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Research Article

Keywords: Nitrate reduction, Mechanism, HCOOH, nZVI-g-C₃N₄/TiO₂ composite

Posted Date: February 12th, 2021

DOI: <https://doi.org/10.21203/rs.3.rs-216615/v1>

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A Study on the Mechanism and Kinetic of Nitrate Reduction by the nZVI-g-C₃N₄/TiO₂ composite under the simulated sunlight

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Abstract

g-C₃N₄/TiO₂ composite has excellent photoelectric properties and is considered as a good carrier of nanoparticles. A novel composite of nZVI-g-C₃N₄/TiO₂ was successfully synthesized through in-situ growth nZVI on the surface of g-C₃N₄/TiO₂ with liquid phase reduction method. The composite was characterized by TEM, XRD, EDS and evaluated its nitrate removal efficiency. The effects of composite dosage, solution initial pH and HCOOH concentration on nitrate reduction were investigated. The results showed that nitrate was rapidly reduced by nZVI-g-C₃N₄/TiO₂ composite. The dosage of 4 g/L nZVI-g-C₃N₄/TiO₂ composite and 3.0 mM of HCOOH concentration was more suitable for nitrate reduction. Solution initial pH had little impact on the nitrate reduction efficiency, but affected the proportion of the nitrate reduction

products. The mechanism of nitrate reduction in the nZVI-gC₃N₄/TiO₂/HCOOH-Xe-lamp system was proposed. The nZVI-gC₃N₄/TiO₂ composite could be considered as a viable and promising technology for water pollution remediation.

Keywords: Nitrate reduction, Mechanism, HCOOH, nZVI-g-C₃N₄/TiO₂ composite

1. Introduction

Nitrate contamination in groundwater and surface water has become more and more serious due to wastewater discharges from industry, agriculture, aquaculture and domestic sewage. Nitrate pollution not only poses a serious threat to human health, such as methemoglobinemia and cancer etc., but also causes serious water deterioration such as eutrophication[1-3]. At present, the traditional nitrate treatment technologies such as ion exchange, reverse osmosis only concentrate nitrate aqueous. And biological denitrification have high operational requirement such as temperature[4]. Among them, the combination of zero-valent iron (ZVI) and photocatalyst is considered as a most promising method for nitrate degradation due to its convenience, high efficiency and low cost[5, 6].

ZVI is widely used for nitrate removal because of its strong reduction ability, high activity, non-toxic, relatively low cost and simple operation[7, 8]. It is reported that nano-ZVI(nZVI) has larger specific surface area and higher reactivity than micro-ZVI (mZVI), which makes it have higher practical application value in nitrate treatment[9]. However, the nitrate degradation efficiency of nZVI often decreases due to its aggregation and agglomeration[10]. Thus, to overcome this drawback of nZVI, the carrier as dispersant is concerned and investigated. For instance, Zhang et al.[11] report that nZVI is highly dispersed on the surface of exfoliated graphite to prevent from aggregation and agglomeration. Furthermore, some carriers with high electrode

potential, such as activated carbon, graphite, rGO, can form micro galvanic cells with nZVI in solution to promote electron transfer, thus increasing nitrate removal efficiency. Luo et al. [12] report that electron is driven from nZVI to the activated carbon due to a relative potential difference to rapidly reduce nitrate. Pu et al. [13] also report that the efficiency of nitrate removal by promoting electron migration from nZVI surface to rGO surface is enhanced. Up to now, supported nZVI materials such as goethite[14], diatomite[15], chelating resin[16, 17], C[4, 18], active carbon[19], biochar[20], silicon[21], graphene[22] have been studied. But these carriers still exist the disadvantages of tedious preparation and high cost. Therefore, it is necessary to develop an easy-prepared, low-cost supportive matrix to effectively disperse nZVI, and to form micro-galvanic cells with nZVI increasing nitrate removal efficiency.

Photocatalysis can effectively degrade environmental pollutants and be thought as a viable and promising technology for water pollution remediation[23-27]. g-C₃N₄/TiO₂ as a semiconductor and a photocatalyst has attracted much attention owing to low cost, non-toxic nature, good stability and environment friendliness etc[28-30]. However, the practical application of g-C₃N₄/TiO₂ was limited due to easy combination of photo-electrons and holes. According to the previous studies, doping metals such as Au, Ag, Pt effectively could suppress the electrons and holes rapid recombination to improve their photocatalytic performance[23, 31-33]. For example, lv et al.[31] report that g-C₃N₄/TiO₂/CQDs/Au of H₂ production rate is 1.8 times than that of g-C₃N₄/TiO₂. Geng[33] et al. prove that doping metal Ag in the g-C₃N₄/TiO₂ composite could accelerate separation of photoelectrons and holes.

Therefore, we design that g-C₃N₄/TiO₂ as photocatalyst is used to support nZVI. On the one hand, nZVI as mediator effectively promote separation of photo-charge carriers to enhance nitrate

reduction. And g-C₃N₄/TiO₂ as carrier could highly disperse nZVI so as to provide more reactive sites. On the other hand, micro-galvanic cells formed by g-C₃N₄/TiO₂ as cathode and nZVI as anode accelerate the transfer of electrons and the redox progress of nitrate[34, 35]. In this work, a novel nZVI-g-C₃N₄/TiO₂ composite was prepared by in-situ liquid-phase reduction method and was used to reduce nitrate from aqueous solution under 300W Xe-lamp. The effects of composite dose, solution initial pH and HCOOH concentration on nitrate reduction were investigated. The mechanism of nitrate reduction in the nZVI-g-C₃N₄/TiO₂/HCOOH/Xe-lamp system was proposed.

2. Materials and methods

2.1 Synthesis of the nZVI-g-C₃N₄/TiO₂ composite

Preparation of the g-C₃N₄/TiO₂ composite: A mixture of 0.0577 g TiO₂, 2.8835 g melamine and 2.0588 g Urea was ground and placed in a crucible covered with aluminum foil before calcinated at 520 °C for 4 h with a heating rate of 10 °C/min in a muffle furnace. After cooling to room temperature, the as-obtained g-C₃N₄/TiO₂ composite was ground into powder and ultrasonic for 0.5 h in deionized water with the ratio of 1 g: 50mL, followed by filtration. The ultrasonic and filtration process was repeated totally four times for removing impurities. Then the g-C₃N₄/TiO₂ composite was dried by microwave and ground into powder.

Preparation of the nZVI-g-C₃N₄/TiO₂ composite: Fifty milliliter of deionized water and 0.8690 g anhydrous ferric chloride (FeCl₃) were stirred and mixed in a two-neck flask before 1 g of g-C₃N₄/TiO₂ composite added in. Then the mixture was treated with ultrasonic for 10 min followed by magnetic stirring for 3 h. After that 80 mL of 0.2 M sodium borohydride (NaBH₄) solution was quickly injected into the flask with syringe under vacuum condition. Then the mixture was thoroughly stirred for another 40 min under vacuum condition before filtration. The

filter residue was washed with 15 mL de-ionized water and 15 mL anhydrous ethanol successively for three times before dried 60 °C for 12 h in vacuum oven. The as-obtained nZVI-g-C₃N₄/TiO₂ composite was then ground into powder ready for use. nZVI was also prepared following this procedure without g-C₃N₄/TiO₂ composite added.

2.2 Characterization

Transmission electron microscope (TEM, FEI Talos F200x and FEI Tecnai G2 F20) images and Energy Dispersive spectrometer (EDS, Oxford8118) spectrograms can investigate the morphology and the elementary content of nZVI-g-C₃N₄/TiO₂ composite. X-ray diffraction patterns (XRD, Bruker D8 ADVANCE A25X) were recorded in 5°-85° range.

2.3 Nitrate reduction experiments

The photo-induced nitrate reduction experiments were conducted by adding XX g as-prepared materials in to 50 mL nitrate solution with an initial concentration of 50 mg N/L. The initial pH of the nitrate solutions was adjusted to 2.0, 2.5, 3.6, 7.0, 8.0, 9.0, 10, respectively, with 0.5 M HCl/NaOH. The suspensions were then irradiated by a 300W Xe lamp. 3 mL sample solutions were taken every 10 min and then filtered with 0.22 μm membrane. All samples were tested in a day. The concentrations of nitrate, ammonium, nitrite and Fe²⁺ in the filtrates were then determined by a UV-Vis spectrophotometer (SP-751, Jinghua, China) the wavelengths of 220 nm, 420 nm, 540 nm and 510 nm, respectively. After Fe³⁺ was reduced by hydroxylamine hydrochloride, the concentration of the total iron ions can be determined by analyzing Fe²⁺. All detection reagents were configured by the laboratory.

