

# Development of a sensor and measurement platform for water quality observations: design, sensor integration, 3D printing, and open-source hardware

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## Research Article

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# 1 Development of a sensor and measurement platform for water quality observations: design, sensor 2 integration, 3D printing, and open-source hardware

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4 *Environmental Monitoring and Assessment*

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## 14 15 **Abstract**

16  
17 A measurement and development platform for collecting water quality data (the WaterWatcher) was  
18 developed. The platform includes sensors to measure turbidity, total dissolved solids (TDS), and water  
19 temperature as variables that are often collected to assess water quality. The design is extensible for  
20 research and monitoring purposes, and all design files are provided under open-source permissive  
21 licenses for further development. System design and operation are discussed for illustrative purposes. A  
22 block diagram indicates elements of mechanical, electrical, and software design for this system. The  
23 mechanical assembly used to house circuit boards and sensors is designed using 3D printing for rapid  
24 prototyping. The electronic circuit board acts as a carrier for an Arduino 32-bit microcontroller board  
25 and an associated cellular module along with a GPS for geolocation of water quality measurements. The  
26 cellular module permits data transfer for Internet of Things (IoT) functionality. System operation is set  
27 up using a command line interface (CLI) and C++ code that allows for calibration coefficients and human-  
28 readable transfer functions to be defined so that sensor voltages are related to physical quantities. Data  
29 are cached on a secure digital (SD) card for backup. The circuit was calibrated, and system operation  
30 assessed by deployment on an urban reservoir. Biogeochemical cycles were identified in the collected  
31 data using spectrogram and semivariogram analyses to validate system operation. As a system with  
32 hardware and software released under an open source license, the WaterWatcher platform reduces the  
33 time and effort required to build and deploy low-cost water quality measurement sensors and provides  
34 an example of the basic hardware design that can be used for measurements of water quality.

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43 photographs for Figure 1 of this paper.

## 44 Introduction

45  
46 Water quality refers to the properties of water that influence biological systems (Karr and Dudley  
47 1981). This includes civil engineering (Brabec et al. 2002) and toxicological applications (Vlaming et al.  
48 2000), where characteristics of water are measured for determination of hazards related to potable  
49 water use and ecosystem services. Pollutants and toxins from sewage, industrial waste, and stormwater  
50 runoff enters rivers and streams (Deblonde et al. 2011), potentially modifying biogeochemical cycles.  
51 Nitrogen and phosphorus from agricultural and domestic uses of fertilizers stimulate the growth of algae  
52 and other microorganisms, decreasing oxygen levels in water and causing eutrophication (Conley et al.  
53 2009). In some urban environments, runoff enters storm sewers (DeFilippi and Shih 1971) that convey  
54 solutes to stormwater retention ponds (Borne 2014) and surface hydrological systems (Marsalek 1991).  
55 Due to an increase in urbanization and a decrease in infiltration associated with a reduction of soil  
56 permeability, stormwater discharge has increased in recent decades, and water quality has decreased  
57 due to a concomitant increase in transported chemicals and ions (McGrane 2016).

58 In light of these aforementioned stressors, water quality is one of the central factors determining  
59 ecosystem functionality and the sustainability of human activities (Gleeson et al. 2020). Despite the  
60 importance of collecting water quality data, traditional techniques for sampling are prohibitive of early  
61 detection of changes (Madrid and Zayas 2007). This is because manual sampling involves the collection  
62 of data (either directly using handheld probes, or from lab analysis of samples) from a field site by  
63 human investigators, which increases cost and limits throughput. Therefore, there is a need for methods  
64 that allow for collection of data at higher temporal and spatial resolutions.

65 The Internet of Things (IoT) concept involves the use of embedded computing devices to collect  
66 and transfer data over a network for automation of observations and the associated display and analysis  
67 of data in near real-time (Ng and Wakenshaw 2017). IoT devices are designed to be ubiquitous and  
68 communicate over WiFi (L. Li et al. 2011), cellular (Mangalvedhe et al. 2016), or mesh radio networks (Yu  
69 et al. 2017) to transfer data between devices and systems (Suo et al. 2012). The collected datasets are  
70 used for decision-making (Lee et al. 2013), process control (Prathibha et al. 2017) or environmental  
71 modelling applications (Wong and Kerkez 2016). IoT intends to provide adequate spatial and temporal  
72 coverage to obtain data useful for predictions and forecasts.

