

Performance Enhancement of Solar Cooker Integrated with Photovoltaic Module and Evacuated Tubes Using ZnO/Acalypha Indica Leaf Extract: Response Surface Study Analysis

Arulraj Simon Prabu (✉ s.shanmugam1982@gmail.com)

Sriram Engineering College <https://orcid.org/0000-0002-7974-5675>

Venkatesan Chithambaram

PERI Institute of Technology

Sengottaiyan Shanmugan

Koneru Lakshmaiah Education Foundation

Pasquale Cavaliere

University of Salento: Universita del Salento

Shiva Gorjian

Tarbiat Moallem University of Sabzevar: Hakim Sabzevari University

Abderrahmane Aissa

Université Mustapha Stambouli Mascara: Universite Mustapha Stambouli Mascara

Abed Mourad

Université Mustapha Stambouli Mascara: Universite Mustapha Stambouli Mascara

Pokkunuri Pardhasaradhi

Koneru Lakshmaiah Education Foundation

Rajamanickam Muthucumaraswamy

SVCE: Sri Venkateswara College of Engineering

Fadi Abdelmonem Elsayed Essa

Kafrelsheikh University

Ammar Hamed Elsheikh

Tanta University

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2 **Evacuated Tubes Using ZnO/Acalypha Indica Leaf Extract: Response Surface Study**
3 **Analysis**

4 **Arulraj Simon Prabu^{1,2*}, Venkatesan Chithambaram³, Sengottaiyan Shanmugan^{4*}, Pasquale**
5 **Cavaliere⁵, Shiva Gorjian⁶, Abderrahmane Aissa⁷, Abed Mourad⁷, Pokkunuri Pardhasaradhi⁸,**
6 **Rajamanickam Muthucumaraswamy¹, Fadl Abdelmonem Elsayed Essa⁹,**
7 **Ammar Hamed Elsheikh¹⁰**

8 ¹ Research Centre of Mathematics, Sri Venkateswara College of Engineering, 602 105, Sriperumbudur, India.

9 ²Department of Electronics and Communication Engineering, Sriram Engineering College, Perumalpattu, Chennai,
10 Tamil Nadu, India – 602024.

11 ³ Department of Physics, Peri Institute of Technology, Tambaram, Mannivakkam, Tamil Nadu 600048, India.

12 ⁴Research Centre for Solar Energy, Department of Physics, Koneru Lakshmaiah Education Foundation, Green
13 Fields, Guntur District, Vaddeswaram, Andhra Pradesh 522502, India.

14 ⁵Department of Innovation Engineering, University of Salento, 73100, Lecce, Italy.

15 ⁶Biosystems Engineering Department, Faculty of Agriculture; and Renewable Energy Department, Faculty of
16 Interdisciplinary Science & Technology, Tarbiat Modares University (TMU), Tehran, Iran.

17 ⁷Laboratoire de Physique Quantique de La Matière Et Modélisation Mathématique (LPQ3M), Université Mustapha
18 Stambouli de Mascara, Mascara, Algeria

19 ⁸Dept of ECE, Koneru Lakshmaiah Education Foundation, Green Fields, Guntur District, Vaddeswaram,
20 Andhra Pradesh 522502, India.

21 ⁹ Mechanical Engineering Department, Faculty of Engineering, Kafrelsheikh University, Kafrelsheikh 33516, Egypt.

22 ¹⁰Department of Production Engineering and Mechanical Design, Faculty of Engineering, Tanta University, Tanta
23 31527, Egypt.

24 ***Emails IDs:*** (Simon) simonprabu07@gmail.com, (Chithambaram) chithambaramv@gmail.com,

25 (Shanmugan) s.shanmugam1982@gmail.com, (Cavaliere) pasquale.cavaliere@unisalento.it,

26 (Shiva) Gorjian@modares.ac.ir, (Aissa) a.aissa@univ-mascara.dz, (Abed) mourad.abed@univ-mascara.dz,

27 (Pardhasaradhi) pspokkunuri@gmail.com, (Muthucumaraswamy) msamy@svce.ac.in,

28 **(Essa)** fadlessa@eng.kfs.edu.eg, (Ammar) ammar_elsheikh@f-eng.tanta.edu.eg.

29
30 ***Corresponding authors, E-mail addresses:**

31 (Simon) simonprabu07@gmail.com,

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36 **Abstract**

37 In this study, the effect of employing ZnO/Acalypha Indica leaf extract (ZAE) on the energy
38 absorption of a coated portable solar cooker have been examined using an experimental setup. A
39 prototypical model has been developed to corroborate in associating an investigative outcome per
40 constituents of the experiments. The studied heat transfer process in ZAE is stable for harsh
41 conditions. The design analysis and an estimation of the system performance were done given
42 various parameters including the pressure of the vacuum envelope, bar plate coating digestion,
43 emissivity, and solar rays. The fabricated solar was tested with and without ZAE to investigate the
44 impact of this coating material on the solar cooker's thermal performance. To observe the
45 performance of the new design, two figures of merit (F_1 and F_2) have been introduced. The factual
46 food cooking assessments were for a family of four people, which operated in ZAE coating (0.8,
47 1.0, 1.2 μm) of the solar cooker. The values of F_1 and F_2 for the proposed cooker were obtained as
48 0.1520 and 0.4235, respectively, which is intact with the BIS values. The results revealed that
49 employing ZAE instead of a thermal NHC - PV solar cooker reduced the time required to boil 2 L
50 of water for about 2,820 seconds. The overall thermal energy productivity of the solar cooker with
51 electrical backup was obtained as 42.65%, indicating that the ZAE coating can improve the thermal
52 efficiency by 10.35%.

53 **Keywords:** Electrical backupz Evacuated tubes; Photovoltaic panel; thermal model; Solar cooker

54

55 **1 Introduction**

56 A solar cooking process is a method in which solar radiation is utilized to naturally cook
57 substances. Research worldwide have found out that solar cookers have sustainability for cooking
58 in rural and urban areas with reduced energy consumption. A solar cooker using sun radiation as
59 a heat source, can be utilized on hot sunny days, but on rainy and winter days it is useless. It has
60 been found that a solar cooker with an electrical backup will overcome these inconveniences. An
61 electric backup integrated with a solar cooker has shown better performance compared to the
62 cooker supported with thermal energy alone. Moreover, selectively coated absorbers using
63 nanoparticles play an important role in enhancing the performance of solar cookers. Several studies
64 have assessed the effect of selective absorber coating using nanoparticles. Kaiyen et al. (2009)
65 used a light funnel to congregate solar energy to achieve temperature suitable for industrial and