2.4 Data analysis

Nitrate removal efficiency, $X_{NO_3^-}$ is calculated by Eq.1:

$$X_{NO_3^-} = \frac{[NO_3^-]_0 - [NO_3^-]_t}{[NO_3^-]_0} \times 100\% \quad (1)$$

Where $[NO_3^-]_0$ and $[NO_3^-]_t$ are the concentration of nitrate nitrogen (mg N/L) at time 0 and t (min), respectively. According to the reviewed research, nitrate nitrogen, ammonium nitrogen and nitrite nitrogen are thought as the main product of reduction because the content of the gas phase nitrous oxide (N_xO) in the nitrate reduction process was negligible [14, 22, 36]. Thus, according to the mass balance of nitrogen, the nitrite selectivity ($S_{NO_2^-}$) is calculated by Eq.2:

$$S_{NO_2^-} = \frac{[NO_2^-]_t}{[NO_3^-]_0 - [NO_3^-]_t} \times 100\% \quad (2)$$

$S_{NH_4^+}$ was calculated by Eq.3:

$$S_{NH_4^+} = \frac{[NH_4^+]_t}{[NO_3^-]_0 - [NO_3^-]_t} \times 100\% \quad (3)$$

S_{N_2} was calculated by Eq.4:

$$S_{N_2} = \frac{[NO_3^-]_0 - [NO_3^-]_t - [NO_2^-]_t - [NH_4^+]_t}{[NO_3^-]_0 - [NO_3^-]_t} \times 100\% \quad (4)$$

Where $[NO_2^-]_t$ and $[NH_4^+]_t$ are the concentration of nitrite nitrogen and ammonium nitrogen (mg N/L) at time t, respectively. Pseudo first-order dynamic model (Eq.5) is used to calculate the rate constant of nitrate reduction [5, 37, 38]. The rate constant of nitrate reduction was calculated as follows:

$$r = -\frac{d[NO_3^-]_t}{dt} = k[NO_3^-]_t \quad (5)$$

$$\frac{d([NO_3^-]_0 - [NO_3^-]_t)}{[NO_3^-]_t} = k dt \quad (6)$$

$$\int_0^{([NO_3^-]_0 - [NO_3^-]_t)} \frac{d([NO_3^-]_0 - [NO_3^-]_t)}{[NO_3^-]_t} = \int_0^t k dt \quad (7)$$

$$\ln \frac{[NO_3^-]_0}{[NO_3^-]_t} = kt = \ln \frac{C_0}{C_t} \quad (8)$$

Where C_0 and C_t are the concentration of nitrate nitrogen (mg N/L) at time 0 and t. The rate constant of nitrate reduction is represented by k .

3. Results and discussion

3.1 Characterization

The X-Ray diffraction (XRD) patterns of the nZVI, TiO₂, g-C₃N₄, g-C₃N₄/TiO₂ and nZVI-g-C₃N₄/TiO₂ composite were shown in Figure. 1. Typical characteristic diffraction patterns of pure g-C₃N₄ appeared at 27.2° (2 θ) and corresponded to (0 0 2) hexagonal crystal planes, which was consistent with the results in the literature[39]. The diffraction peaks of pure TiO₂ appeared at 26.5°, 37.3°, 41.3°, 54.4°, 56.6° and 62.8°, which corresponded to (1 0 1), (0 0 4), (2 0 0), (1 0 5), (2 1 1), (2 0 4) anatase phase of TiO₂ crystal planes, respectively[36]. Compared with pure TiO₂, peaks intensity of anatase TiO₂ plane of thermal polymerization synthesis of g-C₃N₄/TiO₂ composite was weak because of the low content of TiO₂. At the same time, the diffraction peak of g-C₃N₄ moved a short distance after synthesizing g-C₃N₄/TiO₂ composite. For the XRD diffraction pattern of nZVI, the typical diffraction peak appeared at 44.8° corresponds to α - Fe (1 1 0) crystal planes, which was consistent with the results in the literature[40, 41]. Otherwise, the typical characteristic diffraction peaks of Fe₃O₄ appeared at 35.5°, 57.4° and 62.9° (2 θ) corresponds to (3 1 1), (5 1 1), (4 4 0) Fe₃O₄ crystal planes. The XRD diffraction pattern of nZVI-g-C₃N₄/TiO₂ composite revealed that the characteristic peaks of g-C₃N₄, nZVI and TiO₂ appeared at 27.2°, 44.8° and 54.4° without other diffraction peaks of iron oxides. It suggested that g-C₃N₄/TiO₂ well immobilized and stabilized nZVI by a large number of π electrons in the g-C₃N₄ composite,[22] which can inhibit and avoid the oxidation of nZVI in the preparation or storage process of nZVI-g-C₃N₄/TiO₂ composite.

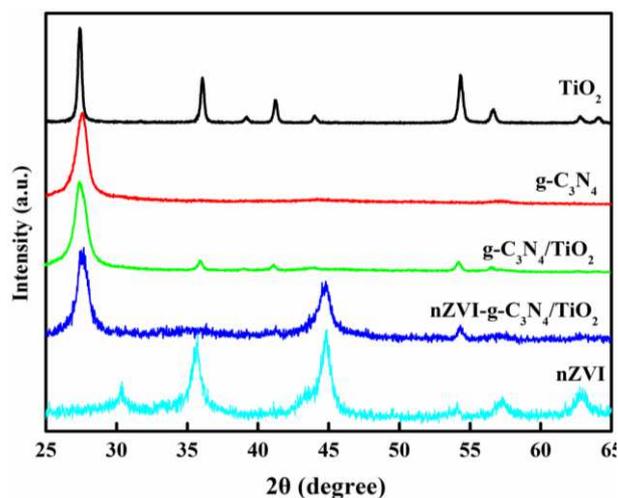


Fig.1 XRD patterns of nZVI, TiO₂, g-C₃N₄, g-C₃N₄/TiO₂ and nZVI-g-C₃N₄/TiO₂ composite.

Fig. 2a-c showed the morphological structure of g-C₃N₄/TiO₂, nZVI and nZVI-g-C₃N₄/TiO₂ composite using TEM. As shown in Fig. 2a, g-C₃N₄/TiO₂ composite was successfully synthesized. And it revealed that TiO₂ was prominently distributed on the surface of the g-C₃N₄. At the same time, the g-C₃N₄ had the layered structure with wrinkles, which could provide abundant supporting sites for nZVI. As described in Fig. 2b, it revealed that nZVI had a chain-like structure and agglomerated. Compared with nZVI alone, nZVI particles supported on the surface of g-C₃N₄/TiO₂ of diameter was shorter, which was observed from the TEM images (Fig. 2b and c). Moreover, Fig. 2c showed that the nZVI was distributed well over the surface of the g-C₃N₄/TiO₂ composite due to in-situ reduction of Fe³⁺ by NaBH₄ on the surface of g-C₃N₄/TiO₂, which suggested that the g-C₃N₄/TiO₂ composite was beneficial to the immobilization of nZVI, thereby inhibiting the aggregation and agglomeration of nZVI. EDS image (Fig. 2d) showed that nZVI-g-C₃N₄/TiO₂ composite mainly contains C, N, O, Ti and Fe elements, and their mass fractions are 30.71%, 54.28%, 6.60%, 1.33% and 7.09%, respectively. It confirmed that these elements coexisted in the nZVI-g-C₃N₄/TiO₂ composite.

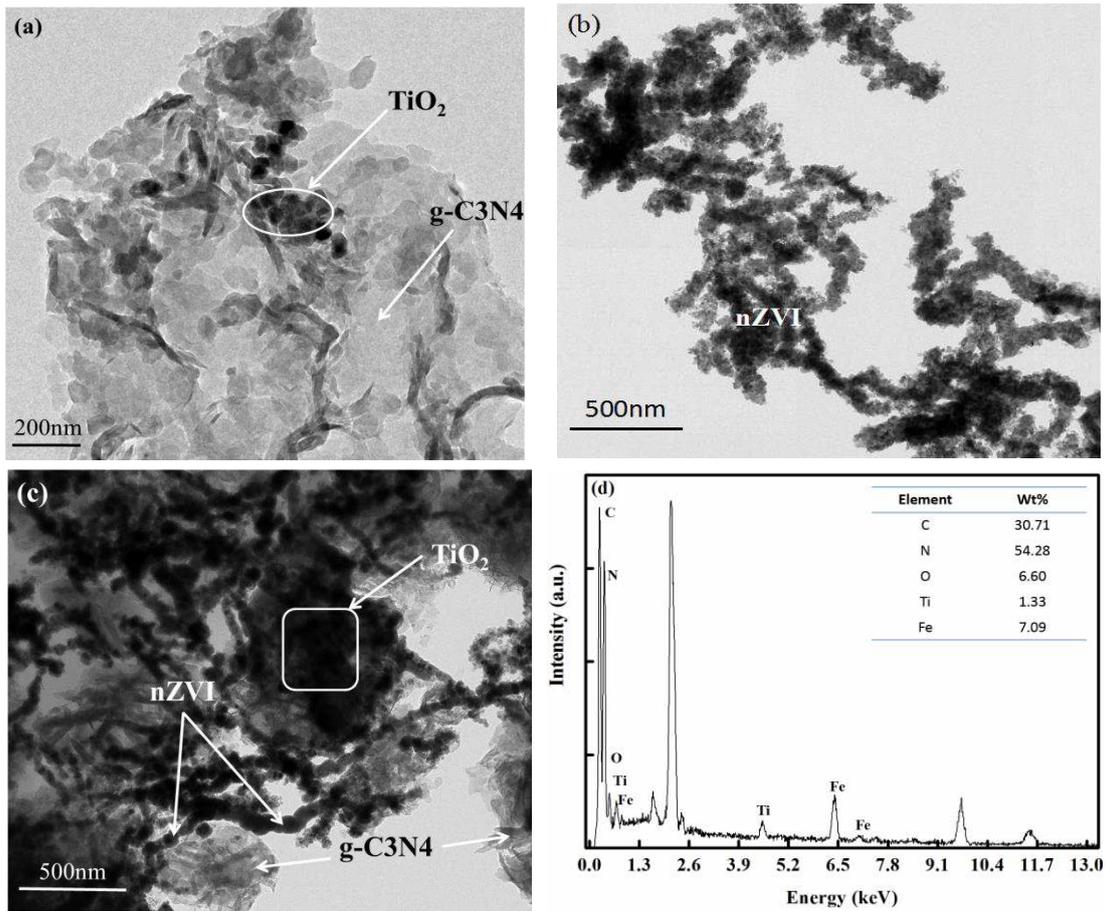
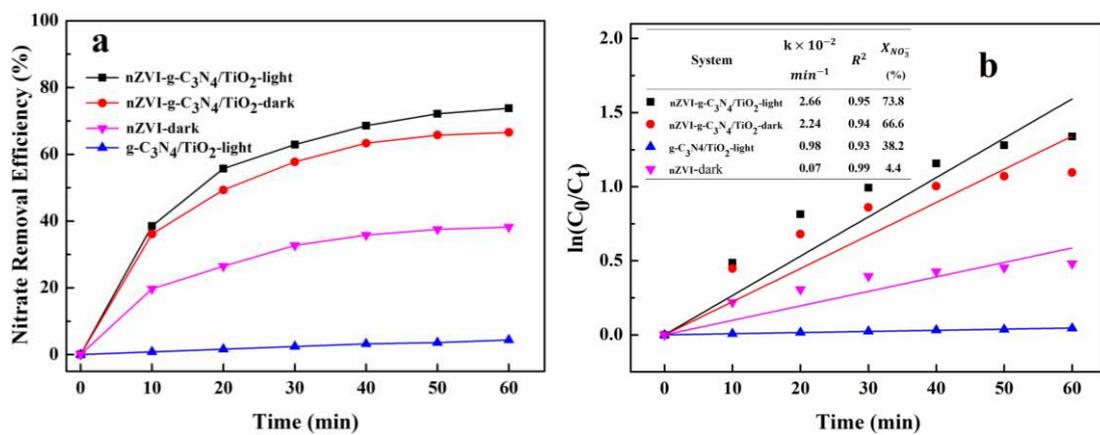