73 Water quality data have been collected using Internet of Things (IoT) technologies. Water  
74 quality sensors have been deployed to monitor river (Chen and Han 2018) as well as inland water and  
75 maritime environments (Prasad et al. 2015), and have also been deployed on a robotic boat to obtain  
76 spatial estimates of water quality (T. Li et al. 2017). Commercial IoT sensor platforms have been utilized  
77 for this purpose (Wong and Kerkez 2016). Commercial devices are relatively expensive, and the use of  
78 commercial hardware can result in vendor lock-in (Willcox et al. 2018), resulting in the need to upgrade  
79 devices when deprecated by the manufacturer (Pal et al. 2018), and supporting the necessity of paying  
80 for access to software and associated technical support required for system functionality (Boehm and  
81 Abts 1999).

82 Water quality measurement systems have been implemented using experimental platforms  
83 involving a Raspberry Pi (Chandrappa et al. 2017; Gopavanitha and Nagaraju 2017; Raju and Varma 2017;  
84 Vijayakumar and Ramya 2015) and electronic evaluation kits (Das and Jain 2017; Geetha and Gouthami  
85 2017; Myint et al. 2017). However, the Raspberry Pi filesystem can become corrupted over time,  
86 resulting in system failure (Nadaf and Bonal 2019) and many evaluation kits are not intended for use in  
87 actual products due to long-term reliability (Texas Instruments 2011).

88 The Arduino platform provides easy-to-use hardware and software with an open source license  
89 (Badamasi 2014; Sarik and Kymissis 2010). Open-source hardware allows for design re-use and  
90 innovation and thereby enables a better understanding of system functionality due to the availability of  
91 schematics and associated design documentation (Fisher and Gould 2012; Pearce 2012). Open-source

92 software also allows for code reuse: since the source code is available, software functionality can be  
93 easily extended and modified (Bonaccorsi and Rossi 2003; Fitzgerald 2006), especially when permissive  
94 licenses such as the GNU GPL allow for freedom of use (Di Penta et al. 2010). Arduino-based platforms  
95 have been used to collect water quality data and exchange data over WiFi (Chowdury et al. 2019;  
96 Parameswari and Moses 2019; Pasika and Gandla 2020), Zigbee (Encinas et al. 2017; Kamaludin and  
97 Ismail 2017; Pranata et al. 2017), LoRa (M. Saravanan et al. 2017) and cellular (Moparthi et al. 2018; K.  
98 Saravanan et al. 2018) networks. However, most of these water quality measurement projects, although  
99 based on open-source hardware and software technologies, do not provide the complete design under a  
100 permissive open-source license. This does not allow previous research work to be easily re-used to  
101 create additional systems.

102 This paper introduces a floating water quality measurement platform with open-source  
103 hardware and software that can be utilized to develop water quality measurement applications without  
104 the need to replicate some common system components. This platform is named the “WaterWatcher.”  
105 The hardware of the WaterWatcher platform is based around a custom electronic circuit that serves as a  
106 carrier printed circuit board (PCB) for an Arduino microcontroller. The microcontroller is interfaced to a  
107 cellular communications module. A 3D-printed enclosure is used to house the circuit board and provide  
108 a mounting platform for solar panels that power the circuit and charge an on-board Lithium-ion battery.  
109 The 3D-printed enclosure, circuit board design files, and Arduino code are provided as an associated  
110 download licensed under permissive open-source licenses. The WaterWatcher platform is intended to  
111 enable future innovation and development of water quality measurements by the scientific community.  
112 This paper is also intended for educational or teaching purposes and serves as an overview of the ideas  
113 and technology for water quality measurements.

114  
115

## 116 **Materials and methods**

117

### 118 *Block diagram and system operation*

119

120 Electronic sensor systems for observations of water quality have common features as identified  
121 by the block diagram of the WaterWatcher system (Figure 1). There are three canonical sensors attached  
122 to the system: turbidity, total dissolved solids (TDS), and temperature. Additional sensors for chemical  
123 measurements can be eventually added. A 3D model of the PCB for this platform implementation is  
124 shown in Figure 2a, whereas the assembled PCB is shown in Figure 2b.

125 An analog frontend provides signal conditioning for voltage inputs from sensors that measure  
126 turbidity and TDS. These two sensors are utilized for water quality estimates by many studies and were  
127 therefore provided for use in this development platform. Temperature influences TDS determined using  
128 an empirical sensor calibration curve (Rusydi 2018) and temperature also influences water chemistry  
129 kinetics (Gholizadeh et al. 2016; Paul et al. 2019), so a temperature sensor should always be included.

130 Turbidity is related to particulate matter from erosion, sewage, geological, and biological  
131 sources. The particulate matter present during periods of higher turbidity reduces photosynthetic  
132 production, increasing absorption of solar radiation and water temperatures (Davies-Colley and Smith  
133 2001) and decreasing dissolved oxygen levels (Henley et al. 2000). Turbidity levels are used to assess the  
134 quality of drinking water since higher amounts of particulate matter can provide environments for  
135 pathogens (Farrell et al. 2018). Electronic turbidity sensors are usually optical and relate light extinction  
136 to Nephelometric Turbidity Units (NTU) (Davies-Colley and Smith 2001).

