCP) for the Ti-Ce ED-RFB is *ca* 1.36V with the $\text{CH}_3\text{SO}_3\text{H}$ supported electrolytes exhibiting a

slightly higher OCP (~ 20mV higher) due to the observed shift in $E_{1/2}$ of the Ce electrolyte when used with $\text{CH}_3\text{SO}_3\text{H}$. Ce^{4+} was verified to not cause any unwanted oxidative reactions in both systems.

Supplementary Materials **Section S3.2** details the calculation of the diffusion coefficients of Ce and Ti redox species in H_2SO_4 and $\text{CH}_3\text{SO}_3\text{H}$ supporting electrolytes (values tabulated in **Table S1**) using the Nicholson-Shain method.⁶⁰ Diffusion coefficients were higher for Ce species as compared to Ti species, and higher diffusion coefficients in $\text{CH}_3\text{SO}_3\text{H}$ -supported electrolytes suggested reduced complexation with both Ti and Ce following Pearson's hard-soft acid-base theory.^{61,62} The first electron transfer rate constants (k_0) for both the Ce and Ti redox couples were also calculated from the CVs using the method of Kochi and Klingler as detailed in Supplementary Materials **Section S3.3**.⁶³ Reduced complexation in $\text{CH}_3\text{SO}_3\text{H}$ -supported electrolytes led to higher k_0 values in these electrolytes. The k_0 values for the Ti redox couple in both supporting electrolytes were 3-orders of magnitude lower than for the Ce redox couple, indicating that negative (Ti) electrode is rate limiting. The H_2SO_4 - and $\text{CH}_3\text{SO}_3\text{H}$ -supported electrolyte formulations were tested further in RFBs.

Having identified and characterized suitable Ti and Ce electrolytes, the key requirement to realize an ED-RFB is a highly permselective AEM. We selected a quaternized cardo-poly(ether ketone) (QPEK-C)-based AEM functionalized with trimethylamine (TMA) (depicted in Fig. 2(c)). We have previously reported this separator³¹ and composites thereof incorporating metal oxide nanoparticles⁵⁰ to improve permselectivity. We have significantly enhanced the permselectivity reported in our previous work by judiciously incorporating various metal oxide nanoparticles (details in Supplementary Materials **Section S4** and AEM characteristics in **Table S3**). The resultant permselectivity improvement is summarized in Fig. 3 in terms of the permeability coefficient, a time-independent measure of permeation of a given species across a separator.^{47,64} QPEK-C-TMA AEMs incorporating Al_2O_3 nanoparticles exhibited the lowest permeability coefficient, equivalent to < 0.4% undesired cross-over of cations over 1000 hours, which compares very favorably in terms of capacity-fade with extant state-of-the-art technologies.⁴⁷

Ti-Ce ED-RFBs incorporating pristine QPEK-C-TMA and its metal oxide nanoparticle enhanced variants were tested (details in Supplementary Materials **Section S6**) and the performance of the ED-RFB with H_2SO_4 -supported Ti-Ce electrolytes separated by a Al_2O_3 enhanced QPEK-C-TMA separator is depicted in Fig. 4. The cell was cycled diurnally (i.e., 12-hour charge- 12-hour discharge) for 1300 hours (about 8 weeks) to mimic the load leveling use case on the electric grid. Despite minimal cycle to cycle variations in capacity (Fig. 4 (a)), the normalized capacity never fell below 90%. Near 100% capacity retention was observed, indicating that the highly perm-selective separator was indeed mitigating a major route for capacity fade, namely active species cross-over. The area-specific resistance (ASR) of the separator remained unchanged within experimental error over the duration of the run, confirming *ex-situ* observations via ^{13}C - ^1H 2D NMR and attached proton test (APT) (detailed in Supplementary Materials **Section S5**) confirming that there was no chemical degradation of the QPEK-C-TMA separator in low pH electrolytes (unlike at high pH, wherein AEM degradation is well documented).^{65,66} Since chemical degradation affects separator conductivity and the separator is the largest resistive source in the device,

this exceptional separator stability confirms its suitability for long-term operation. The coulombic, voltage and energy efficiencies of the ED-RFB are depicted in Fig. 4 **(b)** (calculations detailed in the Supplementary Materials **Section S6** and elsewhere⁶⁷). As expected from the CVs, the irreversible nature of the Ti and Ce redox couples necessitates the application of higher overpotentials to drive the redox reactions. This directly translates into poorer voltage efficiency. Given that the energy efficiency is a product of the coulombic and voltage efficiencies, the energy efficiency is, on average, *ca* 70%. The observation that changing the supporting electrolyte significantly changes the redox potentials for both half-reactions of interest suggests that the use of electrolyte additives or alternate stable supporting electrolytes provide viable pathways to further increase the voltage efficiency of the Ti-Ce ED-RFB, as does electrode-modification to lower redox-reaction overpotentials. Overall, the highly energy efficient diurnal energy storage performance of Ti-Ce ED-RFB makes it an excellent candidate for grid deployment provided economic pathways exist to achieve the DOE target LCOS of <\$0.05/kWh-cycle.