Fig. 2 TEM images for (a) the g-C₃N₄/TiO₂; (b) the nZVI; (c) the nZVI-g-C₃N₄/TiO₂ composite; (d) EDS spectrum of the nZVI-g-C₃N₄/TiO₂;

3.2 Nitrate removal



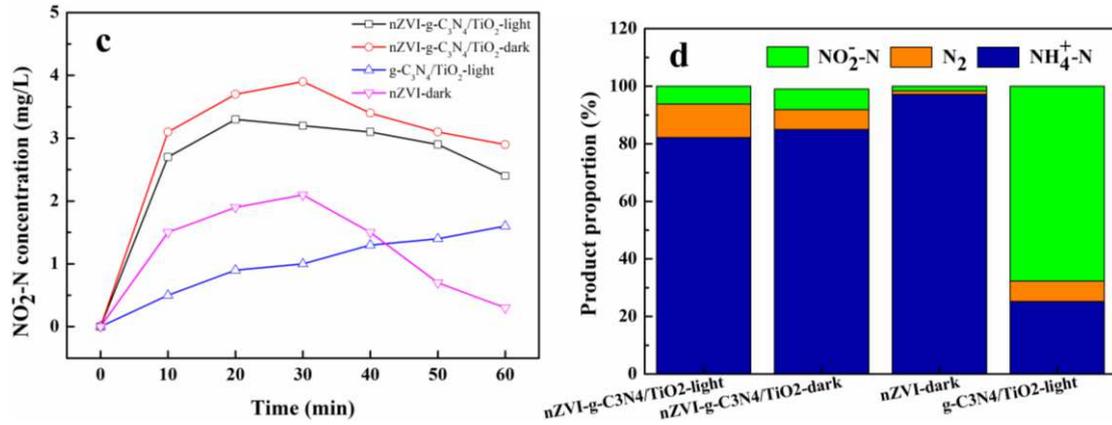


Fig. 3 (a) Nitrate removal efficiency of nZVI, g-C₃N₄/TiO₂ and nZVI-g-C₃N₄/TiO₂ composites; **(b)** Rate constant of nitrate reduction in the different system; **(c)** nitrite nitrogen concentration (mg/L) changes during nitrate reduction; **(d)** Product proportion of nitrate reduction in the different system; (initial nitrate nitrogen concentration at 50 mg/L; reductant dose at 4 g/L and initial pH at 7.0)

As can be seen from Fig. 3a, the nitrate removal efficiency of nZVI-g-C₃N₄/TiO₂ composite (66.6%) under the dark condition was higher than that of nZVI (38.2%). Fig. 3b showed that the rate constant of nitrate reduction by nZVI-g-C₃N₄/TiO₂ composite ($2.24 \times 10^{-2} \text{ min}^{-1}$) was 2.28 times than that of nZVI ($0.98 \times 10^{-2} \text{ min}^{-1}$), which suggested rapid nitrate reduction by nZVI-g-C₃N₄/TiO₂ composite, likely due to micro-galvanic cells formed by nZVI-g-C₃N₄/TiO₂ composite in the solution. It promoted electron release of quickly from nZVI and transfer to nitrate for nitrate reduction. Moreover, this might also be because nZVI highly dispersed on the surface of g-C₃N₄/TiO₂ could provide more active sites for nitrate reduction. Fig. 3a revealed that the order of nitrate removal efficiency was as: nZVI-g-C₃N₄/TiO₂-light (73.8%) > g-C₃N₄/TiO₂-light (4.4%), which suggested that g-C₃N₄/TiO₂ under the light condition contributed to the poor nitrate removal. On the contrary, nitrate reduction efficiency by nZVI-g-C₃N₄/TiO₂ composite was obviously improved. This was because nZVI acting as electron mediator can facilitate the

separation of photo-generated charge carriers. Then a amount of photo-generated electrons excited by the g-C₃N₄/TiO₂ under Xe-lamp can promote nitrate reduction. In brief, nitrate reduction by nZVI-g-C₃N₄/TiO₂ composite was mainly due to the synergistic effect of micro-galvanic cells, followed by photocatalysis.

Fig. 3c indicated that for nitrate removal by nZVI alone, $NO_2^- - N$ accumulated in the initial reaction and then completely reduced to N_2 or $NH_4^+ - N$. For nitrate removal by g-C₃N₄/TiO₂, the concentration of $NO_2^- - N$ increased with time. Moreover, Fig. 4d showed that the primary product nitrate removal by g-C₃N₄/TiO₂ was nitrite and its $NO_2^- - N$ selectivity was 67.7%. However, For nitrate removal by nZVI-g-C₃N₄/TiO₂ composite, $NO_2^- - N$ as an intermediate product was accumulated whether in the dark or light condition, and then only a little reduced to N_2 or $NH_4^+ - N$. The reason was that $NO_2^- - N$ accumulated in the solution prior to electron migration to the surface of g-C₃N₄/TiO₂ for further reduction. Meanwhile, Fig. 4d revealed that the order of N_2 selectivity was as: nZVI-g-C₃N₄/TiO₂-light (11.6%) > g-C₃N₄/TiO₂-light (7.1%) > nZVI-g-C₃N₄/TiO₂-dark (6.9%) > nZVI-dark (1.3%). This was because a standard potential of 1.45 V vs Standard Hydrogen Electrode (SHE) of nitrite reduced to N_2 is higher than that of nitrate $E^\theta(NO_3^-/N_2 = 1.25V)$. It suggested that the high nitrite nitrogen concentration in the solution was more conducive to N_2 than nitrate. Thus, N_2 selectivity of nitrate removal by nZVI-g-C₃N₄/TiO₂ composite was enhanced as the results shown in Fig. 4d.

3.3 Effects of composite dosage on nitrate reduction

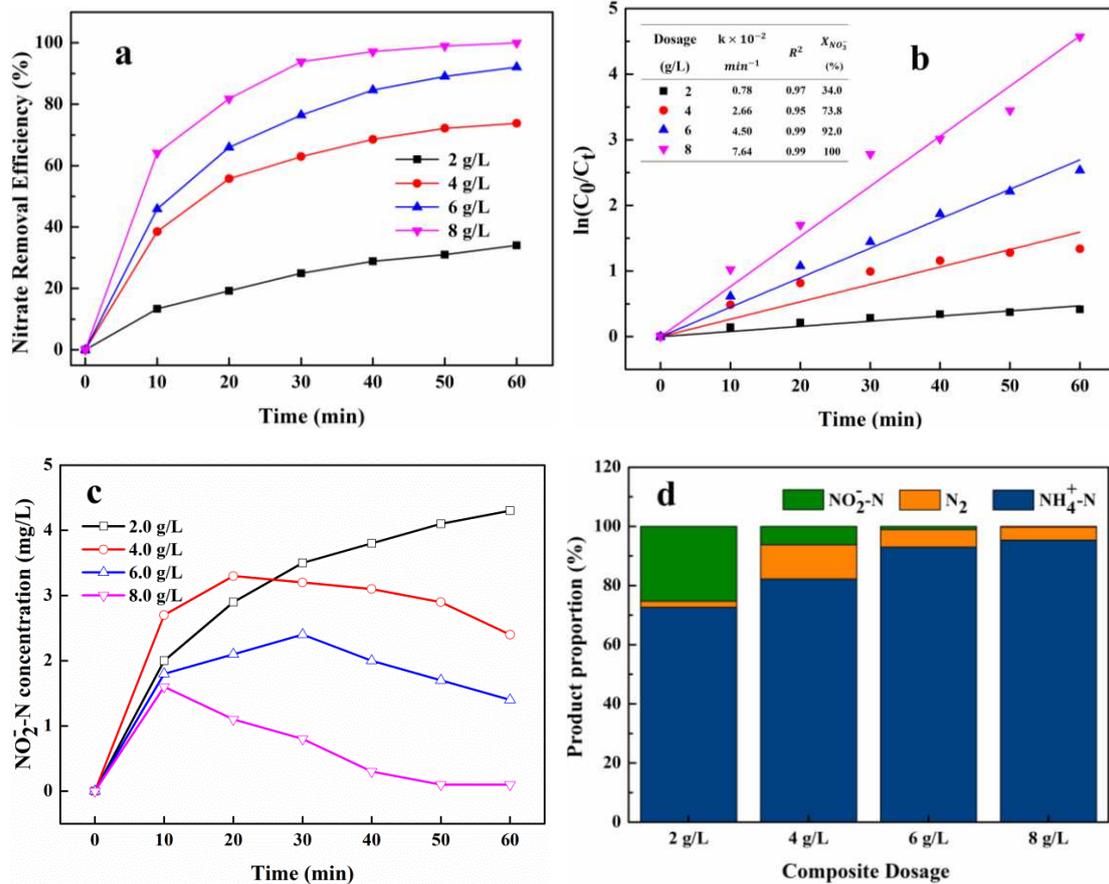


Fig. 4 (a) Nitrate removal efficiency in the different nZVI-g-C₃N₄/TiO₂ composite dosage; (b) Rate constant of nitrate reduction in the different composite dosage; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different composite dosage; (initial nitrate nitrogen concentration at 50 mg/L; initial pH at 7.0)