137 Total dissolved solids (TDS) are a measure of chemical and biological substances that exist as  
138 molecules, ions, or colloids in the water. Higher levels of TDS are related to greater amounts of dissolved

139 substances (Weber-Scan and Duffy 2007). Electronic TDS sensors relate parts-per-million (ppm) TDS to  
140 electrical conductivity (Ivan et al. 2011).

141 Inputs can also be added for additional sensors for measurement of water temperature  
142 gradients at depths below the water surface. These additional sensor inputs can be digital and attached  
143 to a multidrop bus. The WaterWatcher uses the 1-wire bus (Dudak et al. 2018) where multiple sensors  
144 are attached to the same wired connection and each sensor is associated with a unique address. The  
145 temperature sensor used for the WaterWatcher is digital as an application-specific integrated circuit  
146 (ASIC) since the use of an ASIC decreases complexity.

147 The main microcontroller enables periodic sampling of analog and digital inputs. Interfaced with  
148 a cellular communications module, the microcontroller periodically sends data to a base station or  
149 server. However, since radio frequency (RF) communications are not always reliable due to topographic  
150 and environmental effects or infrastructure failure, there must be a means for data to be locally cached.  
151 This enables data to be retrieved later in the field or to be re-sent to the server at a time when the circuit  
152 can communicate with a network. A ubiquitous flash memory device for storing data is an SD card that  
153 is readily available from commercial sources. The SD card can be extracted and inserted into a reader to  
154 transfer data to a computer for analysis. A USB bus allows for Machine-2-Machine (M2M)  
155 communications where system operation is configured using a computer.

156 A GPS receiver module provides geographic location and elevation data. Although the water  
157 quality measurement platform might be installed at a stationary location in, e.g., a stormwater retention  
158 pond or reservoir, GPS measurements allow for WaterWatcher devices to be located on a web map  
159 interface or to be tracked for property inventory purposes. Moreover, if the water quality measurement  
160 platform is towed behind a boat or set adrift in a river or reservoir, geographic location can be related to  
161 spatial changes in water quality.

162 The system requires DC power and cannot be easily interfaced to AC power via a converter since  
163 water quality devices are often placed in bodies of water at remote locations and field sites. The  
164 WaterWatcher therefore requires a battery charger system interfaced to solar panels. To reduce the  
165 overall mass of the system, the batteries are Li-ion cell chemistry, but a protection circuit is also required  
166 to limit the rate of charge, reduce overcharge and over-discharge, and also ensure that a battery fault  
167 does not cause an explosion or fire (Salerno and Korsunsky 1998).

168 To protect the WaterWatcher circuit from water ingress and to provide a mounting platform for  
169 the water quality sensors, a mechanical enclosure is required. This mechanical enclosure can be created  
170 from plastic. To allow for rapid prototyping and modification (Oropallo and Piegl 2016), the enclosure is  
171 3D-printed for prototyping and low-volume applications.

172 At the time of writing, the cost of mechanical parts and electronic circuit boards is under \$1,000  
173 USD. The WaterWatcher can thereby be created at a fraction of the cost of commercial water quality  
174 sensor platforms.

175

176

### 177 *Mechanical design*

178

179 The mechanical design for the WaterWatcher floating water quality sensor platform is shown as  
180 an exploded diagram (Appendix A) and a computer rendering as Figure 3a. Although buoy design can be  
181 conducted with specialized software packages that allow for modeling of wave interaction with the  
182 structure (García et al. 2018), we used a standard mechanical CAD system to maximize reproducibility  
183 and design sharing since this type of software is more readily available to researchers.

184 Mechanical design calculations are performed separately in accordance with engineering  
185 principles, and since the platform is intended for use at inland water locations, it is less important to  
186 model wave action thoroughly using numerical models. Design calculations ensure that the platform has

187 a high enough metacentric height to guarantee static stability and sufficient period of roll to prevent  
188 internal damage of wiring during wave action. These are design goals nominally associated with marine  
189 structures (Terada et al. 2019).

190 Although a proprietary CAD system was used for the design, STEP files are also provided in a  
191 vendor neutral format for use with open-source CAD software packages or for 3D printing. All assembly  
192 pieces shown on the diagram were printed on an engineering-grade 3D printer (Fortus F370, Stratasys  
193 Inc) using acrylonitrile styrene acrylate (ASA) plastic. ASA plastic was chosen since this material is UV-  
194 stabilized for outdoor locations and is similar in hardness to ABS plastic. Support material was used by  
195 the 3D printer to create holes. After removal of the support material in a detergent bath, the holes were  
196 functional and precisely located as specified by the mechanical CAD design. This eliminated the need for  
197 drilling of holes after 3D printing and reduced a step of the manufacturing process. The following  
198 paragraphs indicate alphabetic identifiers on the diagram provided in Appendix A.