66 domestic usage. It was identified that a temperature of 250 °C is achieved with a lighting area of
67 1.5 m². Prasanna and Umanand (2011) experimented by transferring solar energy to the kitchen
68 using fluid circulation to stimulate a cooker using the concept of maximum power point tracking
69 (MPPT) for a thermal collector. Javadi et al. (2013) also reviewed the effect of using nanofluids
70 on the performance of solar collectors. In their review, care was taken to highlight the impact of
71 two-phase analysis of the nanofluid with more than one nanoparticle in the heat transfer
72 fluid. Hussein et al. (2017) reviewed theoretical, numerical, and experimental studies of a heat
73 pipe solar collector incorporating a nanofluid. They reported that various research works have
74 proved the significance of nanofluid in improving the thermal performance and efficiency of solar
75 collectors. Palanikumar et al. (2019) fabricated a solar box-type cooker (SBC) including a phase
76 change material (PCM) and nanoparticles coating in the design and evaluated its performance with
77 thermal imaging of the structure. Then, they used a fuzzy logic algorithm to develop a model to
78 predict the thermal performance of the solar cooker. The results of the study revealed that when
79 eggs are boiled, the thermal performance of the solar cooker can reach 52.17% and 75.47%,
80 utilizing PCM and nanoparticles, respectively.

81 Furthermore, Bhavani et al. (2019) designed an SBC and coated it with black paint and
82 nanoparticles. Then the design was evaluated using fuzzy logic rules. From the results, it was found
83 that using nanoparticles in the coating enhances the thermal efficiency of the solar cooker by
84 7.10%. The fuzzy logic rules have also been utilized in other studies to model solar cookers. Such
85 as Palanikumar et al. (2021) and Venugopal et al. (2012). Thamizharasu et al. (2022) developed a
86 stepped SBC (SSBC) coated with silicon dioxide (SiO₂) and titanium dioxide (TiO₂) nanoparticles
87 and analyzed them at different volume fraction ratios of nanoparticles between 5% to 25%. The
88 findings indicated that the overall thermal efficiency of the solar cooker can be improved by
89 31.42% when using the SiO₂/TiO₂ nanolayers at 15% volume fractions of nanoparticles. In another
90 study by Thamizharasu et al. (2021) the solar cooker was analyzed using an adaptive control
91 method which was modeled using the online sequential extreme learning machine (OSELM), and
92 the heat analysis of the system was made in the Binary Search Tree data structure. From the results,
93 the efficiency of the solar cooker was obtained as 49.21% for a 15% volume fraction of SiO₂/TiO₂.

94 Palanikumar et al. (2021) performed a comparative study on a fabricated SBC, this include an SBC
95 with PCM, and an SBC with PCM and a nanocomposite (NPCM). After analysing the fuzzy logic
96 and Cramer's rules, image processing techniques were applied. The results indicated that coating

97 the bar plate absorber with nanoparticles and integrating a PCM increases the internal temperature
98 of the SBC up to 164.12 °C, and enhance the overall thermal efficiency by 11% compared to the
99 other tested configuration (2019). Palanikumar et al. (2020) studied an SBC coated with a
100 nanocomposite film containing tantalum pentoxide (Ta_2O_5) doped with stannic oxide/Silver. The
101 results indicated that the spectrally selective characteristic is improved and the bar plate
102 temperature reaches 203.33 °C.

103 Shinde et al. (2016) utilized preheated water to increase the thermal efficiency of a large-scale
104 cooker with three levels of screw speed, solid flow rate, and liquid flow rate. The results indicated
105 that the required time for batch cooking is equivalent to the minimum residence time. Cerium
106 oxide (CeO_2) nanoparticles of 25 nm were prepared and combined with heat transfer fluid,
107 including water in different concentrations by Sharafeldin and Gróf (2018). The obtained nanofluid
108 was used in solar evacuated tube collectors (ETCs) to improve thermal performance. It was found
109 that the thermo-optical characteristics were increased by 34%. Khallaf et al. (2020) also fabricated
110 a Quonset solar cooker with dome-shaped polymeric glaze incorporated with internal reflectors
111 and performed experimental and theoretical analysis. The study revealed that cooking fluid
112 glycerine gives efficiency ranging from 9% to 92% during cooking hours. The solar cooker's
113 energy and exergy efficiencies with multiwalled carbon nanotube-oil nanofluid were investigated
114 with varying volumetric flow rates by Hosseinzadeh et al. (2021). It was found that nanofluid-
115 based solar cooker gives improved efficiency of 37.30% and 65.87% for 0.2% and 0.5% wt
116 concentration in oil, respectively. Mallikarjuna et al. (2021) reviewed the effect of nanofluids to
117 enhance the heat transfer rate in solar energy harvest. The results of different research works
118 conducted by various researchers have been presented in more detail in their study.

119 Bo Liu et al. (2021) carried out studies using zinc oxide (ZnO), SiO_2 , copper oxide (CuO),
120 aluminum oxide (Al_2O_3), and carbon derivative nanomaterials on copper, silicon, SiO_2 , aluminum,
121 and stainless-steel substrates and found the enhancement of thermal performance of the absorbers
122 due to selective absorber coatings. Alshukri et al. (2018) used micro ZnO and nano CuO
123 nanoparticles with paraffin wax in a solar heat-pipe ETC. The results indicated that the efficiency
124 increases in the range of 33.8% to 45.7%. A comprehensive review regarding the various kinds of
125 nanofluids in ETCs was conducted by Vijayakumar et al. (2021), and conclusions were highlighted
126 with the performance enhancement of the ETCs. Vengadesan and Senthil (2021) fabricated finned
127 cooking vessels with a variable length of 25, 35, and 45 mm and evaluated them. It was found out

128 that the fin length of 45 mm gives higher thermal efficiency of 50.03% with a heat transfer
129 coefficient of 58.54 W/m²°C. Hosseinzadeh et al. (2021) used different nanofluids in a solar
130 collector and cooking unit and performed energy and exergy analyses. The study indicated that
131 employing silicon carbide (SiC) nanofluid in the system provides good performance in which 2 L
132 of water boiled in 17 min. Shehayeb et al. (2021) employed cathodic electrophoretic deposition to
133 enhance the optical properties of the CuO tandem solar absorber. It was observed that the
134 fabricated tandem absorber provides enhanced efficiency.

135 Based on the reviewed literature presented supra, it is clear that a number of studies have been
136 conducted to assess the impact of nanoparticles on the performance of various solar cookers. This
137 study therefore uses ZnO/Acalypha Indica leaf extract (ZAE) and black mat paint on the sides and
138 bottom of a cooking vessel to enhance its performance. A mathematical model has been proposed,
139 and the validation of the analytically obtained results is obtained through experimental
140 observations. Moreover, two figures of merit F_1 and F_2 were proposed to evaluate the solar cooker
141 performance with and without using ZAE with black mat paint.