As shown in Fig. 4a and b, nitrate reduction rate constant k and nitrate removal efficiency $X_{NO_3^-}$ were both enhanced with the increase nZVI-g-C₃N₄/TiO₂ composite. $X_{NO_3^-}$ increased from 34% to 100% with the dosage increase from 2 g/L to 8 g/L. And the k of 8 g/L dosage was 9.8 times higher than of 2 g/L dosage. The enhanced nitrate reduction was because higher dosage of nZVI-g-C₃N₄/TiO₂ composite provided more active sites to react with nitrate. Fig. 4c showed that except for dosage of 2g/L, $NO_2^- - N$ concentration of other dosage accumulated at the beginning stage of reaction and then decreased. When the dosage was 8g/L, nitrite nitrogen was completely

reduced. The reason was that excess composite dosage could provide sufficient active sites. Noticeably, $\text{NO}_2^- - \text{N}$ concentration of nitrate removal by 2 g/L dosage increased with time. And Fig. 4d indicated that its $\text{NO}_2^- - \text{N}$ selectivity was higher others, which might be because that the low dosage of nZVI-g- $\text{C}_3\text{N}_4/\text{TiO}_2$ composite provide insufficient electron for nitrate reduction, thus resulting in nitrite accumulation.

3.4 Effects of initial pH on nitrate reduction

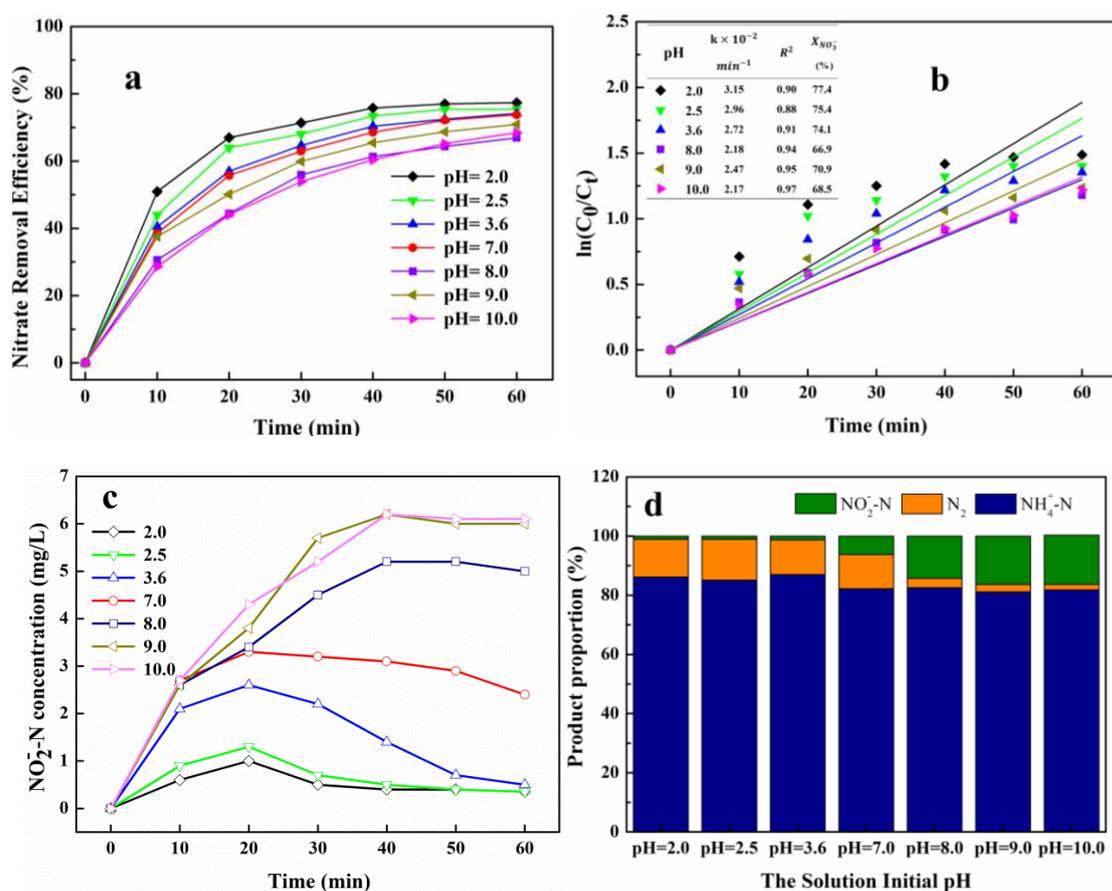
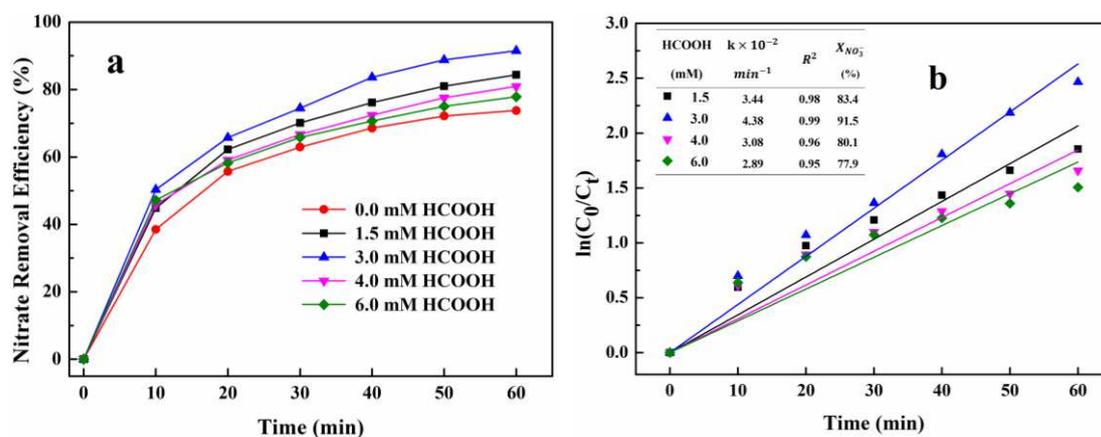


Fig. 5 (a) Nitrate removal efficiency in the different solution initial pH; (b) Rate constant of nitrate reduction in the different Initial pH of solution; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different Initial pH of solution; (initial nitrate nitrogen concentration at 50 mg/L; reductant dose at 4 g/L)

Fig. 5a and b indicated that the nitrate removal efficiency slightly increased as the solution

pH decreasing from 7.0 to 2.0, and the rate constant slightly increased from $2.66 \times 10^{-2} \text{ min}^{-1}$ to $3.15 \times 10^{-2} \text{ min}^{-1}$. This was because a part of H^+ occupied active sites on the surface of g-C₃N₄/TiO₂ because of electrostatic attraction. Fig. 5c revealed that $\text{NO}_2^- - \text{N}$ concentration was accumulated firstly, and then reduced to $\text{NH}_4^+ - \text{N}$ or N_2 . Moreover, Fig. 5d also showed that the $\text{NO}_2^- - \text{N}$ selectivity decreased from 6.2% to 1.1% with the decreasing solution initial pH from 7.0 to 2.0. However, at the alkaline condition, Fig. 5c showed that $\text{NO}_2^- - \text{N}$ concentration continuously increased with time. And Fig. 5c also showed that its $\text{NO}_2^- - \text{N}$ selectivity obviously increased. The reason might be that the high concentration of OH^- suppressed the reduction of $\text{NO}_2^- - \text{N}$. The nitrate removal efficiency $X_{\text{NO}_3^-}$ and rate constant k slightly decreased. This result might be related to the surface charge of nZVI-g-C₃N₄/TiO₂ composite. In brief, changing initial pH mainly affected product proportion of nitrate product.