199 A bottom rudder (A) is fastened to a circular inner assembly (B) that provides a conduit for wires  
200 and a mounting point for the three basic sensors that measure turbidity, TDS, and temperature.  
201 Analogous to rudders on boats (Liu and Hekkenberg 2017), the rudder allows the sensor platform to  
202 travel with the flow in a river or stream. The rudder can be turned to different cardinal directions by  
203 removing the fasteners and updating the 3D model. Additional holes created in the circular inner  
204 assembly (B) can accommodate wires for additional sensors.

205 The circular inner assembly (B) is attached by fasteners to two carbon fiber (C) plates glued  
206 between polyethylene foam sheets (D, E). The edges of the sheets are rounded to prevent mechanical  
207 disaggregation of the sheets if a collision occurs. This distributes the collision force over a larger surface  
208 area.

209 Regions of the bottom foam sheet (D) were removed to ensure that the inner assembly and the  
210 carbon fiber plates are flush with the foam sheet surface. The removal was done by hand, but a CNC  
211 machine can also be used. The removal of material ensures that the foam sheets can be glued together  
212 without a gap. The carbon fiber plates (C) were glued together using a marine adhesive epoxy.

213 The platform is assembled in a stacked fashion by threaded rods (F) inserted into holes created  
214 in the circular inner assembly. The rods are held in place by nuts inside of the circular inner assembly. A  
215 cap (G) protects against water ingress and provides a seating plane for the upper part of the assembly. A  
216 hole is created through the top of the cap to admit wires from the sensors.

217 A plate (H) with holes is placed on top of the polyethylene foam sheets. The plate is held in  
218 place by the threaded rods and provides a mounting location for GPS and cellular antennas. Conduits for  
219 the coaxial cables connected to each antenna are created in the foam. The plate was divided in half to  
220 not exceed the lateral build dimensions of the available 3D printer. This entails printing the single plate  
221 as two separate plastic pieces that are later joined together.

222 A plastic parallelepiped (I) is placed on top of the threaded rods. Holes on opposite sides of the  
223 parallelepiped allow for the coax cables from the GPS and cellular antennas to be brought into the  
224 internal cavity and connected to the PCB (Figure 2). The sides of the parallelepiped are recessed to hold  
225 solar panels (J) glued to the sides using a marine epoxy. The solar cells are placed on all sides of the  
226 parallelepiped to maximize electrical power output.

227 Another cap (K) and a similar plastic parallelepiped (L) are placed on top of the lower  
228 parallelepiped (I). The threaded rods (F) are used to stack together the two parallelepipeds. The top  
229 parallelepiped has threaded inserts to admit bolts that fasten on a lid (M). Integrated into the lid is a  
230 holder for the PCB (N). The PCB is bolted to the holder (Figure 2b) along with a RF (radio frequency) bias  
231 tee module to provide power to the active GPS antenna. The top of the lid has a holder for a solar-  
232 powered strobe light (O). The strobe light (O) is inserted into the holder and glued in place.

233 During and after assembly, a silicone sealant was applied to waterproof portions of the design to  
234 protect against water ingress. A sprayable sealant was applied to all surfaces for weatherproofing and to

235 fill in small gaps in the plastic. Since ASA tends to shrink after printing, the sealant further waterproofed  
236 the mechanical assembly.

237 The total height of the assembly from the bottom of the rudder to the top of the strobe light is  
238 36 inches (91.4 cm). The maximum width of the foam is 18 inches (45.7 cm) and the maximum length is  
239 24 inches (61 cm). These dimensions indicate that the WaterWatcher is a compact platform for water  
240 quality measurements, and it has been successfully deployed and retrieved by a single person from a  
241 canoe.

242 Images of assembly are available for download. The images are licensed under a permissive  
243 license and serve as an example of how the WaterWatcher was assembled.

244

245

## 246 *Electrical design*

247

248 Appendix B provides schematics for the circuit. Two analog inputs (A0 and A1) allow for  
249 digitization of voltages from turbidity and TDS sensors. The analog inputs are connected to  
250 microcontroller port pins set up as analog inputs. The microcontroller has an integrated 12-bit ADC for  
251 digitization of voltages and a nominal resolution of 0.8 mV for a configured internal voltage reference of  
252 3.3 V.