A second grid-scale deployment use case examined was that of long duration energy storage (LDES). Since the RFB places the energy storage media outside the cell itself, the amount of energy that can be stored is limited only by tank size. Thus, the potential exists to scale RFBs to enable multi-day or even multi-week (i.e., extended-duration) energy storage. The key to this use case is the minimization of capacity fade during storage (i.e., self-discharge). The self-discharge performance of the Ti-Ce ED-RFB was examined by cycling it for 100 hours followed by charging it to a 90% state of charge (SOC), withdrawing the charged electrolytes, and storing them in their tanks. After 96 hours of storage, the electrolytes were reintroduced into the RFB and discharged, and the discharge capacity was measured. The polarization performance of the RFB before and after storage at 90% SOC is depicted in Fig. 5**(a)**. The OCP before and after storage was unchanged within experimental error, indicating minimal self-discharge during storage. The polarization curve was also essentially unchanged, as were the activation and ohmic polarization. The near-quantitative absence of self-discharge was confirmed by discharging the cell from 90% SOC (Fig. 5**(b)**). The coulombic efficiency was close to 100% for both this “charge-store-discharge” cycle and for the previous conventional charge-discharge cycle (Supplementary Materials **section S6**). Thus, the Ti-Ce ED-RFB was found to be suitable for both diurnal and for LDES in scenarios mimicking normal grid operations.

The next key consideration in the analysis of the commercial viability of the Ti-Ce ED-RFB is the economics of the system. A comprehensive cost model considering the manufacturing of the AEM separators at various production scales, incorporating ED-RFB component and system-level costs and examining the LCOS in various operational scenarios is presented in Supplementary Materials **Section S7**. The DOE defined component cost target level is <\$10/kWh for the separator.⁴⁸ Incorporating this separator, the DOE defined system level cost target is <\$100/kWh.⁵ The separator cost was obtained by developing heuristic process models for its production at 1000 metric tons per annum (MTA) scale with industry appropriate cost scaling factors. The inevitable uncertainty in raw material, utilities, staffing and other operational costs were accounted for by cost sensitivity analysis that let us set bounds for the component and system level costs. The QPEK-C-TMA AEMs were found to cost as little as

\$2.5/kW_{equivalent}. There was minimal cost impact upon changing the cation in the AEM, with a 100x cation-precursor cost increase resulting in only a 5.5% separator cost increase. Enhancing the permselectivity by incorporating metal oxide nanoparticles into QPEK-C-TMA also had an inconsequential impact on the separator cost as the metal oxide cost and added processing cost was found to be 0.13% of the total separator cost.

The component costs were incorporated into a system cost model with RFBs at the 1MW/4MWh (distributed power system) and 2GW/10GWh (utility integrated system) scales. This analysis considered both the H₂SO₄ and CH₃SO₃H electrolytes and examined the impact of the electrolyte cost on the system cost while accounting for differences in energy density. Interestingly, while the CH₃SO₃H electrolytes cost ~ 4x the H₂SO₄ electrolytes, the near doubling of the energy density meant that the system level cost differential between the H₂SO₄ and CH₃SO₃H based systems was only a factor of 2. Overall, the Ti-Ce ED-RFB was found to cost \$90/kWh in the H₂SO₄ configuration, coming in lower than the DOE cost target.⁴⁸

The LCOS was calculated incorporating the system level costs as depicted in **Fig. S22**. The LCOS was calculated for the unoptimized system with performance metrics matching those in the lab. Following this conservative baseline, several scenarios for operational optimization at scale and cost reduction are presented in Fig. 6. Most interestingly, it was found that relatively incremental improvements in the Ti-Ce ED-RFB such as operating at 200 mA.cm⁻² current density, designs incorporating air cooling of the stack, and changing storage-tank material (and hence cost) significantly impacted the system-level cost. Similar robust pathways to reduce the LCOS were also found to exist (4 scenarios are presented in the Supplementary Materials) with plausible scenarios exceeding the DOE LCOS target of \$0.05/kWh-cycle. Thus, we posit that in addition to demonstrated technical viability, the Ti-Ce ED-RFB is an economically viable candidate for grid scale diurnal load leveling and long duration storage applications.

Materials And Methods

Extended materials and methods are available in the Supplementary Materials.

Synthesis of the anion exchange membrane (AEM) separator

The separator used herein has been previously reported by us in Yun *et. al.*⁵¹ and the synthesis procedure is unchanged. 10 g of QPEK-C (Xuzhou Vat Chemical Company, China) was dissolved completely in 500 ml 1,1,2,2-tetrachloroethane (98.5%, Acros Organics). 6 g of paraformaldehyde (96%, Acros), 25 ml of Chlorotrimethylsilane (98% Acros), and 0.47 ml of tin tetrachloride (>99%, Sigma Aldrich) were added to a well-stirred solution. The mixture was heated, and the reaction carried out at 80 °C for a week with reflux. The reaction scheme is presented in **Fig. S12**. The reaction solution was precipitated in methanol (3~4 times the volume of the reaction mixture). The white precipitate was filtered and purified by re-dissolving in dimethylformamide (DMF, 99.8%, Acros Organics) followed by re-precipitation in methanol. The purification process was carried out 2~3 times. The precipitate was dried at 40 °C over 12 hours and stored for further use. The white solid CPEK was obtained with a degree of chloromethylation

(chloromethyl groups per polymer repeating unit) of 0.8-0.9. The NMR spectra is shown in **Fig. S13**. 0.5 g of QPEK-C was dissolved completely in 9 ml of DMF followed by the addition of 0.7 ml of trimethylamine (TMA) to the mixture. The solution was stirred and allowed to react at 30 °C for 2 days. The membrane was obtained by casting the reaction mixture onto a 3" x 3" flat glass plate in an oven at 70 °C, heated overnight on a leveled surface. The thickness of the obtained membranes was approximately 40 μm. The measurement methodology for the membrane ionic conductivity and ion exchange capacity is detailed in Supplementary Materials **Section S5**.