3.5 Nitrate reduction mechanism of nZVI-gC₃N₄/TiO₂/HCOOH/Xe-lamp



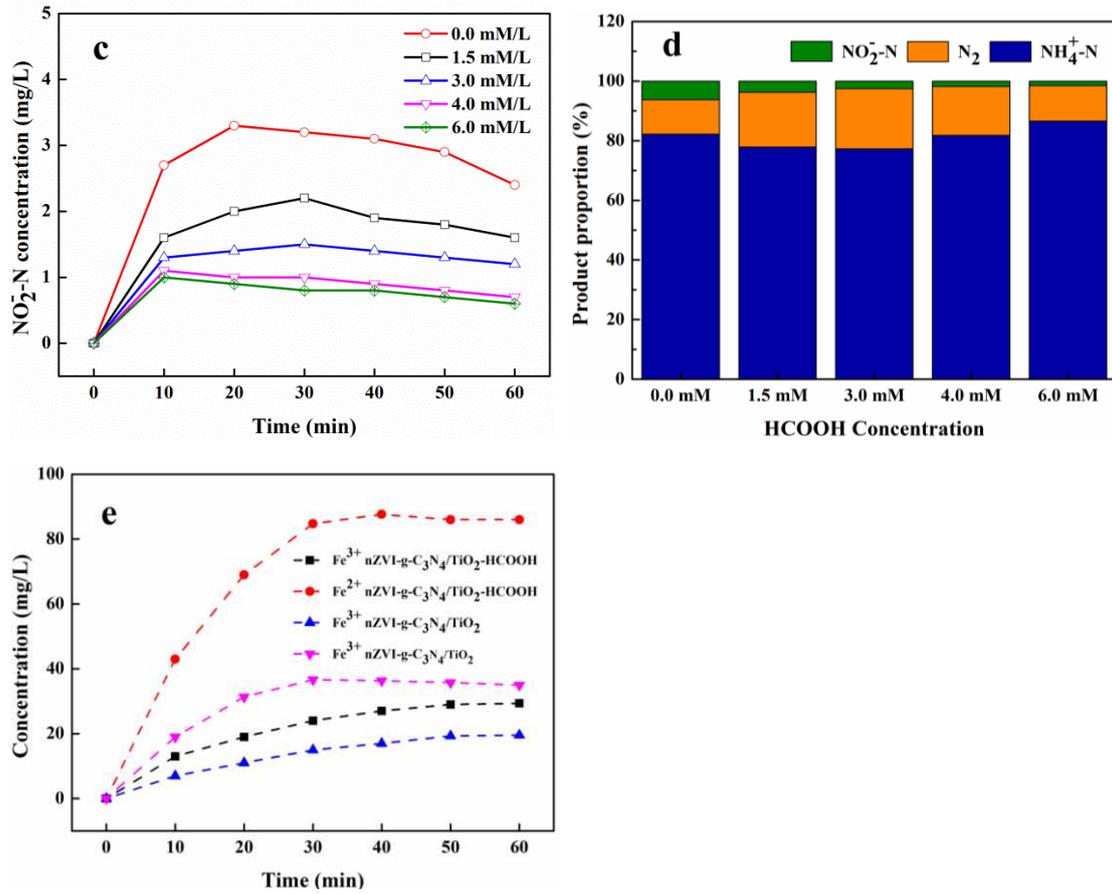
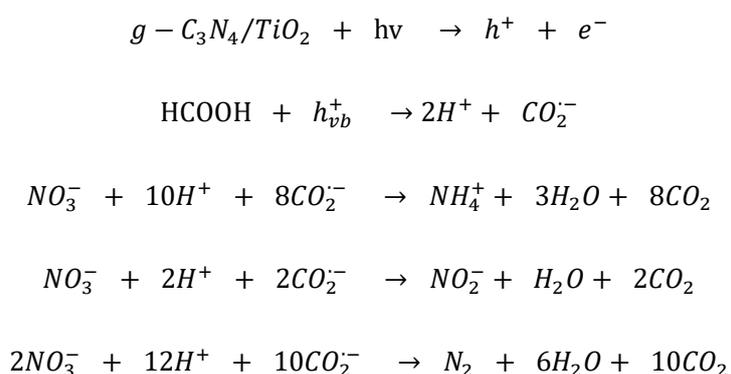


Fig. 6 (a) Nitrate removal efficiency in the different HCOOH concentration; (b) Rate constant of nitrate reduction in the different Initial pH of solution; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different Initial pH of solution; (e) and the concentration of Fe²⁺ and Fe³⁺ with time; (initial nitrate nitrogen concentration at 50 mg/L; reductant dose at 4 g/L)

HCOOH is widely used as a hole scavenger for nitrate reduction based on the single electron transfer mechanism and forming a strong reductant species $CO_2^{\cdot-}$ as the only product[36, 42]. Moreover, the strong reductant species $CO_2^{\cdot-}$ ($E^\theta(CO_2/CO_2^{\cdot-}) = -1.8V$), which was produced by the reaction between HCOOH and the photo-generated hole excited by g-C₃N₄/TiO₂ composite under the Xe-lamp, can reduce nitrate nitrogen to ammonium nitrogen ($E^\theta(NO_3^-/NH_4^+) = 1.203$), nitrite nitrogen ($E^\theta(NO_3^-/NO_2^-) = 0.94V$) and nitrogen gas ($E^\theta(NO_3^-/N_2) = 1.25V$).

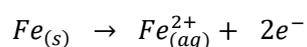
As depicted in Fig. 6a and b, the nitrate removal efficiency ($X_{NO_3^-}$) and the rate constant k increased after adding HCOOH. The $X_{NO_3^-}$ increased from 73.8% to 91.5% when HCOOH concentration increased from 0 to 3.0 mM. The k increased from $2.66 \times 10^{-2} \text{ min}^{-1}$ to $4.26 \times 10^{-2} \text{ min}^{-1}$. It suggested that adding HCOOH in the reaction system was conducive to nitrate reduction rate and efficiency. Noticeably, the nitrate removal efficiency decreased when HCOOH concentration increased from 3.0 mM to 6.0 mM, and the k also decreased from $4.26 \times 10^{-2} \text{ min}^{-1}$ to $2.94 \times 10^{-2} \text{ min}^{-1}$. This was because that the active sites on the surface of nZVI-g-C₃N₄/TiO₂ composite might be occupied by excessive HCOOH. As depicted in Fig. 6c, only a little $NO_2^- - N$ remained in the solution aqueous. At the same time, as can be seen from Fig. 6 d, $NO_2^- - N$ selectivity decreased as the increasing HCOOH concentration. In addition, N_2 selectivity was enhanced. Especially, when the concentration of HCOOH was 3.0 mM, its N_2 selectivity was 20.2%. But Fig. 6 d revealed that nitrate nitrogen was mainly reduced to ammonium nitrogen. Therefore, the related reaction was described as followed:



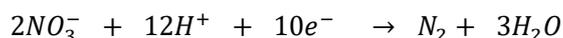
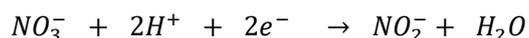
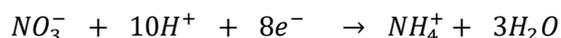
In addition, a lot of photo-generated electron produced by the excitation of g-C₃N₄/TiO₂ under the Xe-lamp could reduce nitrate. Meanwhile, electrons from the micro-galvanic cells formed by nZVI as anode and g-C₃N₄/TiO₂ as cathode in the solution aqueous also can promote nitrate reduction. And Fig. 6e indicated that nZVI after releasing electrons was mainly oxidized to

ferrous ions in the solution aqueous. Especially, the concentration of ferrous ions at the HCOOH condition was far higher than no HCOOH. This might be because Fe^{3+} was reduced by the strong reductant species $CO_2^{\cdot-}$. In the Section 3.2, it proved that $NO_3^- - N$ was rapidly reduced to $NH_4^+ - N$, $NO_2^- - N$ and N_2 due to micro-galvanic cells formed by nZVI as anode and g-C₃N₄/TiO₂ as cathode. Therefore, the related actions can be described as follows:

Fe⁰anode (oxidation):



g-C₃N₄/TiO₂ cathode (reduction):



Thus, the nitrate nitrogen in the nZVI-g-C₃N₄/TiO₂-HCOOH system was rapidly reduced to $NH_4^+ - N$, $NO_2^- - N$ and N_2 due to the synergistic effects of the micro-galvanic cells formed by nZVI as anode and g-C₃N₄/TiO₂ as cathode, the photo-generated electrons excited by g-C₃N₄/TiO₂ under the Xe-lamp and a $CO_2^{\cdot-}$ species, which was produced by the reaction of the HCOOH and the photo-generated holes excited by g-C₃N₄/TiO₂ under the Xe-lamp. In order to clearly understand the mechanism of nitrate reduction in the nZVI-gC₃N₄/TiO₂/HCOOH/Xe-lamp system, the diagram of mechanism was proposed (Fig. 7).

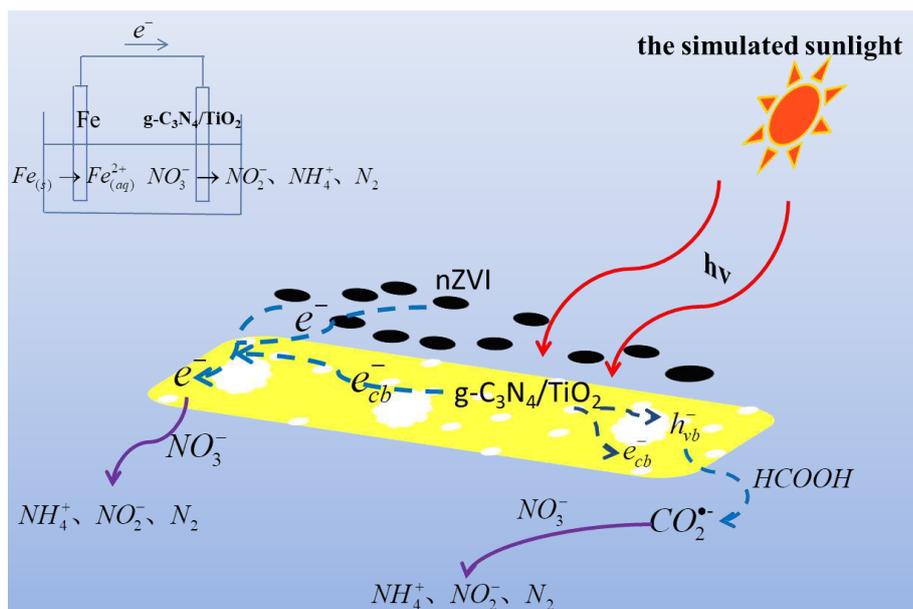


Fig. 7 The Mechanism of Nitrate Reduction in the nZVI-gC₃N₄/TiO₂/HCOOH-Xe-lamp System

3. Conclusion

The SEM and XRD analysis of nZVI-g-C₃N₄/TiO₂ composite revealed that g-C₃N₄/TiO₂ effectively could inhibit oxidation and agglomeration of nZVI. Compared with nZVI alone, the rate and efficiency of nitrate removal by nZVI-g-C₃N₄/TiO₂ composite were significantly enhanced. And the experimental results suggested that the *k* of 8 g/L dosage was 9.8 times higher than of 2 g/L dosage. Changing initial pH affected the product proportion of nitrate reduction. In the acid condition, NO₂⁻ - N as an intermediate product was accumulated firstly, and then completely reduced to NH₄⁺ - N or N₂. In the alkaline condition, NO₂⁻ - N concentration increased with time. Adding HCOOH obviously improved the rate and efficiency of nitrate reduction. In the nZVI-g-C₃N₄/TiO₂/HCOOH/Xe-lamp system, nitrate was rapidly reduced due to its synergistic effects of electron from the micro-galvanic cells, the photo-generated electron excited by g-C₃N₄/TiO₂ under the Xe-lamp and a CO₂^{•-} species produced by the reaction of HCOOH and the photo-generated holes excited by g-C₃N₄/TiO₂ under the Xe-lamp.