253 Op-amp U23A is configured as a unity gain buffer to provide a high-impedance input for the  
254 turbidity sensor. A voltage divider comprised of resistors R35 and R36 scales the maximum sensor  
255 voltage to be less than 3.3V as the input to a microcontroller port pin configured as an analog input. Op-  
256 amp U23B is another unity-gain buffer that provides a low driving impedance to the analog input port  
257 pin so that the accuracy of the measurement is not affected. Diode D3 is a low-capacitance electrostatic  
258 discharge (ESD) protection diode.

259 Since the TDS sensor voltage output is pre-processed using circuitry on a small PCB provided  
260 with the sensor module, the driving impedance is low enough to directly interface this sensor to the  
261 analog input. An ESD diode D4 also protects the input. Similar diodes are also used for ESD protection  
262 on other inputs shown throughout the schematic.

263 A 1-wire multidrop bus (D0) is implemented using microcontroller GPIO bit-banging. A 1-wire  
264 temperature sensor to measure water temperature is attached to this bus. The 1-wire bus has multidrop  
265 communications, where each sensor on the bus has a unique serial number and is enumerated using a  
266 bus protocol. As per the name, only one wire is used for the bus and another for electrical ground (GND)  
267 (Eisenreich and DeMuth 2003, pp. 345–369). Similar to other digital busses, the maximum number of  
268 devices added to the bus is limited only by wire connection resistance and capacitance allowing for  
269 dozens of sensors to be added. Linear regulator U22 provides power to the temperature sensors.

270 Headers J1 and J2 connect two 3.7 V Li-ion batteries with a capacity of 2 A hr in series to provide  
271 a 7.4 V nominal source. U3 is an overvoltage protection IC that also performs cell balancing to ensure  
272 that the voltages of each battery are approximately equal during charging and discharging. This  
273 increases efficiency and battery life and protects against thermal runaway that can create a fire hazard.  
274 U1 and U2 are field effect transistors (FETs) with integrated charge pumps and current-limiting circuitry  
275 that limits the maximum bi-directional current flow to the battery. U4 is a battery monitor with a charge  
276 integrator that reports the battery state-of-charge. An ADC integrated into U4 is connected to header J3  
277 to provide another ADC input (identified as A2). ADC input A2 can be used to measure the voltage  
278 output of another sensor.

279 The battery charger U5 provides maximum power point tracking (MPPT) for solar panels to  
280 ensure that the batteries are efficiently charged when enough solar energy is present. Each solar panel  
281 has a 9 V nominal open circuit voltage with a current of 220 mA for a maximum output power of approx.  
282 2 W. Connecting the cells in the configuration shown results in a maximum 18 V open circuit voltage

283 with a maximum current of 880 mA for a maximum output of approx. 16 W. Diodes D7 and D9 allow for  
284 the solar panels to power the circuit directly or when the battery is dead or not present.

285 The power supply built around U17 utilizes a switch-mode topology with inductor L4. This  
286 power supply is more efficient than a linear regulator to provide a 5 V main system rail. The input to U17  
287 is filtered using an LC filter to reduce the effects of electromagnetic interference (EMI). U18 is a FET with  
288 integrated charge pump that acts as a switch to turn on and off the external 5 V rails that provide power  
289 to the sensors. This conserves current since the 5 V rail is only turned on during the time of a  
290 measurement.

291 U7 is a GPS module. Linear regulators U8 and U9 provide a quiet power supply to the GPS to  
292 reduce noise from the 5 V main system rail. U8 is the main linear regulator whereas U9 serves as a  
293 battery backup for the GPS, reducing the time to first fix (TTFF) when the main supply to U8 is turned off  
294 between measurements to conserve battery power.

295 U20 is a unique serial number that identifies each circuit board. Linear regulator U21 provides  
296 current to a real-time clock (RTC), a port expander (U24), and a buffer (U15). The RTC provides a  
297 timestamp for each observation and allows for measurements to be taken on a schedule ranging from  
298 minutes to hours. The port expander samples battery state and is used to determine if there is a battery  
299 fault or if the battery is charging.

300 Buffer U15 protects against current flow to the GPS module when it is powered down and serves  
301 as a Faraday shield (Zumbahlen 2008, pp. 845–846) for reduction of logic noise from the main  
302 processor module port pins configured as a TTL serial port. The Arduino MKR GSM 1400 module (U14) is  
303 based around a 32-bit ARM processor interfaced to a cellular chipset for IoT connectivity. A SIM card is  
304 inserted into the module. For this reference implementation, we initially used the Hologram.io cellular  
305 platform to exchange data: the platform is inexpensive, provides a REST API for implementation of web  
306 services, and is supported for use with the Arduino ecosystem. Later experimentation utilized a web  
307 server with a web framework to store data in a custom database.