142 The rest of the study is presented in the following order, the materials and method used for the
143 study are presented in section 2, section 3 presents the results and discussion, whiles the
144 conclusions made on the study is presented in section 4.

145 **2 Materials and methodology**

146 *2.1 Preparation of Acalypha Indica leaf extract*

147 Fresh Acalypha Indica leaves were collected in March 2021 in Mellampude, Vijayawada - AP,
148 India. The surface of the leaves was cleaned with running tap water to remove the dust and other
149 contaminated organic compounds, followed by distilled water and dried at room temperature for
150 15 days (total count of 1,000 leaves). The dried leaves were collected and then about 30 g of the
151 collected leaves were taken and mixed with 300 mL of distilled water. The prepared sample was
152 then heated and stirred at 50 °C for 3 h. The solution was boiled at 70 °C for 20 min. The color of
153 the solution changed to green which indicates the formation of a leaf extract. The obtained solution
154 was filtered with Whatman No. 1 sieve paper to obtain a clear extract. Then Acalypha Indica
155 extracts were filtered two times and pure samples were collected and maintained at 5 °C. The
156 extract samples were prepared to be directly utilized in synthesis experimentations as shown in
157 **Fig. 1(a)**.

158

159 2.2 Preparation of ZnO using *Acalypha Indica* leaf extract (ZAE)

160 The experimental materials were prepared and all chemical materials were purchased from the
161 company AR Scientific, Basaveshwara Layout, Bengaluru, and Karnataka 560094. Zinc acetate
162 dihydrate (99.7%) and ethanol (99.5%) chemicals as standard cleaning agents in experimental
163 works were obtained from the Research Centre for Solar Energy at Vijayawada civic KLEF India.
164 A 2 g nickel nitrate ($\text{Ni}(\text{NO}_3)_2$) was added to 200 mL of distilled water and allowed to stir for 20
165 min. The solution was added in drops to the leaf extract under constant stirring for 2 h using a
166 magnetic stirrer (Ghamsari et al, (2019); Alamdari et al, (2019); Alamdari et al, (2017); Alamdari
167 et al, (2015); Vafae et al, (2011) as shown in **Fig. 1(b)**. The solution was then dried on a hot plate
168 to obtain a powder form. Finally, the nickel oxide (NiO) sample was prepared. The powder was
169 then placed in a muffle furnace at a temperature of 500 °C for 3 h in ZnO/*Acalypha Indica* stem
170 extract, as shown in **Fig. 1(c)**. The obtained sample can be used in further studies. **Fig. 1(d)** shows
171 this process and the establishment of chemical bonds structure and extracted with particles of ZnO
172 using *Acalypha Indica* Leafs.

173 2.3 Characterizing of ZnO/ *Acalypha Indica* extract

174 2.3.1 X-ray diffraction

175 **Fig. 2(a)** shows the X-ray diffraction (XRD) pattern of NiO nanoparticles (NiO-Z)
176 prepared using *Acalypha Indica* leaf and stem extract (AE). In the XRD analysis, the x-axis
177 represents 2θ , and the y-axis indicate the intensity of the peak. The presence of 2θ for ZAE
178 corresponds to (1 1 1), (2 0 0), (2 2 0), and (3 1 1) & (1 1 1), (2 0 0), (2 2 0), (3 1 1), and (2 2 2)
179 orientation confirms the presence of NiO particles in a cubic structure. The grain size (D) of the
180 nanoparticles was calculated using the Debye-Scherrer formula using the reflection form of the
181 XRD pattern. Debye-Scherrer formula for grain size is presented in Eq. (1):

$$182 D = 0.9\lambda / \beta \cos\theta \quad (1)$$

183 where D is the grain size, λ is the wavelength of copper (1.54\AA), β is the full width half maximum
184 after correcting the instrument peak broadening (β expressed in radians), and θ is the Bragg's
185 angle. In this XRD analysis, the grain size of NiO using ZAE was calculated as 20.61938×10^{-9} m
186 and 22.3126×10^{-9} m, respectively. The Lattice Parameter (a) was calculated using Eq. (2):

$$187 a = d\sqrt{(h^2+k^2+l^2)} \quad (2)$$

188 where d is the interplanar spacing value; h , k , and l are Miller indices. The Lattice Parameter of
189 ZAE has been calculated as 4.20825\AA and 4.17629\AA . The Cell Volume (a^3) is calculated from the
190 value of Lattice Parameter (a). Therefore, the value of the Cell Volume for ZAE is calculated as
191 $52.544 (\text{\AA}^3)$ and $72.84033 (\text{\AA}^3)$.

192 2.3.2 Fourier Transform Infrared Spectroscopy (FTIR) analysis

193 Fourier Transform Infrared Spectroscopy (FTIR) is a technique use to obtain an infrared spectrum
194 of absorption or emission of a solid, liquid, or gas. An FTIR spectrometer simultaneously collects
195 high spectral resolution data over a wide spectral range. The Fourier Transform Infrared
196 Spectroscopy (FTIR) investigation was carried out using PERKIN ELMER (Spectrum RXI)
197 spectrometer in 400 cm^{-1} to 4000 cm^{-1} . The functional groups were identified using the peaks
198 assignments. **Fig. 2(b)** shows the FTIR spectrum of nickel oxide nanoparticles using ZAE in **Table**
199 **1**.

200

201 2.3.3 Analysis of UV Spectrum

202 This study mixed the Nickel nitrate source with the plant extract of the Acalypha Indica leaf and
203 stem extract. The color of the AE changes from brown to dark green, the color of NiO (Z) also
204 changes from yellow to light green. These color changes are due to the excitation of surface
205 Plasmon vibrations. The UV-visible spectrum x-axis indicate wavelength whiles the y-axis
206 indicate absorption. AE represents nickel oxide (Ni_2O_3) nanoparticles using Acalypha Indica Leaf
207 extract in the UV spectrum, and Z represents ZAE. In this spectrum, the range of Ni_2O_3
208 nanoparticles using leaf and stem extract was reported in the range of 293 nm and 291.3 nm as
209 shown in **Fig. 2(c)**. The corresponding absorptions are also identified. It indicates the possibility
210 of the formation of Nickel Oxide nanoparticles, and in this spectrum, comparing the two ranges,
211 we observed that the AE is better than ZAE.