Acknowledgements

This work is supported by the key research and development project of Sichuan Province (2018GZ0455), the key research and development project of Chengdu City (2019-YF05-00192-SN), and also supported by the High Performance Computing Center of Sichuan Normal University, China.

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Figures

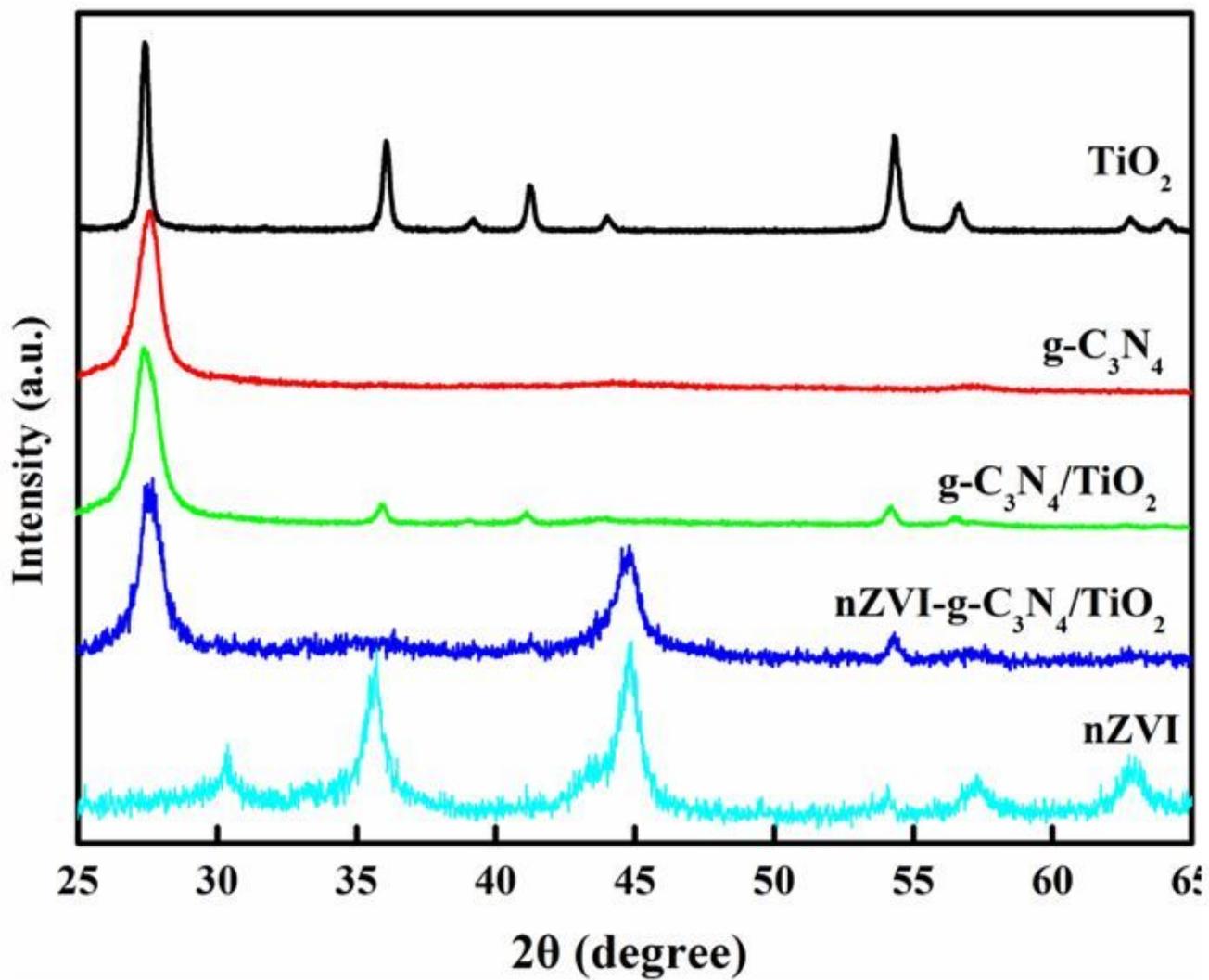


Figure 1

XRD patterns of nZVI, TiO_2 , $\text{g-C}_3\text{N}_4$, $\text{g-C}_3\text{N}_4/\text{TiO}_2$ and $\text{nZVI-g-C}_3\text{N}_4/\text{TiO}_2$ composite.

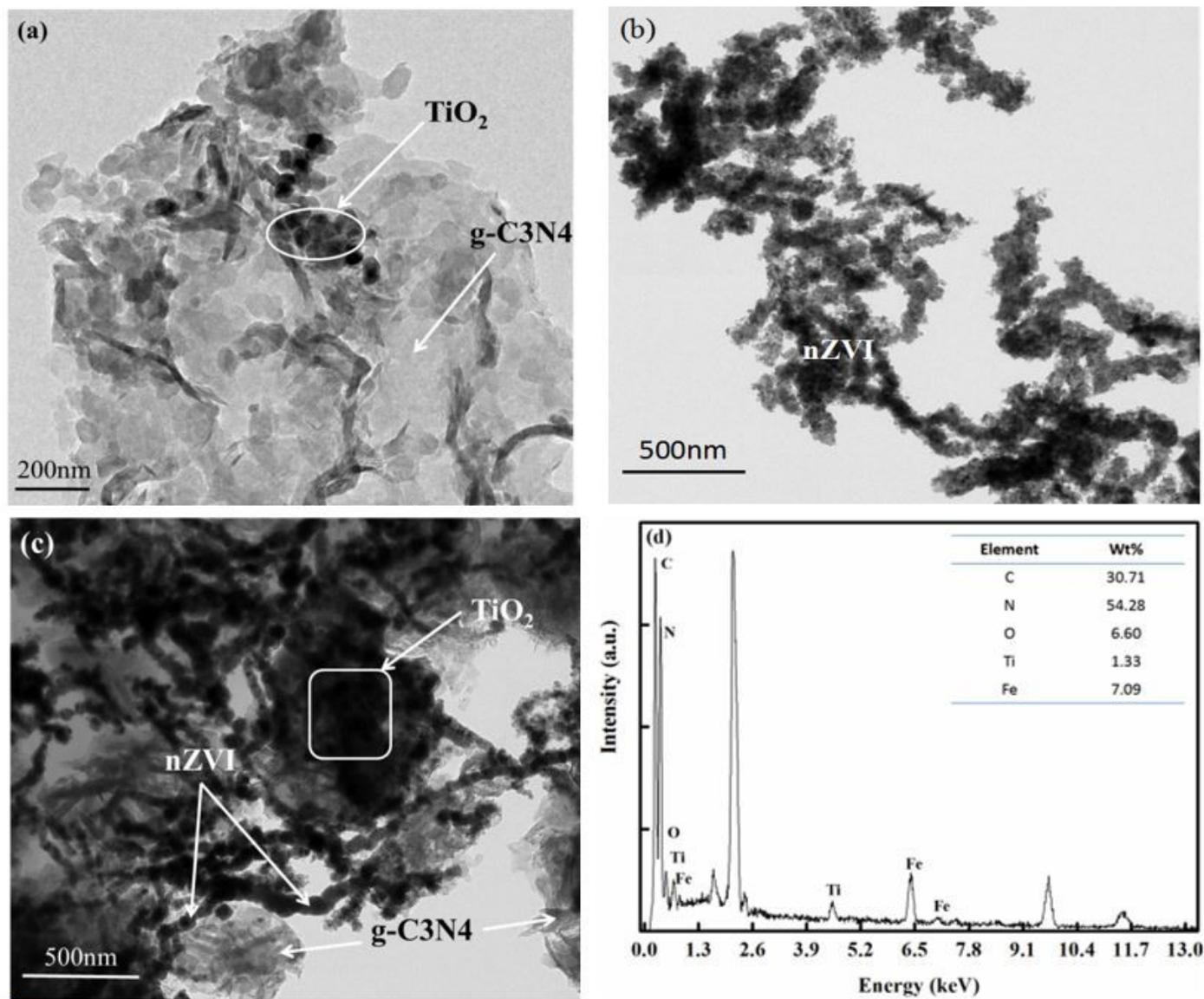


Figure 2

TEM images for (a) the g-C3N4/TiO₂; (b) the nZVI; (c) the nZVI-g-C3N4/TiO₂ composite; (d) EDS spectrum of the nZVI-g-C3N4/TiO₂;