308 The main processor module U14 is interfaced to an SD card by a serial peripheral interface (SPI)  
309 bus. The SD card is operated in SPI mode in lieu of a 4-bit parallel bus since the main processor module  
310 lacks a hardware SD card master but analogous to most microcontrollers incorporates an SPI master. For  
311 power-down between measurements, linear regulator U16 is turned off by the main processor module.  
312 To prevent current flow between the main processor module port pins and the SD card during power-  
313 down, all port pins connected to the SD card are set as inputs.

314 A micro-USB connector on the main processor module U14 serves to implement a USB serial  
315 port that provides a command line interface (CLI) for the WaterWatcher. The CLI allows for the sampling  
316 platform to be configured and tested.

317

318

### 319 *Software design*

320

321 The software design for the WaterWatcher is based around the Arduino platform for  
322 reproducibility and to reduce the amount of effort required for modification. Although existing Arduino  
323 software libraries were used as required, custom code was also created for the RTC U19, port expander  
324 U24, battery monitor U4, and serial number integrated circuit U20. This ensured flexibility in the context  
325 of the application. The SD card library required for reading and writing the FAT filesystem was FatFs  
326 (version 86604) with a custom media access interface written specifically for SPI communications. This  
327 custom implementation was chosen over Arduino-provided SD card libraries to ensure that high-capacity  
328 exFAT cards could be used as interfaced to the SPI bus. The use of exFAT cards allows for years of data to  
329 be stored on a single card.



330 An example of the setup is provided as C++ code in Table 1 as an Arduino sketch file. Arduino  
331 code requires two functions: `setup()` and `loop()`. The `setup` function initializes the hardware, whereas  
332 the `loop` function is an infinite loop that checks the state machine logic implemented by the code.

333 An instance of the `WaterWatcher` class is created as a global object in the main sketch. The  
334 `setup` is implemented by a call to class member `setup()`. The check of internal state is implemented by a  
335 similar call to class member function `checkState()` in the `loop()` function. These are the only required  
336 functions in the user code and the `WaterWatcher` class encapsulates functionality. Additional  
337 functionality, such as the sampling interval, is set using the Command-Line Interface (CLI).

338 The basic structure of the code in Table 1 can be modified if required to add additional  
339 functionality. The code demonstrates how the `WaterWatcherOptions` sub-class is inherited from the  
340 associated base class to override transfer functions that provide processed analog outputs relating a  
341 voltage to a physical measurement such as turbidity or TDS. The processed water temperature can also  
342 be adjusted based on calibration. The analog channels are set to sample or not to sample during a  
343 measurement.

344 Table 2 lists commands entered using the CLI when the `WaterWatcher` is attached to a host  
345 computer via the USB cable. The commands allow for various sub-systems to be read, specify whether  
346 the data is to be sent over cellular, and indicate whether the system is to enter a power-saving mode.  
347 CLI arguments are separated by spaces. As indicated in the table, some settings can be saved into non-  
348 volatile flash memory using the *write-flash* command. These settings are reloaded after each power  
349 cycle. The total length of non-volatile strings saved into flash memory is limited by the amount of flash  
350 memory available for storage.

351 Data can be stored on the SD card in JSON (JavaScript Object Notation) format. CSV (Comma-  
352 Separated Values) format has been nominally used by dataloggers and is not self-documenting. JSON  
353 format is widely used for data interchange and is human-readable (Bassett 2015). Each object is clearly  
354 identified, unlike CSV that relies on additional metadata to identify the contents of each column. Most  
355 programming languages (including R and Python) can easily parse JSON and convert this format to CSV  
356 or other table-based formats. The code can be modified to store data in CSV or JSON formats.

357

358

### 359 *Laboratory testing and calibration*

360

361 The `WaterWatcher` was placed into a tank at the Toxicology Centre, University of Saskatchewan  
362 (Figure 3b). Waves were created in the tank by displacement to test the buoyancy and stability of the  
363 platform (Figure 3c). A video of the wave testing experiment is provided in the associated downloads for  
364 this paper.

365 A commercial multiparameter sonde equipped with turbidity and TDS sensors (EXO2, YSI  
366 Incorporated, Yellow Springs, Ohio, USA) was also inserted into the tank and used to collect comparison  
367 data to relate `WaterWatcher` sensor voltages to turbidity and TDS. The tank was filled with deionized  
368 water and fitted with a standpipe to allow it to overflow. Commercially available coffee whitener and  
369 sodium chloride was used to create water with defined turbidity and TDS. After starting the readings, a  
370 constant flow of deionized water was used to dilute the colloid and salt. This caused a time-dependent  
371 drop in turbidity and TDS following first-order kinetics. All laboratory data were logged to the SD card  
372 using a 5-minute sampling interval. The same 5-minute sampling interval was also used for the YSI  
373 sonde. Data were collected for approximately 31 hours for a total of 365 samples.