212 2.3.4 SEM and EDAX analyses

213 The surface morphology of the resulting powder was examined using a scanning electron
214 microscope. **Fig. 2(d)** indicates that AE and ZAE were observed within the range of $\times 10,000$ and
215 $\times 10,000$. The image shows that the morphology of Ni_2O_3 nanoparticles is a spherical shape for
216 AE and in coral reef structure for ZAE without any agglomeration in nano size. From the EDAX
217 (Energy Dispersive X-Ray Analysis) spectrum image, elements in the Acalypha Indica leaf and

218 stem extract are evident. The EDAX spectrum of nickel oxide nanoparticles were used, while that
219 of ZAE shows only the peak of nickel (Ni) and Oxygen (O₂) elements. ZAE shows only the peak
220 of nickel (Ni), and oxygen (O) elements, which confirms that the prepared nickel nanoparticles are
221 essentially free from impurities and are at the limit of EDAX. Identification lines for the significant
222 emission energies for Ni, O₂ and thus correspond with the peak in the spectrum; thus, nickel has
223 been identified correctly as shown in **Fig. 2(e)**. The AE atomic weight percent values of Ni, O
224 have been absorbed, 38.98, 57.79. The ZAE atomic weight percent values of Ni, O that have been
225 observed are 41.98, 55.17.

226

227 *2.4 Design of the solar cooker*

228 The compatible solar cooker has three components with evacuated tubes with a high vacuum ($P <$
229 5×10^{-3} m bar) enclosed in a rectangular wooden box with parabolic trough reflectors (PTRs)

- 230 ➤ Solar photovoltaic (PV) panel (2 x 100W);
- 231 ➤ 12 V 75AH Battery;
- 232 ➤ Stove with two vessels for cooking.

233 A compatible solar cooker with a PV panel and evacuated tubes (Solar Chulha) was designed and
234 fabricated. Evacuated tubes have a high vacuum ($P < 5 \times 10^{-3}$ Pa) used in the proposed cooker, and
235 it is used to produce hot water of about 75°C for cooking. PTRs were designed, and the evacuated
236 tubes were fixed on the focal line of the trough to receive maximum solar radiation. The copper
237 tubes carrying the heat transfer fluid (water) were made to run through the evacuated tubes to
238 extract the thermal energy received by the tube. The temperature of the heat transfer fluid at the
239 outlet was high. A PV panel with a power output of 200 W was used to charge a 12V 75 AH
240 battery. The electricity drawn from the battery was used to heat the heating filament (Nichrome)
241 covering the cooking vessel. Hot water from the evacuated tubes was further heated up to the
242 boiling point, and the food was cooked quickly. The DC power produced by the panel was stored
243 in the battery during the daytime to be used at night. **Fig. 3(a)** and **Fig. 3(b)** show the solar cooker's
244 photograph and its different components. Among the two cooking vessels, one vessel was coated
245 with ZAE and mat black paint on the sides and base of the cooking vessel, and the other vessel
246 with only black mat paint.

247

248 2.5 *Experiment performance*

249 Two cooking vessels are used with and without coated ZAE sides in which the vessel's bottom,
250 was subjected to stagnation temperature test without any load in the vessel. The cooking vessels
251 by the bottom (base) and the absorber were allowed to absorb thermal energy via the sides and
252 bottom of the vessel. Thermal energy was produced by the Nichrome heating coil and conducted
253 through the sides and bottom of the vessel, coated with black mat paint with and without ZAE.
254 The experiments were carried out to find the figure of Merit F_1 , which is a function of stagnation
255 temperature. F_1 is calculated from the Standard formula presented in Eq. (3) (Alamdari et al
256 (2019)):

257
$$F_1 = \frac{T_{bs}-T_a}{H} \quad (3)$$

258 **Table 2** represent the variation of temperature at the base of the two cooking vessels with and
259 without ZAE. The observed first figure of merit (F_1) for the cooking vessels with and without ZAE
260 was 0.1520 and 0.1143, respectively. Due to the enhanced heat transfer from Nichrome heating
261 coil to the sides and base of the cooking vessel with a coating of ZAE along with black mat paint,
262 and also, the thermal stability of ZAE led to a good thermal conduction of the thermal energy
263 transferred to the cooking vessel, as shown in **Fig. 4(a)**.

264 From the graph, the temperature of the cooker's base with ZAE with black mat paint is noticeable
265 throughout the path towards the stagnation temperature of 133°C compared to the vessels without
266 ZAE. According to the Bureau of Indian Standard, the F_1 value of 0.12 km²/W is significant, and
267 in the present cooker, the value is 0.1520 km²/W. A Figure of Merit (F_2) was found by
268 experimenting with the proposed solar cooker with load (sensible heat material), i.e., 1 kg of water
269 in the cooking vessels with and without a coating of ZAE on the sides of the bottom of the vessel.

270

271 2.5.1 *Second Figure of Merit (F_2)*

272 The cooker performs based on the sensible heating of a load inside. The proposed cooker was filled
273 with a sensible load of 1 kg of water in the two cooking vessels with and without a coating of ZAE
274 and black mat paint on the sides and bottom of the vessel. F_2 can be calculated using the expression
275 presented in Eq. (4):

276
$$F_2 = \frac{F_1(MC)_w}{A(t_2-t_1)} \ln \left[\frac{1-(1/F_1)((T_{w1}-T_a)/H)}{1-(1/F_1)((T_{w2}-T_a)/H)} \right] \quad (4)$$

277 Measurements were done to find the second figure of merit, and they are:

- 278 (i) Cooking fluid temperature at a regular time interval until the fluid temperature reaches
279 a maximum of 95°C.
- 280 (ii) Duration of time between the initial and final cooking fluid temperature
- 281 (iii) The intensity of solar radiation and ambient temperature were measured using a solar
282 radiation monitor and digital thermometer.

283 **Table 3** characterizes the data collected from the measurements made during the testing for the
284 Second Figure of the Merit of the solar cooker.

285

286 2.5.2 Interval Cooking Power (P)

287 It is also called average cooking power (P) which means the helpful energy available during the
288 cooking period. It is defined as the ratio of increase in temperature of the cooking fluid for each
289 interval of time multiplied by the mass and specific heat of the cooking fluid to the time interval
290 specified, and the expression given as indicated in Eq. (5).

$$291 \quad P = \frac{(MC)_w(T_2 - T_1)}{600} \quad (5)$$

292 2.5.3 Standardized cooking power (P_s)

293 Standard solar insolation of 750 W/m² for each interval has been used, and utilizing Interval
294 cooking power (P), the standardized Cooking Power (P_s) can be evaluated using Eq. (6).

$$295 \quad P_s = \frac{P \times 750}{H} \quad (6)$$

296 **Table 4** represents the variation of interval cooking power and standardized cooking power during
297 the testing load for the second figure of merit.