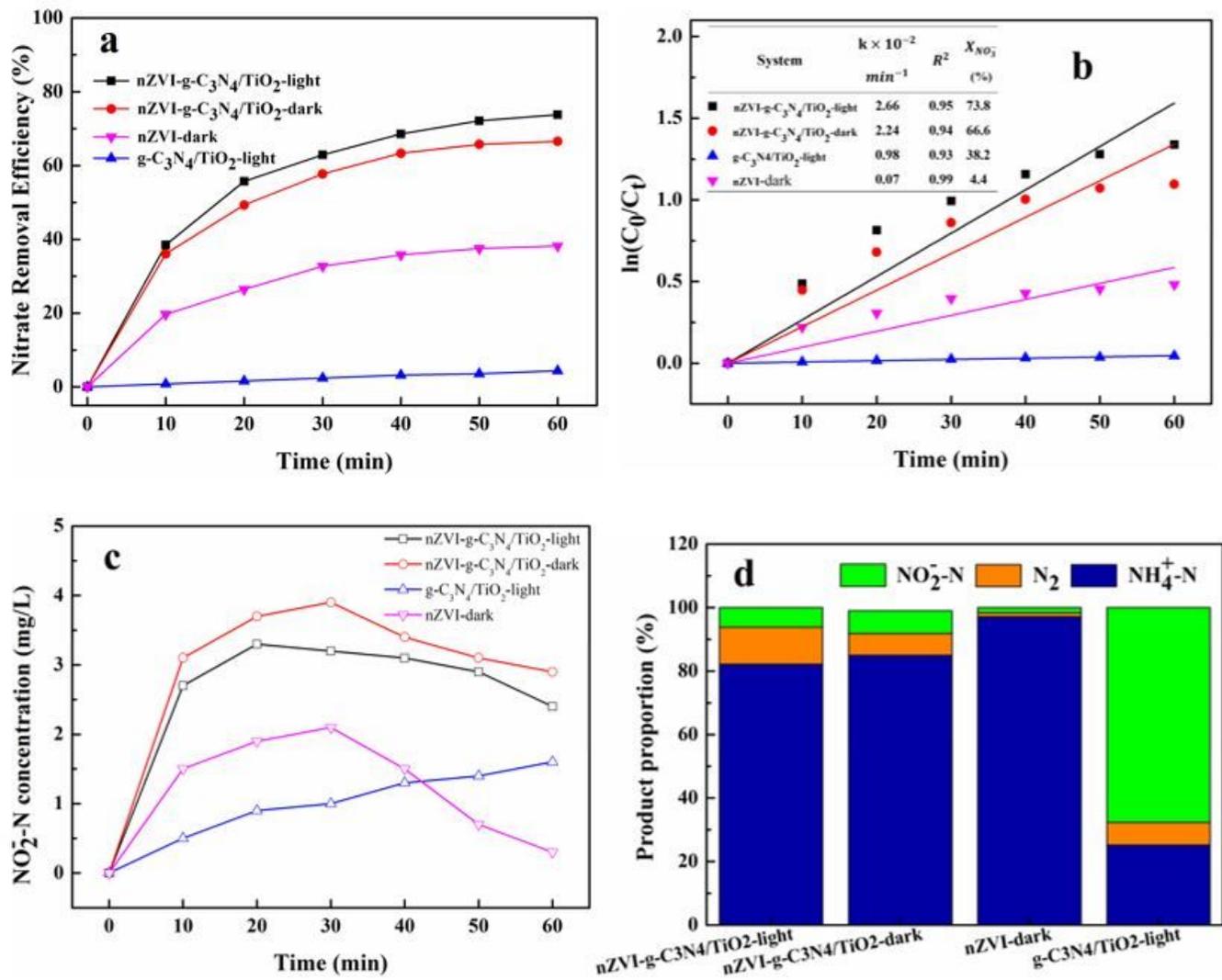


Figure 3

(a) Nitrate removal efficiency of nZVI, g-C₃N₄/TiO₂ and nZVI-g-C₃N₄/TiO₂ composites; (b) Rate constant of nitrate reduction in the different system; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different system; (initial nitrate nitrogen concentration at 50 mg/L; reductant dose at 4 g/L and initial pH at 7.0)

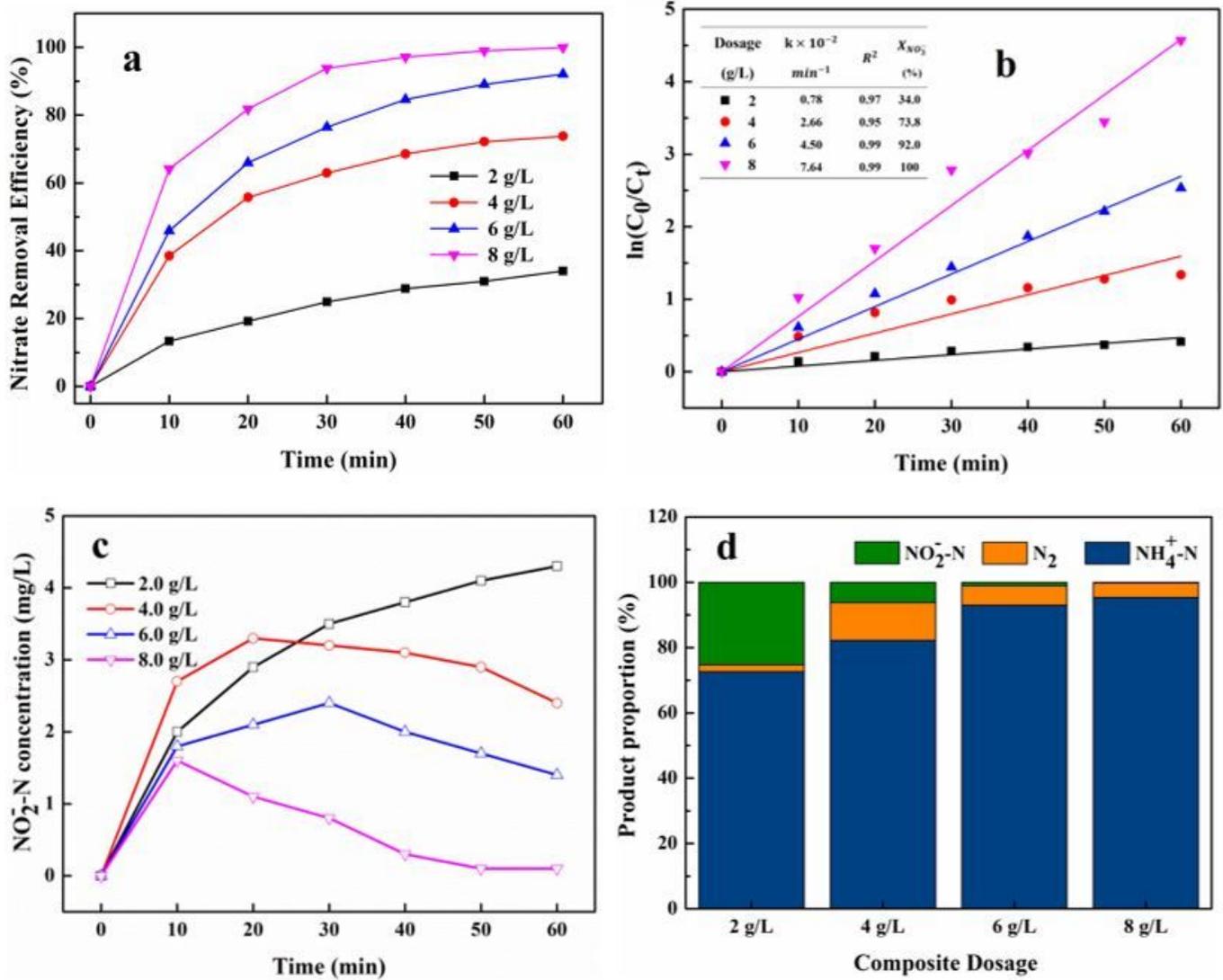


Figure 4

(a) Nitrate removal efficiency in the different nZVI-g-C3N4/TiO2 composite dosage;(b) Rate constant of nitrate reduction in the different composite dosage; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different composite dosage; (initial nitrate nitrogen concentration at 50 mg/L; initial pH at 7.0)