Synthesis and characterization of ED-RFB electrolytes

The electrolytes used in this study consisted of two formulations, based on H₂SO₄ and CH₃SO₃H supporting electrolytes, respectively. The composition of the H₂SO₄-supported electrolytes was 0.5M TiSO₄ in 4M H₂SO₄ and 0.5M Ce₂(SO₄)₃ in 3M H₂SO₄. The composition of the CH₃SO₃H-supported electrolytes was 0.9M TiSO₄ in 5.8M CH₃SO₃H and 0.9M Ce(CH₃SO₃)₃ in 4M CH₃SO₃H. TiSO₄ (97%, Sigma-Aldrich) readily dissolved in water and H₂SO₄ (95-98%, Sigma-Aldrich) or CH₃SO₃H (99%, Acros Organics) to yield the desired electrolyte. The Ce₂(SO₄)₃ was made by reacting Ce₂(CO₃)₃ (99%, Treibacher Industrie A.G.) with H₂SO₄ as follows –



The Ce(CH₃SO₃)₃ was made by the reaction between CH₃SO₃H and Ce₂(CO₃)₃^{56,68}.



The Ce₂(CO₃)₃ was suspended in DI water and the desired acid was added dropwise with constant stirring. Due to the sensitivity⁵⁷ of Ce₂(SO₄)₃ and Ce(CH₃SO₃)₃ solubility to the acid concentration, the reaction mixture was diluted periodically with DI water to prevent precipitation of the cerium salt. Electrochemical characterization using cyclic voltammetry was carried out in a small-volume electrochemical cell (Pine Instruments, RRP223) with a 3mm diameter glassy carbon (GC) disc working electrode, a Pt mesh counter electrode and an Ag/AgCl reference electrode. The electrochemical measurements were performed using a Solartron multichannel potentiostat.

Redox-flow battery (RFB) tests

The redox-flow battery testing was carried out using a Scribner Inc. 857 RFB test stand using a 25cm² plate-and-frame configuration cell. The carbon felt electrodes (Sigracell GFA6, SGL carbon) were activated by heating in air in a muffle furnace at 400°C, immersing in *aqua regia* (1:3 mole ratio of HNO₃:HCl) at 60°C for 4 hours followed by thorough DI water wash and drying in an oven. All tests were carried out using interdigitated flow fields at a flow rate of 100 mL.min⁻¹ and at 25°C. The polarization measurements were carried out by initially charging the ED-RFB to the voltage corresponding to the desired state of charge (SOC) and increasing the current stepwise with a 30s hold after each step

increase to allow for equilibration. The initial SOC was maintained by discharging (or charging) the cell for 30s after each 30s hold. The charge-discharge cycling was carried out galvanostatically at a minimum current density of 100 mA.cm⁻² followed by a potentiostatic hold at the cutoff voltage until the current density trickled down to 4 mA.cm⁻². The H₂SO₄-based ED-RFBs were charged and discharged between 2V and 0.3V while the cutoffs for the CH₃SO₃H based cells were 1.85V -0.3V. The efficiency calculations for the RFB are detailed in the Supplementary Materials **Section S6**.

Cation cross-over measurements

The cation cross-over was determined by UV-vis spectroscopy. The Ti side of the ED-RFB was drained upon completion of the ED-RFB test and the concentration of Ce³⁺ ions was determined. All RFB tests were completed in such a manner that the final cell state of charge (SOC) was 0% (i.e., complete discharge) so as to have only Ce³⁺ ions in the system. The collected electrolyte was then diluted so the concentration of the dominant cation (i.e., TiO²⁺) was 0.1M. Supporting electrolyte background was separately collected and subtracted from the electrolyte spectra. To allow the comparison of cross-over values across experiments, an intensive, time independent measure, the permeation coefficient was used to describe the cross over rates. The permeation coefficient is defined as follows⁶⁴ –

$$P = \left(\frac{\ln\left(1 - \frac{2C_r}{C_0}\right) \left(\frac{-VI}{2A}\right)}{t} \right)$$

where C_r is the concentration measured at the receiving reservoir (determined using UV-Vis spectroscopy), C_0 is the active species concentration in the other electrolyte tank (0.5M or 0.9M), V is the volume of the receiving side (1 L), l is the membrane thickness (60-70 μ m), A is the membrane area (25 cm²), and t is the time.

NMR characterization

All NMR measurements were carried out on a Bruker Avance 360 MHz NMR spectrometer. The ¹H-¹³C heteronuclear multiple-quantum correlation spectroscopy (HMQC) measurements were carried out using gradient pulse for selection, incremental resolution of 1024 x 128 and 10 scans each. The samples for NMR spectra acquisition were prepared by dissolving approximately 50 mg of the polymer in 0.85 mL of deuterated dimethylsulfoxide. 35 mL of tetramethylsilane was added as an internal standard to all samples. The NMR spectra are presented in Supplementary Materials **Figs. S13-S15**.