298 From **Fig. 4(b)**, it is understood that the standardized cooking power is a function of Interval
299 Cooking Power (P) and is inversely proportional to the intensity of solar radiation during the
300 interval of time. Interval cooking power is the functional difference in initial and final temperature
301 during the time interval with a standard intensity of solar radiation of 600 W/m². Moreover, the
302 standardized cooking power has a conjoint trend concerning the interval cooking power at each
303 time interval with power less than that of the interval cooking power.

304

305 *2.6 Thermal Modeling*

306 Since the cooker is incorporated with the evacuated tube, it can obtain preheated cooking fluid
 307 from the outlet of the evacuated tubes. The temperature of the cooking fluid at the outlet is
 308 considered the initial temperature of the cooking fluid in the cooking vessel. The base and sides of
 309 the cooking vessel are surrounded by the Nichrome heating coil, which receives the current from
 310 the solar panels of 200 W each. The base and sides of the cooking vessel are coated with ZAE to
 311 enhance the heat conduction of the vessel to deliver the auxiliary heat to the preheated cooking
 312 fluid. Since the nanoparticles play a vital role in transferring the heat from the nichrome heating
 313 coil to the cooking fluid, it will reduce the cooking time for the foodstuff reasonably. Here, energy
 314 balance equations have been written for the cooking fluid, base and sides of the cooking vessel
 315 and solved for the analytical solution.

316 *The base of the cooking vessel:*

$$317 P_e A_b \times t + T_{out} A_b S M = h_{bs} A_b (T_b - T_a) + h_{cbcf} (T_b - T_w) \quad (7)$$

318 *Sides of the cooking vessel:*

$$319 P_e A_s \times t + T_{out} A_s S M = h_{bs} A_s (T_s - T_a) + h_{cscf} (T_s - T_w) \quad (8)$$

320 The outlet water from the evacuated tube into the cooking vessel absorbs energy given by the
 321 Nichrome heating coil through the base and sides of the cooking vessel. Since the base and sides
 322 of the cooking vessel are coated with ZAE, heat energy is convected to the preheated cooking
 323 fluid. Due to an effective heat transfer from the Nichrome heating coil to the cooking fluid through
 324 the ZAE coated base and sides of the cooking vessel, the cooking fluid absorbs much more energy.
 325 The temperature of the fluid increases rapidly. As a result, the time for cooking the food in the
 326 proposed cooker is reduced.

327 *The lid of the cooking vessel:*

$$328 h_{cfl} (T_w - T_l) = h_{la} (T_l - T_a) \quad (9)$$

329 *Cooking fluid*

$$330 M_w C_w \frac{dT_w}{dt} + h_{cbcf} (T_b - T_w) + h_{cscf} (T_s - T_w) = h_{cfl} (T_w - T_l) \quad (10)$$

331 Eqs. (7), (8), and (9) have been solved for T_b , T_s , and T_l , and substituted in Eq. (10). Rearranging
 332 Eq. (10) and can be written as

$$333 \frac{dT_w}{dt} + a T_w = f(t) \quad (11)$$

334 where a and $f(t)$ are constants, this can be obtained from the equations on temperature components
 335 of the evacuated tube collector, Nichrome heating coil, and cooking vessel. At $t=0$, $T_w = T_{w0}$, and
 336 due to the initial condition, we can write the solution of the equation as

$$337 \quad T_w = \frac{f(t)}{a}(1 - e^{-\alpha t}) + T_{w0}e^{-\alpha t} \quad (12)$$

338 where α is a constant and depends on the different heat transfer coefficients of the cooker. The
 339 photovoltaic with evacuated tubes which connects the nichrome heating coil utilized in the solar
 340 cooker's input and output has been calculated and the overall energy efficiency (η_{ZAE}) can be
 341 written as presented in Eq. (13)

$$342 \quad \eta_{ZAE} = \frac{E_{NHC,out,ave} - \frac{E_p}{\eta_{pv}}}{A_{sc} \int_{t_1}^{t_2} H dt} \quad (13)$$

343

344 **3 Results and Discussion**

345 This research work is focused on the effect of the presence of ZAE coating and its thickness on
 346 the thermal performance of a solar cooker.

347 *3.1 Effect of ZAE coating thickness*

348 An experiment was carried out with the proposed cooker during summer and winter days under
 349 local climatic conditions of Vijayawada, Andhra Pradesh, India. The analytical solutions of the
 350 energy balance equations for the temperature elements of the cooker were used to evaluate the
 351 temperature of the base, sides, and lid of the cooking vessel, followed by the temperature of the
 352 cooking fluid. The climatic parameters during the experiment were recorded using the solar
 353 radiation monitor and digital thermometer. Calibrated copper-constantan thermocouples were used
 354 to measure the temperature of the cooker.

355 The impact of varying the thickness of the ZAE coating on the performance of the solar cooker
 356 and the overall thermal efficiency was investigated, where tested thicknesses are 0.8-micron, 1.0-
 357 micron, and 1.2-micron. It was found that the coating thickness with the best absorption solar
 358 energy and ambient temperature on the design is 1 micron of the ZAE material. The performance
 359 of the solar cooker with a 1.0-micron coating was measured and analyzed from June 2020 to June
 360 2021. The solar cooker with a one-micron thickness coating of ZAE was absorbed in more solar
 361 radiation and ambient temperature during experimental average values compared to others with
 362 different thickness levels. KLEF climate conditions utilization of the solar cooker has improved

363 performance in more absorption by solar radiation around 25W/m^2 and ambient temperature is
364 4°C , individually.

365 *3.2 Effect of the presence of ZAE coating*

366 An output thermal influence analysis of a design was utilized. We are focused on the best-
367 performing thickness which was chosen as one micron as demonstrated in **Fig. 5(a)**. Cooking
368 vessels with and without the ZAE coating (one micron) were filled with 1 kg of water. The
369 experimental work was performed until the temperature of the sides and base of the cooking vessel
370 reached its stagnation temperature. **Fig. 5(b)** represents the variation of the temperature of the
371 cooking vessel's side, base, and lid. The base and sides of the vessels with and without ZAE were
372 experimented for their activity to find the impact of ZAE coating. From the figure, it is observed
373 that the temperature of the vessel with a coating of ZAE has dominated temperature at each
374 measurement in regular intervals and proved that the ZAE enhanced the conduction of thermal
375 energy from the Nichrome heating coil to the base and sides of the cooking vessel. Moreover, ZAE
376 has a significant capacity to transfer heat energy to the cooking fluid through the base and sides of
377 the cooking vessel. Furthermore, validation of the model was performed for the temperature of
378 the base, sides, and lid of the cooking vessel with the analytical solutions obtained by solving the
379 energy balance equations of the temperature elements of the cooker.