374 The data were subjected to statistical analysis. Additional plotting and analysis were conducted  
375 using the Python programming language and the source code provided for download.

376

377

## 378 *Field deployment*

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380 The WaterWatcher was deployed at an urban reservoir (Aspen Ridge Forebay) situated near the  
381 Northeast Swale within the municipal boundaries of the City of Saskatoon, Saskatchewan, Canada  
382 (Figure 4). The urban reservoir is a pond with engineered storm drain discharge from surrounding  
383 neighborhood locations.

384 The Northeast Swale is a geographical area representative of ecosystem diversity with native  
385 grassland, wetlands and rare species that are subjected to increasing urban land use (Shen et al. 2019).  
386 The WaterWatcher was anchored to the bottom of the reservoir using coated aircraft cable and a  
387 concrete weight. To conserve power, measurements of turbidity, TDS and temperature were collected  
388 every 30 minutes, cached on the SD card, and sent via cellular communications to a server.

389

390

## 391 **Results and discussion**

392

### 393 *Laboratory testing and calibration*

394

395 The wave-testing experiment (Figure 3c) showed that the platform did not capsize during water  
396 turbulence and demonstrated the veracity of the engineering design. Since water ingress was not  
397 observed after more than a week of the sensor floating in the tank, we deemed the enclosure sealing  
398 and the plastic thickness to be suitable for a waterproof design demonstrating system operation. This  
399 does not preclude the possibility of leaks arising over time, or water ingress from total submersion of the  
400 WaterWatcher, necessitating the need for maintenance and possible repair between field deployments  
401 in a similar fashion to commercial sensors.

402 As determined from laboratory testing and calibration, Figure 5a shows the relationship between  
403 turbidity and voltage as well as the associated model found by curve-fitting. Figure 5b exhibits similar  
404 relationships and curve-fitting models related to TDS.

405 Polynomial curve-fitting was used to smooth the output voltage time series of the  
406 WaterWatcher turbidity sensor. The sensor voltage was related to YSI sonde turbidity measurements  
407 using polynomial curve-fitting subject to the constraint that the polynomial must be monotonic to model  
408 a decrease in turbidity over the time of experiment. This is to ensure that higher output voltages are  
409 always correlated with lower turbidities. Since the turbidity sensor measures turbidity by light  
410 extinction, lower levels of turbidity will be associated with less light extinction and higher voltages.  
411 A univariate spline model was then used to obtain a function relating turbidity sensor output voltage to  
412 turbidity (Figure 5a).

413 After polynomial curve-fitting to initially smooth the output voltage time series of the  
414 WaterWatcher TDS sensor, 2D polynomial curve-fitting was used to obtain a function relating the output  
415 voltage and water temperature to TDS as measured by the YSI sonde (Figure 5b). The function outputs  
416 were corrected for linear offsets to compensate for differences between tank and field observations  
417 associated with differences in temperature and fluid mixing processes. Table 3 shows that the Root  
418 Mean Squared Difference (RMSD) and Mean Bias (MB) are sufficiently low for the calibration  
419 experiments and this indicates that the models adequately characterize relationships between turbidity,  
420 TDS and associated voltages.

421 The theoretical measurement resolution  $M_r$  was estimated by converting the microcontroller  
422 ADC resolution to NTU and ppm using a transfer function  $f(v)$  determined using calibration curve-fitting  
423 and by averaging a difference as shown in Equation (1) below over the calibration range of voltages.

424

$$M_r = \frac{1}{N} \left| \sum_{i=1}^N [f(v_i) - f(v_i + \Delta v)] \right| \quad (1)$$

425  
426  
427 The  $v_i$  is the voltage output of a sensor (turbidity or TDS) measured at a known water temperature,  $i$  is  
428 an index, and  $N$  is the number of discrete data values collected during the experiment. The  
429  $\Delta v = 0.8$  mV is the voltage resolution of the 12-bit ADC and  $v_1 = \Delta v$ . The theoretical measurement  
430 resolution  $M_r$  for turbidity and TDS was estimated (Table 3). Although the actual measurement  
431 resolution will be lower due to circuit noise and sensor circuit errors associated with non-linearities and  
432 component variation with respect to time and temperature, this theoretical resolution is likely sufficient  
433 to characterize water quality processes at a field site.

434 The 12-bit resolution is not as accurate as some commercial sensors that may use an ADC with a  
435 higher number of bits but digitization of voltages using this resolution can provide an estimate of water  
436 quality using low-cost electronics associated with an IoT open-source platform. A higher-resolution  
437 external ADC can be added as a circuit board revision for providing more accurate measurements along  
438 with additional front-end circuitry such as a programmable gain amplifier (PGA). The PGA can be used to  
439 change the amplification of the voltage inputs, thereby allowing for smaller voltages to be measured  
440 more precisely.