Conclusions

A Ti-Ce ED-RFB was successfully developed for grid-scale energy storage applications for both diurnal load-leveling and LDES (multi-day to multi-week) use cases. This ED-RFB was enabled by a highly permselective AEM separator that exhibited < 0.4% cation crossover over 1000 hours of operation. The ED-RFB exhibited 100% capacity retention over 1300 hours diurnal cycling with >70% energy efficiency. Additionally, it exhibited close to 100% charge retention upon storage at 90% SOC for over 96 hours. Given this level of performance and capacity retention, the Ti-Ce ED-RFB promises to match and surpass the sub-decadal lifetime of Li-ion batteries. The Ti-Ce ED-RFB can be less expensive than DOE cost targets at both system cost and LCOS levels through multiple pathways (that can be deployed in parallel) such as **1)** improved power density, **2)** passive thermal management, **3)** operational automation and **4)** higher utilization rate (i.e., more cycles per year). In summary, the aqueous Ti-Ce ED-RFB incorporating earth-abundant elemental actives can be inexpensively deployed in frequency regulation and demand-response when coupled with an intermittent power source (such as solar or wind) while the modular nature and sub-linear cost scaling enable applications in weak grid and off-grid energy storage applications^{1,2}.

Declarations

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Author contributions

S.S and V.R conceived the Ti-Ce ED-RFB. S.S identified electrolyte compositions, characterized them with the help of C.H and performed ED-RFB tests with the help of Y.Z. Y.Z prepared and characterized the separators used in this study. T.G prepared the cost models with input and help from S.S and V.R. All authors analyzed the data. S.S and V.R wrote the manuscript. All authors edited the manuscript. V.R supervised the project, obtained funding and instrumental facilities.

Competing interests

The authors currently have no financial interests that may be perceived to influence the conclusions presented in this work. The authors are seeking intellectual property protections on aspects of one or

more technologies described in this report through the Office of Technology and Management (OTM) at Washington University in St. Louis (WUSTL) and have filed US Patent Application 16/299,693 and PCT Patent Application WO2020028374A1.

Data Availability

All of the data associated with these studies are represented in the manuscript and supplemental information. The raw data are available from the corresponding author upon reasonable request.

Code Availability

This manuscript does not utilize custom codes or mathematical algorithms.