380 **Fig. 5(c)** shows the variation of the theoretical and experimental values of the temperature of the
381 base, side, and lid of the cooking vessel with a coating of ZAE. It was observed that both the
382 theoretical and experimental values have a conjoined trend with maximum coincidence. Standard
383 deviation between the experimental and theoretical values ensures the validation of the model. For
384 the temperature of the base, side, and lid of the vessel, the standard deviation values between the
385 experimental observation and theoretical values were 0.025, 0.109, and 0.0416, respectively. The
386 mathematical model calculated precise values for temperature elements of the cooker which agree
387 with the experimental observations.

388

389 *3.3 Experimental and theoretical cooking values analysis*

390 The cooking fluid's temperature was used to find the theoretical values and compared with the
391 experimental observations by finding the standard deviation between the experimental and
392 theoretical values. **Fig. 5(d)** represents the variation of the experimental and theoretical values of

393 cooking fluid temperature concerning that of time with a load of 1 kg of cooking fluid in the
394 cooker.

395 Preheated water from the ETC with a temperature of 76°C entered the cooking vessel. The
396 temperature of the preheated water was taken as the initial temperature of the cooking fluid in the
397 cooking vessel with a coating of ZAE on the sides and the base. The preheated water reached a
398 maximum temperature of 96°C within 15 min with the auxiliary heat obtained from the Nichrome
399 heating coil through the base and sides of the cooking vessel. The energy balance equation for the
400 cooking fluid was considered to evaluate the temperature of the cooking fluid during the cooking
401 time. The theoretical values for the temperature of the cooking fluid were compared with the
402 experimental observation by finding the standard deviation between them. From the graph, it is
403 clear that both the experimental and theoretical values have conjoined trends throughout the
404 working period. It was found that the average standard deviation between the experimental and
405 theoretical values is 0.16122, which was expected.

406

407 *3.4 Cooking performance*

408 The new design was analyzed for different thicknesses of ZAE coating for a given water
409 temperature inside the solar cooker as shown in **Fig. 6(a)**. The solar cooker's values were recorded
410 during the heating of water (2 L), which was performed with coating with various ZAE
411 thicknesses, the time required for cooking decreased from 102 min to 58 min, 47 min, and 54 min.
412 That is, 58 minutes (0.8 μm), 47 minutes (1.0 μm), and 54 minutes (1.2 μm) and without ZAE
413 coated test the obtained values are 102 min by the system. The analysis of the solar cooker with
414 ZAE coated in 1.0-micron show that the average time to boil a 2 L water increased by 24.32 min
415 (32.26%) from June 2020 to June 2021.

416 The absorbed energy by the 2 L of water can reduce the cooking time and obtain over a time
417 intermission of 15 min. The performance of the solar cooker is established with output period
418 intermissions, and the cooking ends at a constant temperature. As indicated earlier, ZAE coating
419 in the solar cooker was found to enhance the cooking performance by absorbing more thermal
420 energy from the bar plate. The PV power and nichrome heating coil were also connected with the
421 solar cooker to increase the internal heat transfer modes, thereby increasing the thermal heat flow
422 rate of the system. The experiments proved that the mathematical modeling for the proposed

423 cooker could be utilized to optimize design parameters for large-scale installation to serve large
424 communities. Further, the model can be used to evaluate the proposed cooker in any other location
425 with a similar climatic condition to study its performance.

426 The proposed cooker with cooking vessels with and without the ZAE coating (one micron)
427 was evaluated to cook various kinds of food stuffs. The time taken for cooking with both vessels
428 is tabulated in **Table 5**. The cooking time for various foodstuff in **Table 5** demonstrate that the
429 cooking period for the vessel with ZAE coating reduced compared to that of the vessel without
430 coating. Additionally, a cooker size of 24×7 can be used by a family of 4 members short of
431 intermission. During the daytime, one can use the cooker by incorporating the thermal energy
432 received from the evacuated tubes supported by electrical backup provided through the Nichrome
433 heating coil. In the nighttime, the battery can be discharged to supply current through the
434 Nichrome heating coil to fulfill the required energy for cooking in the vessel.

435 *3.5 Design performance of ZAE mass fraction*

436 The solar cooker with impact of using ZAE coated with 0.8-micron, 1.0 micron, and 1.2-microns
437 on the overall performance of the solar cooker is assessed from the perspective of thermal
438 energy. Also, the impact of the presence and absence of the ZAE coating (one micron) on the solar
439 cooker's performance was evaluated and discussed in Section 3.1. It established that the solar
440 cooker has been analyzed with coated samples in different micron levels including 0.8, 1.0, and
441 1.2, with enhanced thermal energy productivities compared to the other cases. The solar cooker is
442 achieved in one micron used in the investigation. Average solar radiation during the model was
443 789.43 W/m^2 , 791.27 W/m^2 , and 785.11 W/m^2 for the test with the ZAE coated solar cooker with
444 0.8-micron, 1.0 micron, and 1.2 microns, respectively. The ambient temperature values were also
445 $34.77 \text{ }^\circ\text{C}$, $35.28 \text{ }^\circ\text{C}$, and $34.73 \text{ }^\circ\text{C}$, respectively, indicating that the achieved model is somewhat
446 comparable with the climatic environmental conditions.

447 *3.6 Efficiency analysis*

448 One of the solar cooker vessels was coated with ZAE materials using different micron levels and
449 the impact of this variable on the heat transfer and productivity of the solar cooker is shown in **Fig.**
450 **6(b)**. The coated section with ZAE increased the thermal energy absorption which in turn enhanced
451 its heat transfer characteristics. This consequently increased the energy efficiency of the system.
452 The average design energy efficiency is found to be around 39.11%, 48.31%, and 41.24%, for heat

453 transfer with an efficient ZAE materials coating of 0.8-micron, 1.0 micron, and 1.2-micron
454 thickness, respectively. The solar cooker performed with characteristics performance on ZAE as
455 followed in **Table 6** as comparative studies.