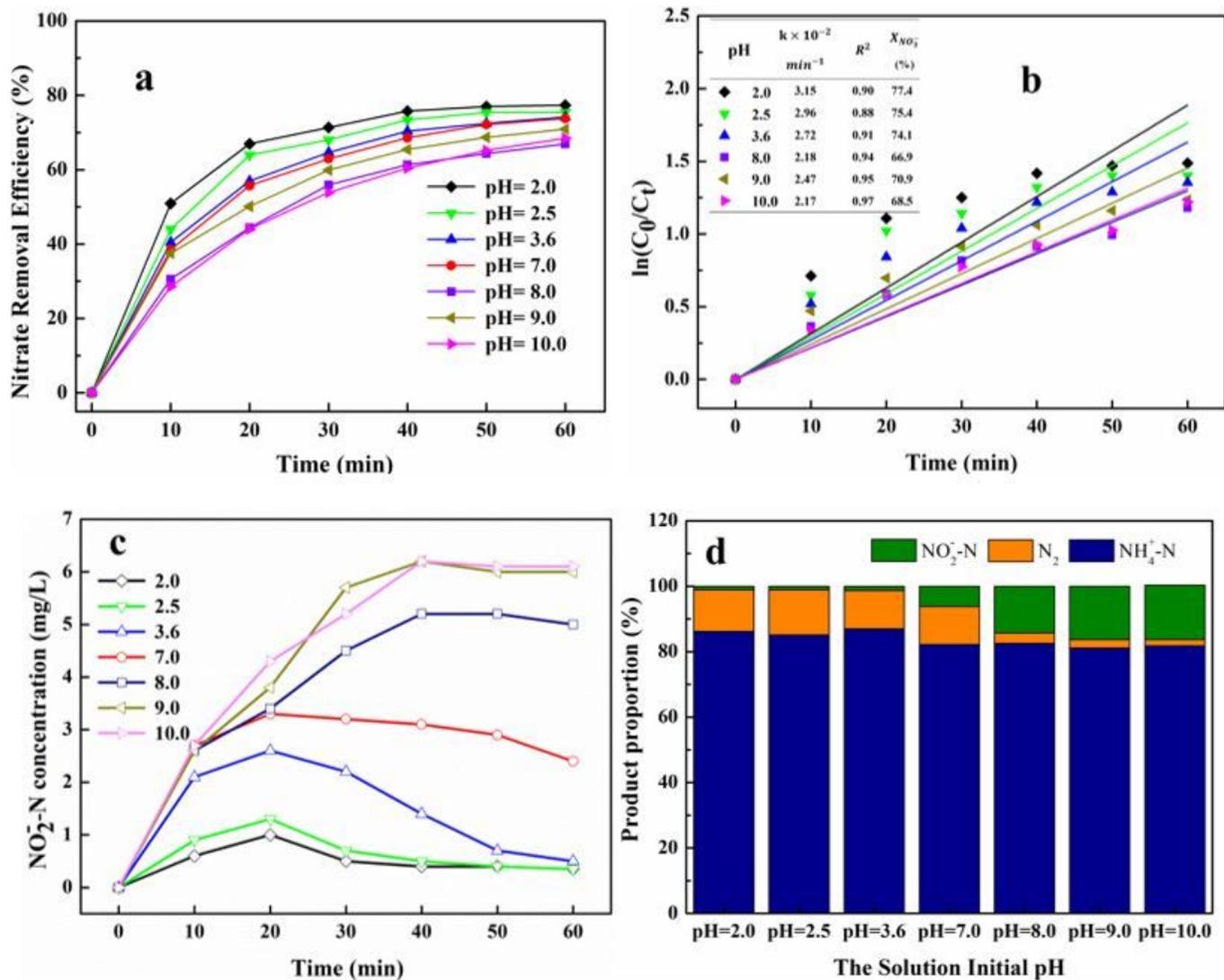


Figure 5

(a) Nitrate removal efficiency in the different solution initial pH; (b) Rate constant of nitrate reduction in the different Initial pH of solution; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different Initial pH of solution; (initial nitrate nitrogen concentration at 50 mg/L; reductant dose at 4 g/L)

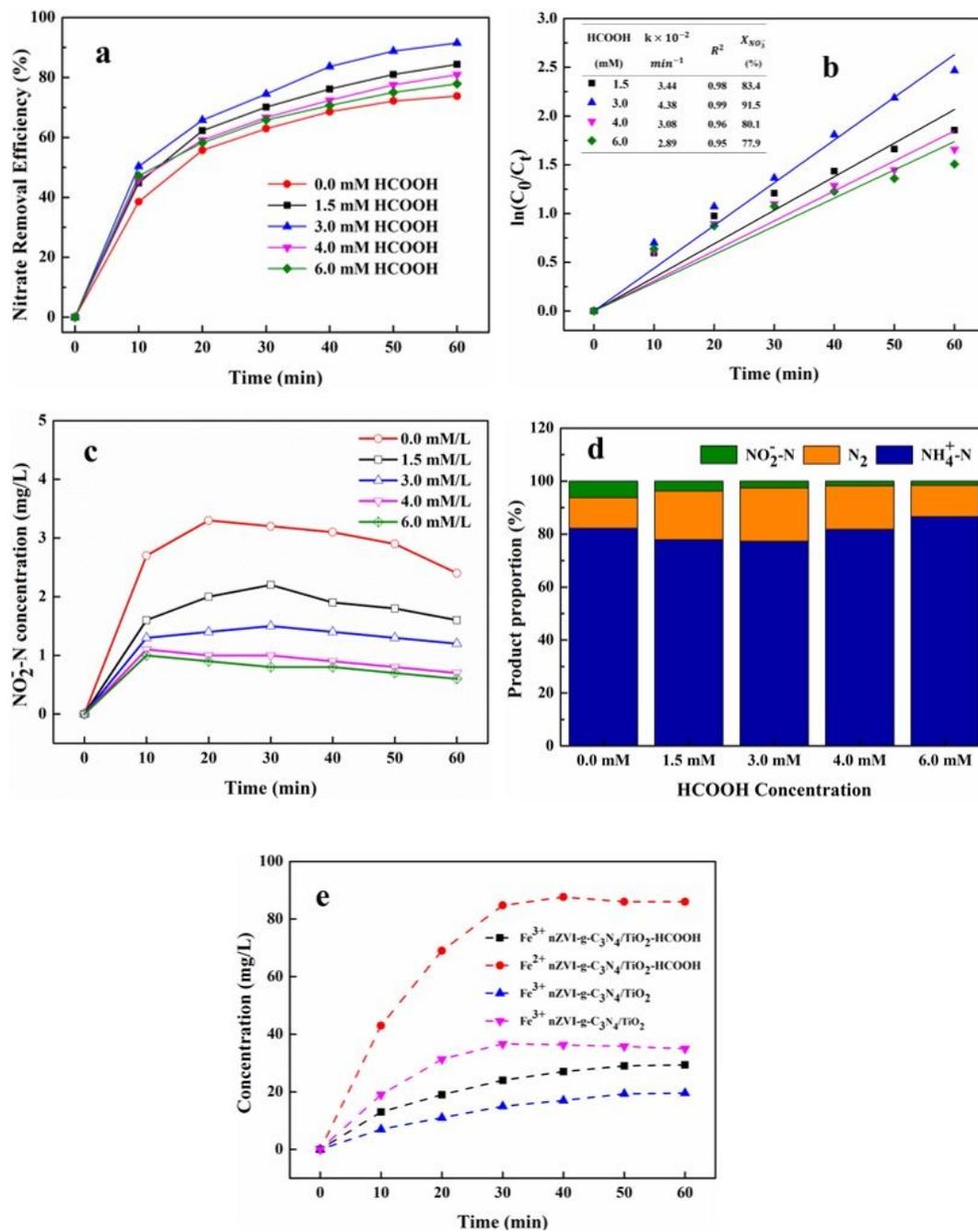


Figure 6

(a) Nitrate removal efficiency in the different HCOOH concentration; (b) Rate constant of nitrate reduction in the different Initial pH of solution; (c) nitrite nitrogen concentration (mg/L) changes during nitrate reduction; (d) Product proportion of nitrate reduction in the different Initial pH of solution; (e) and the concentration of Fe^{2+} and Fe^{3+} with time; (initial nitrate nitrogen concentration at 50 mg/L; reductant dose at 4 g/L)

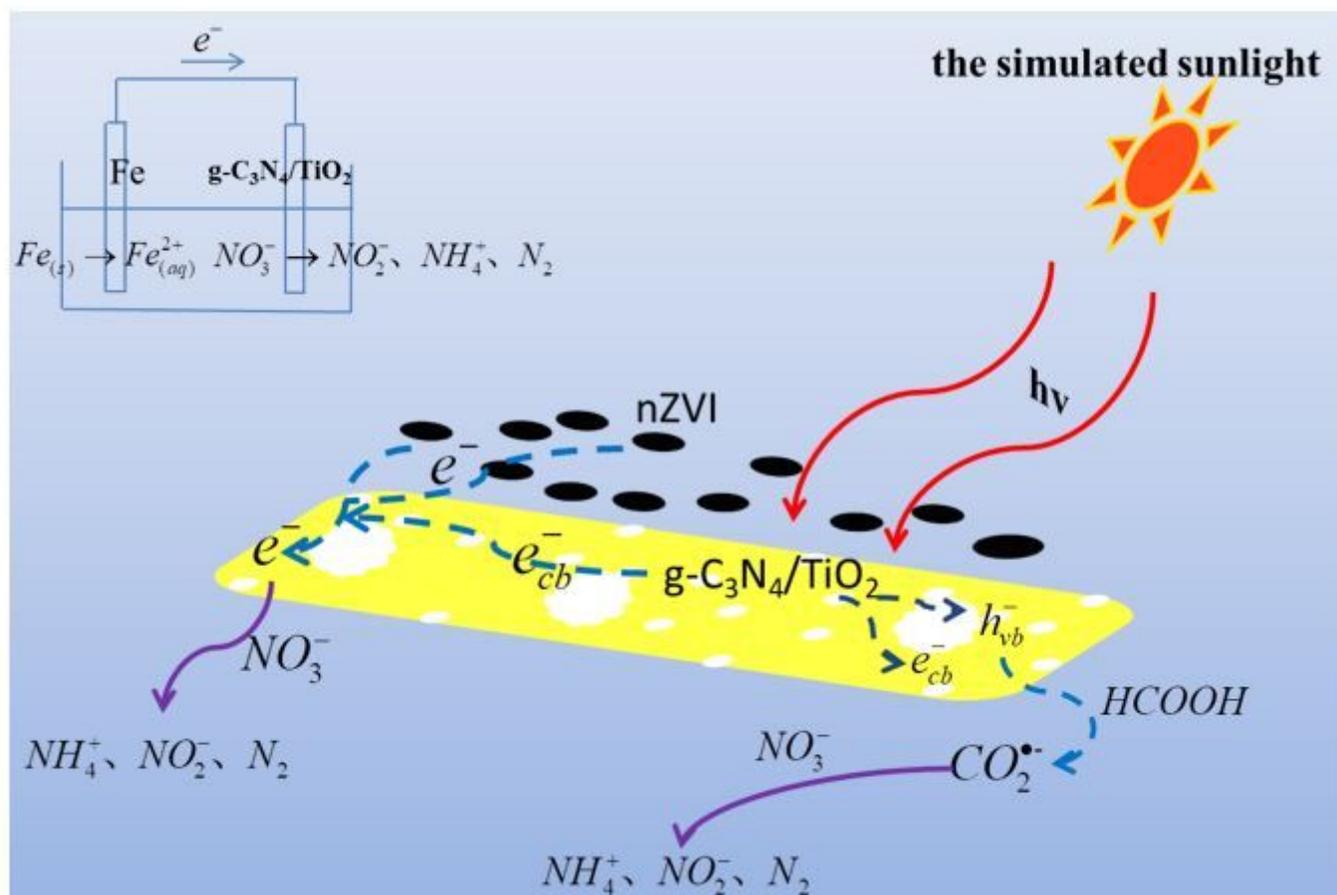


Figure 7

The Mechanism of Nitrate Reduction in the nZVI-gC₃N₄/TiO₂/HCOOH-Xe-lamp System

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