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Figures

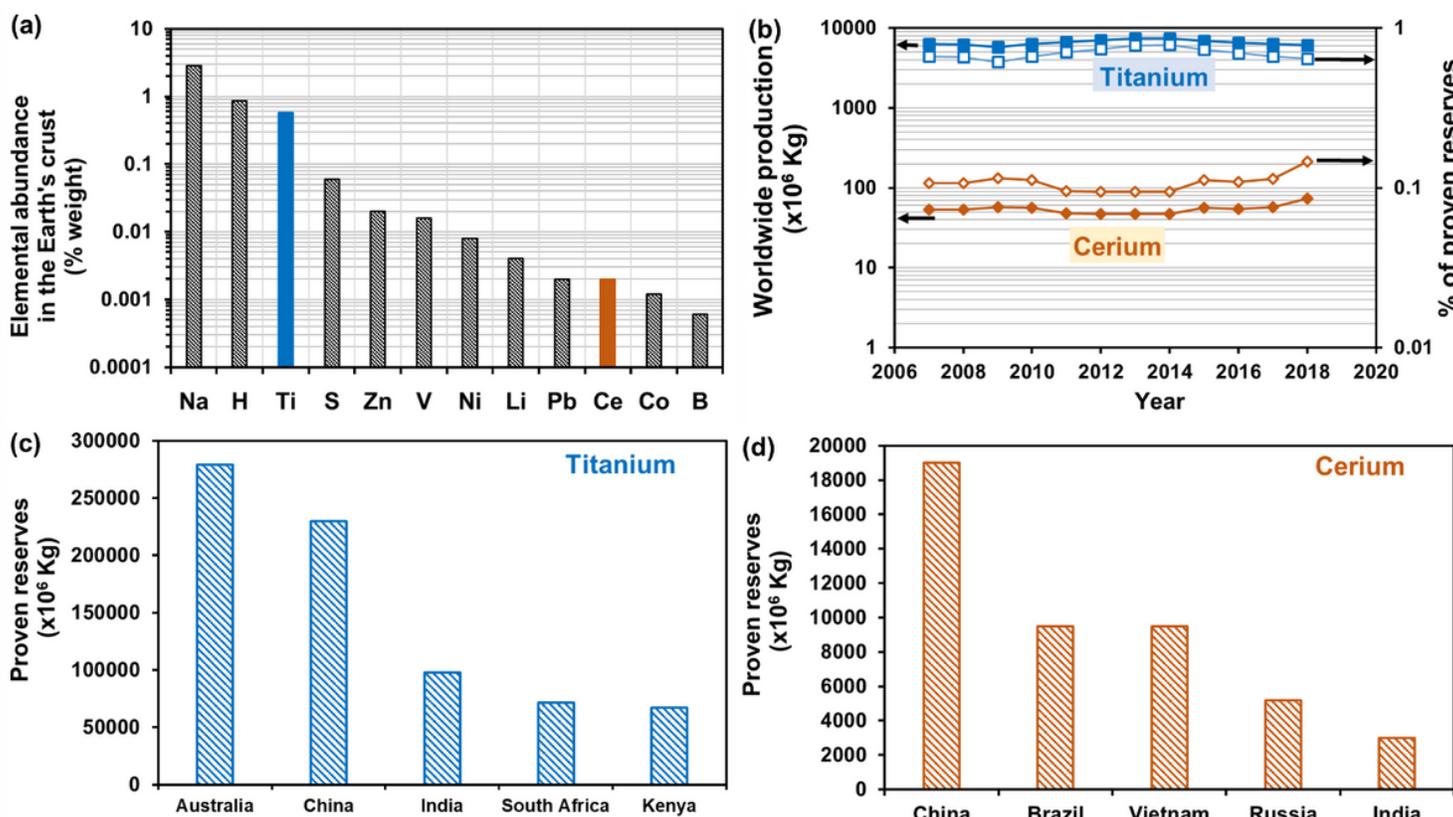


Figure 1

(a) Abundance of some common battery materials in the earth's crust; (b) Yearly production and corresponding rate of reserves exploitation for Ti and Ce over the past decade (c) Countries with top 5 proven reserves of Ti (d) Countries with top 5 proven reserves of Ce.

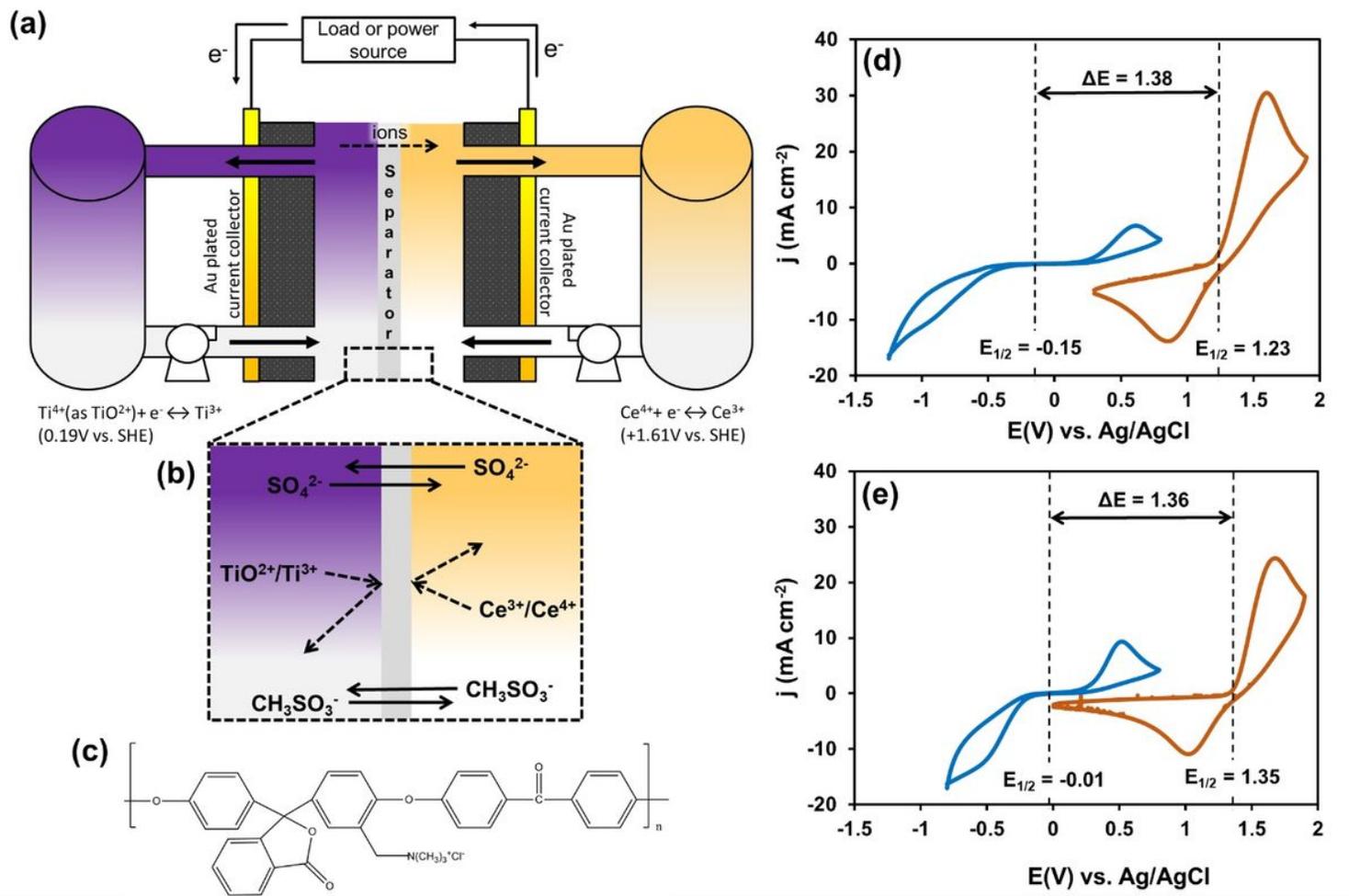


Figure 2

The Ti-Ce electrode-decoupled redox-flow battery (ED-RFB). (a) Schematic of the Ti-Ce ED-RFB, (b) ionic conduction through the anion exchange membrane (AEM) separator, (c) chemical structure of the quaternized cardo-poly(ether ketone) (QPEK-C) AEM separator, (d) cyclic voltammograms of the Ti and Ce active species in H_2SO_4 supporting electrolyte, (e) cyclic voltammograms of the Ti and Ce active species in $\text{CH}_3\text{SO}_3\text{H}$ supporting electrolyte.