456 **4 Conclusion**

457 An overall performance of a solar cooker using ZAE coating was investigated from a thermal
458 energy performance point of view. Also, the output of a cooker using PV and evacuated tubes with
459 cooking pots with and without ZAE coating were estimated. Investigated parameters in this
460 research include ZAE coatings with different thicknesses of 0.8 micron, 1.0microns, and 1.2
461 micron, which were used in the ZAE mass fraction of the system. The following conclusions are
462 drawn from the current study:

- 463 (i) The ZAE coating on the sides and the base of the cooking vessel were evaluated in
464 terms of F_1 (0.1520) and F_2 (0.4230) which are below the BIS (Bureau of Indian
465 Standards) values of Indian Standards.
- 466 (ii) The mathematical model was validated with a negligible difference in the cooker's
467 experimental and theoretical temperature which was proved by finding the standard
468 deviation between the theoretical and experimental observations.
- 469 (iii) For the temperature of the base, sides, lid, and cooking fluid, the standard deviation
470 value between the experimental observation and theoretical values were 0.025, 0.109,
471 0.0416, and 0.16122.
- 472 (iv) The cooking time for various foodstuff in the cooking vessel with ZAE coating reduced
473 significantly to save time.
- 474 (v) The thermal efficiency of the cooker was found to be 42.65% by incorporating the input
475 energy with extra energy supplied through electrical backup. When ZAE coating was
476 used, the efficiency was enhanced by 10.35% compared to the cooking vessel without
477 the coating.
- 478 (vi) The newly designed solar cooker with ZAE coating was used on a 24 x 7 basis as
479 necessary to cook for a family of 4 which proves its reliability.

480 Consequently, the utilization of ZAE as a coating material for the solar cooker was found to be a
481 suitable technique to improve the thermal performance of a solar cooker. In addition, phase change
482 material (PCM)-based energy storage materials when integrated into a solar cooker can offer the

483 possibility of cooking after sunset. Therefore, the upcoming study will be to investigate the
 484 consequences of simultaneous use of ZAE and PCM to improve the energy productivity of solar
 485 cookers.

486

487 **Nomenclature**

- 488 A - Area of the base and side of the cooking vessel (m^2)
 489 A_{sc} - Solar cooker area (m^2)
 490 C - Specific heat capacity of water (J/kgK)
 491 $E_{NHC,out,ave}$ - average energy output in NHC (%)
 492 E_p - Energy pump
 493 $F_{1\&2}$ - First and second Figure of Merit
 494 H - Intensity of Solar Radiation (W/m^2)
 495 $H dt$ - Hourly variation of solar radiations (W/m^2)
 496 h_{cbcf} - Convective heat transfer coefficient from base of the cooking vessel to cooking
 497 fluid (W/mK)
 498 h_{scsf} - Convective heat transfer coefficient from side of the cooking vessel to cooking
 499 fluid (W/mK)
 500 h_{cfl} - Convective heat transfer coefficient from cooking fluid to the lid of the cooking
 501 vessel (W/mK)
 502 h_{la} - Convective heat transfer coefficient from the lid of the cooking vessel to the
 503 ambient
 504 (W/mK)
 505 M - Mass of water (kg)
 506 P - Interval cooking power (W)
 507 P_s - Standardized Cooking power (W)
 508 T_a - Ambient Temperature ($^{\circ}C$)
 509 t_1 - Initial time
 510 t_2 - Final time
 511 T_{w1} - Initial water temperature (K)
 512 T_{w2} - Final Water Temperature (K)
 513 T_I - Initial water temperature during the evaluation of Interval Cooking Power ($^{\circ}C$)

514	T_2	-	Final water temperature during the evaluation of Interval Cooking Power (°C)
515	M_w	-	Mass of cooking fluid (kg)
516	C_w	-	Specific heat capacity of cooking fluid (J/kgK)
517	T_w	-	Temperature of cooking fluid (°C)
518	T_b	-	Temperaure of the base of the cooking vessel (°C)
519	T_s	-	Temperature of the sides of the cooking vessel (°C)
520	T_l	-	Temperature of the lid of the cooking vessel (°C)
521	T_a	-	Temperature of the ambient (°C)
522	T_{ps}	-	Stagnation temperature of the base of the cooking vessel without load (°C)
523	η_{pv}	-	Overall output of PV

524

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530

531 **Conflict of Interest**

532 There is no conflict of interest among the authors.

533

534 **Author Contributions**

535 **A. Simon Prabu**

536 Synthesis and characterization of SiO₂ NPs with herbal extracts

537 **Dr. V. Chithambaram**

538 Data validation, reviewing and editing the paper

539 **Dr.S. Shanmugan**

540 Analysis of results, writing the manuscript, reviewing and editing the paper

541 **Dr. Pasquale Cavaliere and Dr. Shiva Gorjian**

542 Data validation, Editing of the manuscript

543 **Dr. Abderrahmane Aissa and Abed Mourad**

544 Analysis of results

545 **Dr. P. Pardhasaradhi and Dr. R. Muthucumaraswamy**

546 Analysis of results, writing the manuscript,

547 **Dr. F. A. Essa and Dr. Ammar Hamed Elsheikh**

548 Analysis of results, Data validation,

549 **Availability of Data and Material**

550 The synthesized materials with herbal extracts and data of results of characterization are
551 available.

552 **Compliance with ethical standard**

553 The research work is ethically complied.

554 **Consent to participate**

555 All the authors give their consent to having participated in the current work.

556 **Consent for publication**

557 All the authors give their consent for publication of this work.
558

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Figures

Figure 1

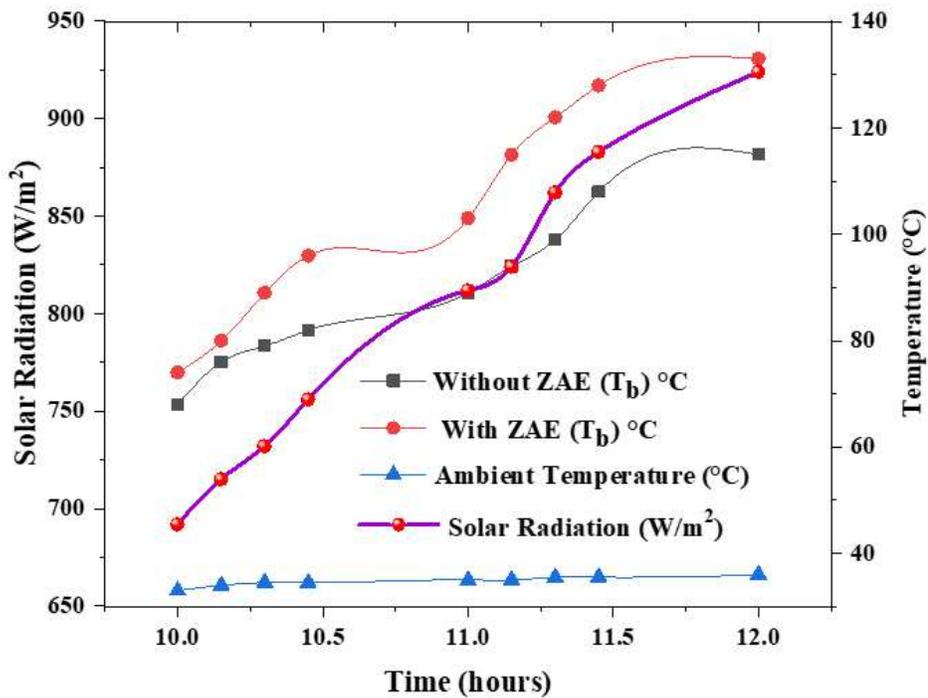
- (a) Photos of preparing leaf extract from *Acalypha Indica* leaves.
- (b). The prepared ZnO/*Acalypha Indica* leaf extract.
- (c). The prepared ZnO/*Acalypha Indica* stem extract.
- (d). ZAE chemical bond energy absorption process.