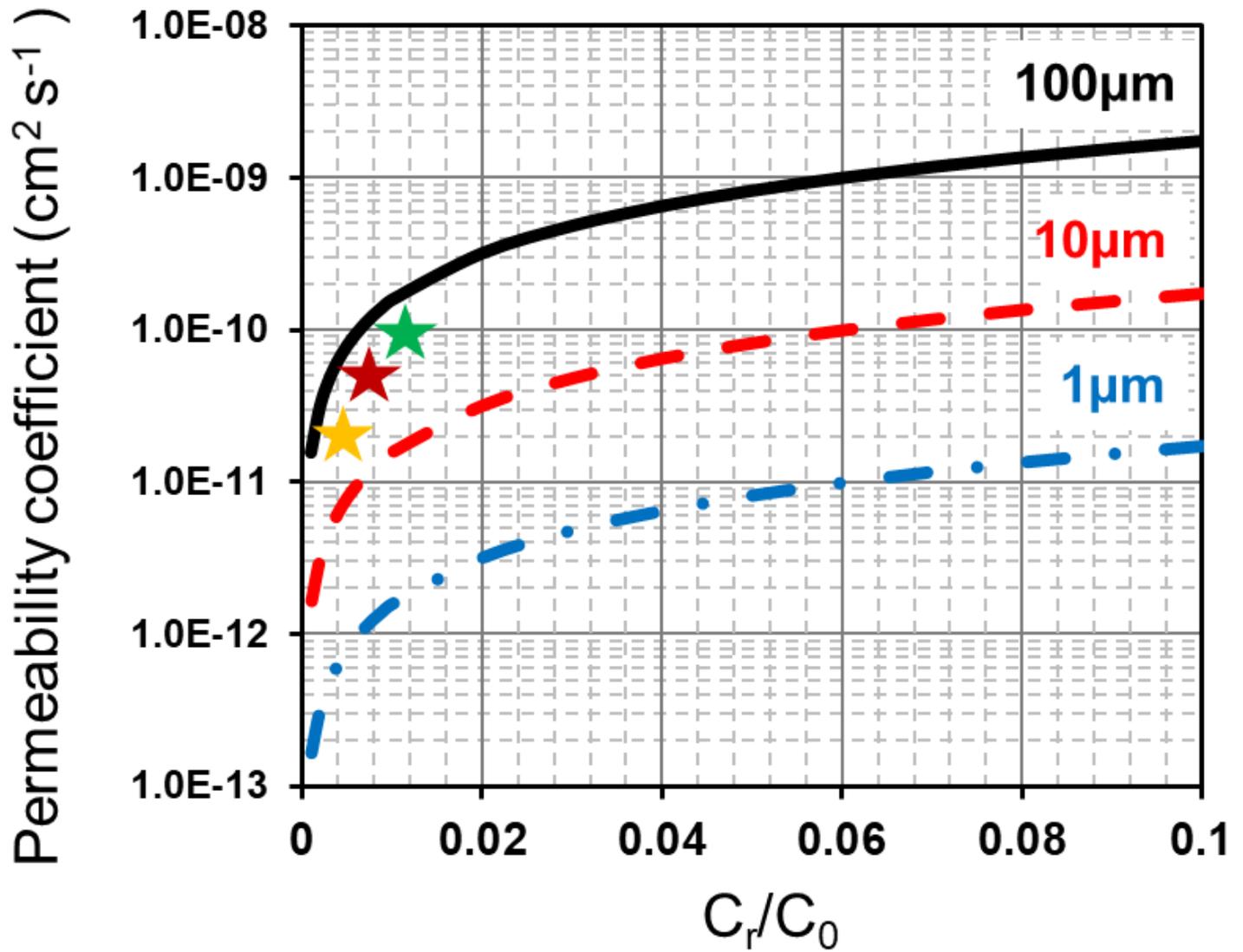
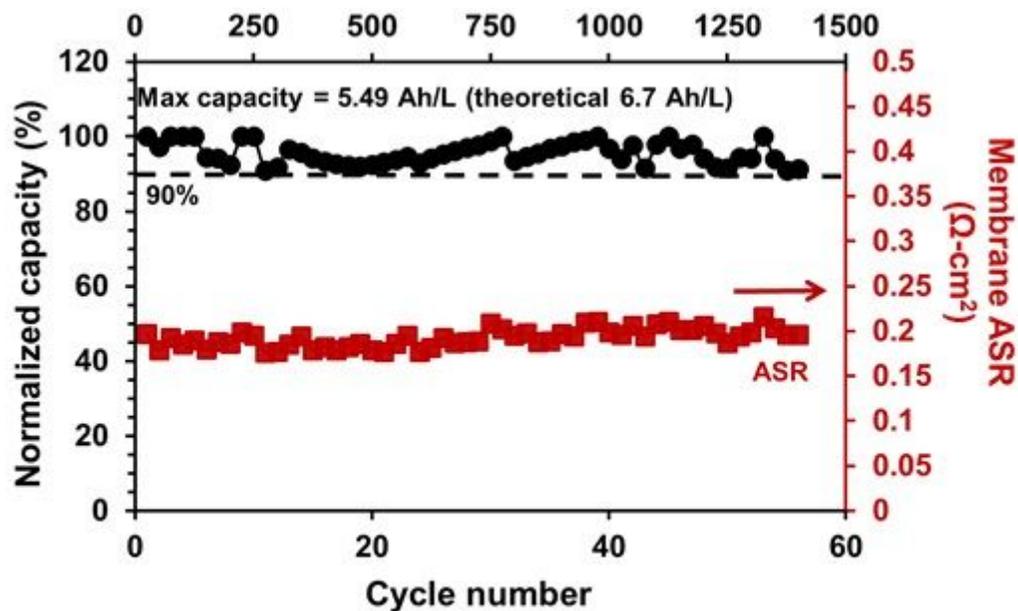
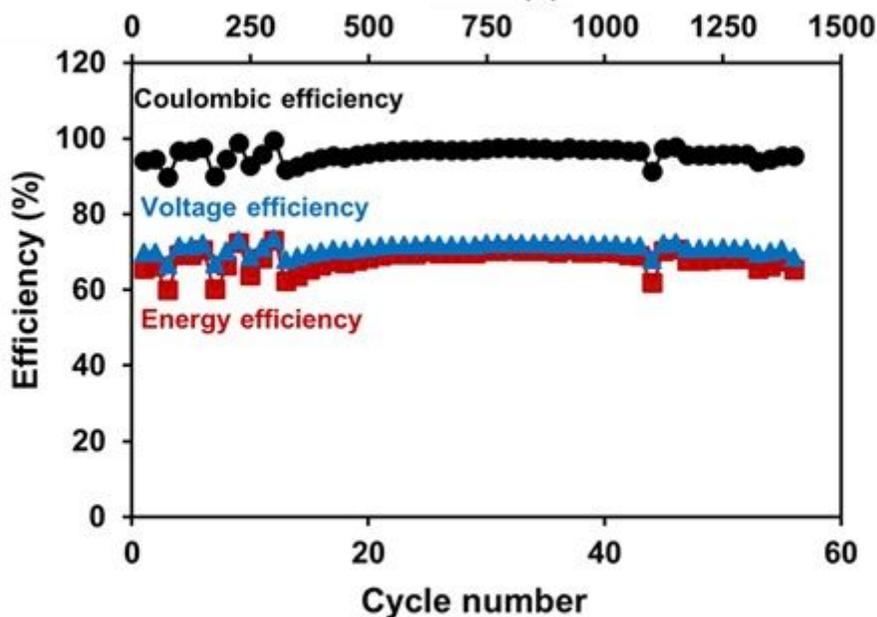