Figure 2

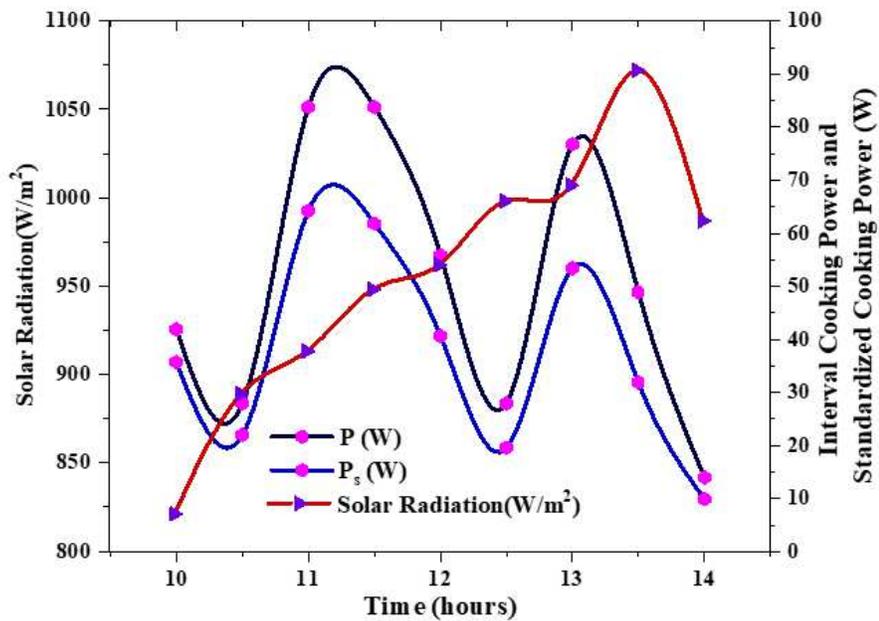
- (a). XRD analysis of ZnO/*Acalypha Indica* extract.
- (b). FTIR analysis of ZAE.
- (c). The UV analysis ZAE.
- (d) SEM analysis of ZAE.
- (e) EDAX analysis of ZAE.

Figure 3

- (a) An experimental setup of the solar cooker that coated with ZAE and fixed in a cooking vessel with an ETC, a battery charge controller.
- (b) The ZAE coated in Nichrome heating coil and different food cooked by the solar cooker.



A



B

Figure 4

(a) Variation of solar radiation and temperature of the cooking vessel (T_b) with and without ZAE.

(b) shows a variety of interval and Standardized cooking power.

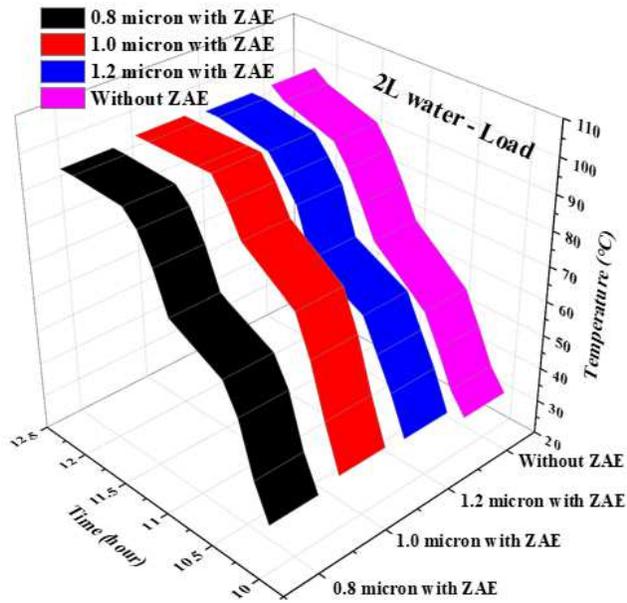
Figure 5

(a) Variation of solar radiation and ambient temperature in the solar cooker average values from June 2020 to June 2021.

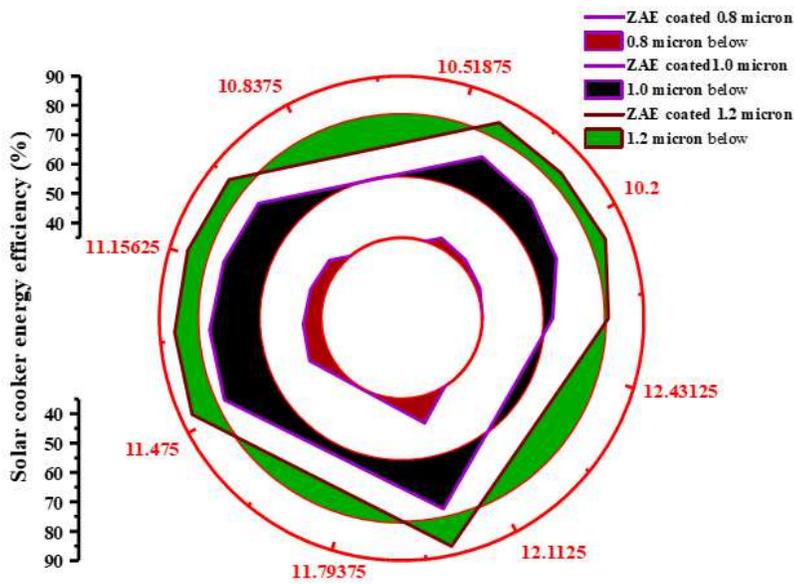
(b) shows a variation of the side, base, and lid of the cooking vessel with and without a coating of ZAE in one-micron levels.

(c) shows various theoretical and experimental values of the temperature of the side, base, and lid of the cooking vessel.

(d) shows a variation of the cooking fluid's temperature.



A



B

Figure 6

(a) The water temperature in the cooking pot for different coated ZAE micron levels. (b) Average energy efficiency of the solar cooker for different thicknesses of ZAE coating.