Figure 3

Redox active species permeability coefficient as a function of the ratio between species concentration in the receiving reservoir (C_r) to the species concentration in the source reservoir (C_0). Permeability coefficient across separators of different thicknesses are provided as tie lines. The permeability coefficient across QPEK-C composite membranes with TiO_2 (green star), SiO_2 (red star) and Al_2O_3 (gold star) fillers is provided.



(a)
Time (h)



(b)

Figure 4

Performance of a H₂SO₄ based Ti-Ce ED-RFB with a QPEK-C-TMA + Al₂O₃ separator – (a) Normalized capacity and area specific resistance (ASR) over 1300 hours of cycling (56 cycles); (b) Coulombic, voltage and energy efficiencies corresponding to each cycle in panel (a). Additional cycling data is presented in the Supplementary Materials.

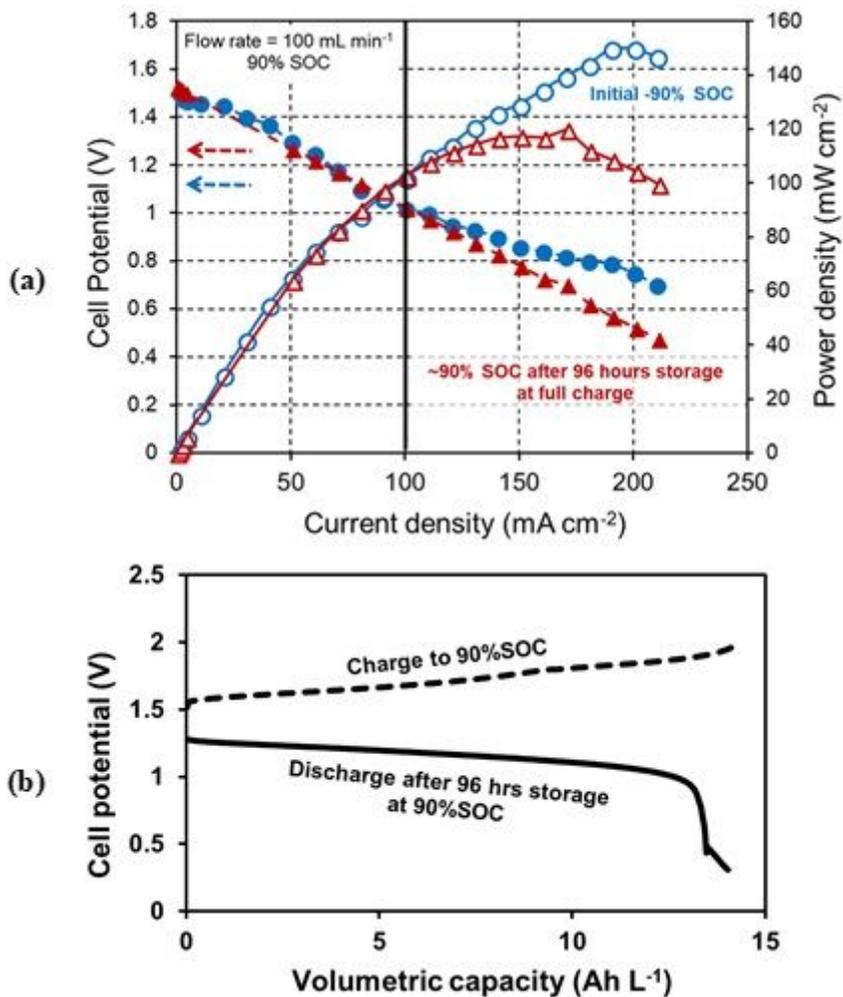


Figure 5

Performance of a CH₃SO₃H based Ti-Ce ED-RFB - (a) Polarization curves before and after extended storage (96 hours) at 90% SOC following long-duration cycling of the Ti-Ce ED-RFB (cycling data shown in Supplementary Materials) (b) Charge-store-discharge curve corresponding to the half cycles before and after storage at 90% SOC. Additional cycling data is presented in the Supplementary Materials.

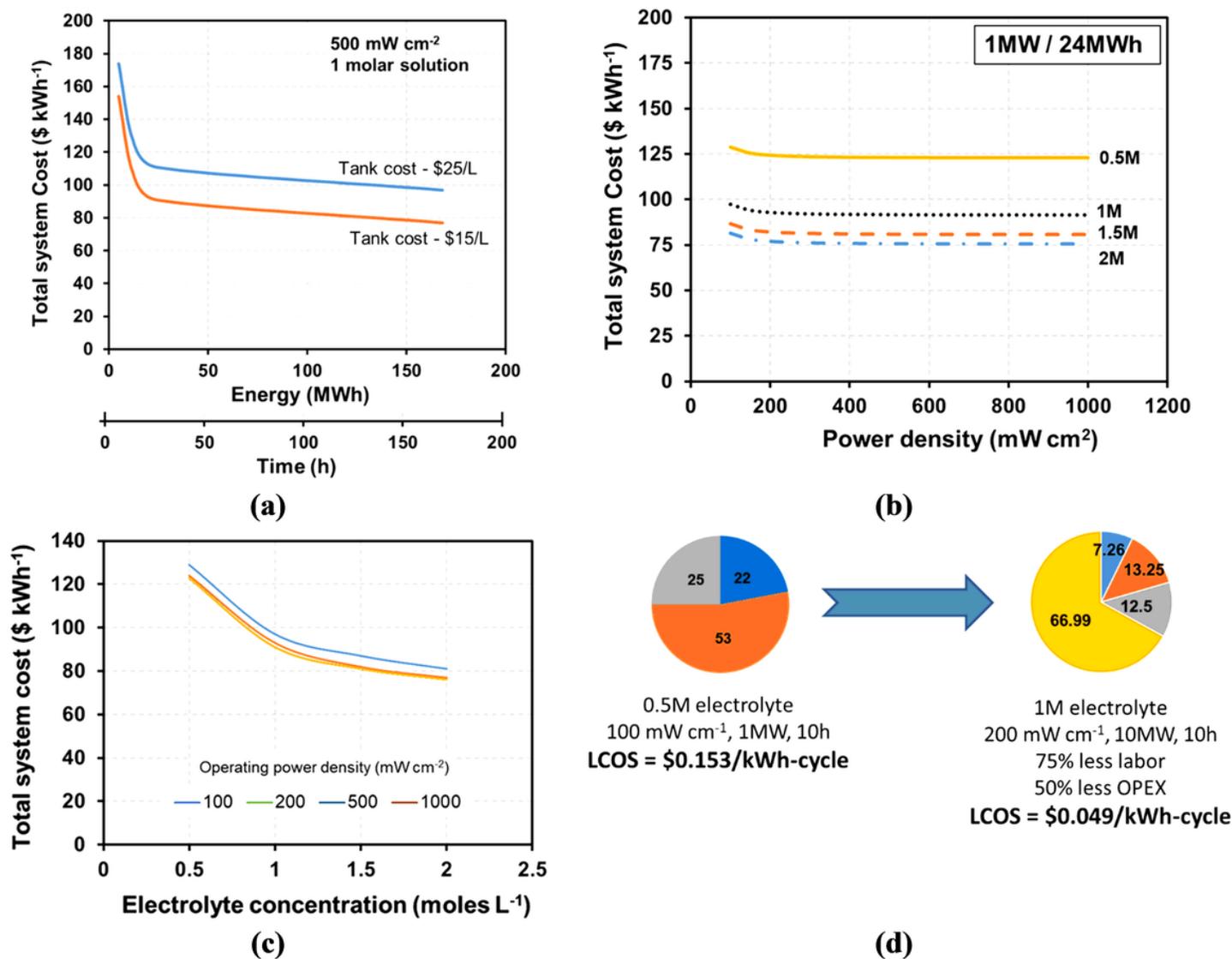


Figure 6

Economics of the Ti-Ce ED-RFB Impact of (a) cycle duration; (b) power density; (c) electrolyte concentration on system installed cost and (d) one (of many) pathway to achieving LCOS < \$0.05/kWh-cycle. All calculations depicted are for the H₂SO₄ based system. Economics of the CH₃SO₃H based system and pathways to LCOS as low as \$0.025/kWh-cycle can be found in the Supplementary Materials.

Supplementary Files

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