441 The CLI allowed for system functionality to be expeditiously tested during calibration. At an  
442 indoor location with an average light flux exceeding  $5 \text{ W m}^{-2}$  from artificial lighting, the microcontroller  
443 module was observed to operate using power provided by the solar cells when the batteries were  
444 disconnected, demonstrating the efficiency of the switch-mode topology power supply design. However,  
445 the Li-ion batteries are still required to provide additional power for reliable GPS, SD card and cellular  
446 modem operation. The system current consumption during field deployment is discussed in the sections  
447 below.

448

449

#### 450 *Field deployment*

451

452 Figure 6 shows turbidity (a) and TDS (c) time series observations collected by the WaterWatcher  
453 at the Aspen Ridge Forebay. To characterize cyclical biogeochemical processes occurring at this location,  
454 the time series of turbidity and TDS were subjected to spectrogram analysis (b, d). The spectrogram  
455 vertical axis is expressed in Fractional Frequency (FF) ranging from 0 to 0.5, where the high end of this  
456 range corresponds with half the sampling frequency as per the Nyquist sampling theorem. The vertical  
457 range of the spectrogram plot is set to a maximum of  $\text{FF} = 0.04$  for visualization and because most of the  
458 Power Spectral Density (PSD) of the signal occurs at a lower frequency than this maximum. Since the  
459 sampling interval for field deployment was 30 minutes as 1800 s, the sampling frequency was  
460  $\sim 5.56 \times 10^{-4}$  Hz.

461 The turbidity and TDS time series show diurnal cycles associated with water circulation and  
462 mixing in the reservoir that also includes the addition of water from storm sewer systems. The  
463 spectrogram corresponding to the turbidity time series (Figure 6b) shows the gradual development of  
464 cyclical processes over the time of observation, whereas the spectrogram corresponding to the TDS time  
465 series (Figure 6d) shows a reduction in cyclical processes.

466 An increase in the turbidity and an increase in the TDS occurred concomitant with precipitation  
467 events (Figure 6e) near the midpoint of the time series observations. After these precipitation events  
468 occur, the turbidity exhibits an increase in cyclical processes, whereas the TDS exhibits fewer cyclical  
469 processes. The increase in turbidity and associated cyclical processes in relation to the rainfall event may

470 have been caused by an increase in water flow to the reservoir and an increase in sediment conveyed to  
471 the reservoir by runoff events. Alternately, an increase in TDS and a decrease in associated cyclical  
472 processes may indicate an increase in the mixing of water in the reservoir after the addition of runoff  
473 from the precipitation events. As expected, water temperature (Figure 6e) exhibits diurnal cycles  
474 associated with land surface temperature changes and heating by solar radiation.

475 The turbidity spectrogram exhibits a dominant cyclical process at  $FF \approx 0.004$  corresponding to  
476 125 hr or 5.2 days. This indicates a temporal change in reservoir turbidity associated with sediment  
477 transport from rainfall events. Alternately, the TDS spectrogram exhibits a dominant cyclical process at  
478  $FF \approx 0.02$  corresponding to 25 hours, indicating that the TDS has more temporal variability than the  
479 turbidity and suggesting the prevalence of diurnal mixing processes in the reservoir.

480 The battery voltage over the time of field deployment (Figure 6f) ranged between 8.33 V and  
481 5.92 V without any missing data indicating that the system was powered by the battery and solar panels  
482 over the time of deployment. Figure 6f also shows discrete battery charging events, demonstrating the  
483 operation of the battery charger connected to the solar panels. Battery charging events only occurred  
484 when solar power was sufficiently high to provide the required current for charging. The average  
485 operating current sourced from the battery over the time of deployment was 64.6 mA, with an increase  
486 in current consumption during cellular transmission events, during cloudy days, and at night when  
487 current could not be sourced from the solar panels. The average operating current could be reduced  
488 using a custom microcontroller in lieu of the Arduino module. This is because the Arduino module and  
489 associated electronics has LEDs and the use of lower-efficiency circuit elements that are always powered  
490 over the time of deployment.

491 Figure 7 shows semivariograms computed for the turbidity (a), TDS (b) and (c) water  
492 temperature time series. A temporal semivariogram  $\gamma$  indicates autocorrelation over successive time  
493 intervals (Haslett 1997). The range is the position on the horizontal plot axis where the semivariogram  
494 reaches an approximate plateau referred to as the sill (Goovaerts 1997, p. 89). For the turbidity time  
495 series, the range is 9100 min as 6.3 days, whereas for the TDS time series, the turbidity is 8000 min as  
496 5.6 days. The temperature semivariogram exhibits a range of 9200 min as 6.4 days with some diurnal  
497 cycles evident at shorter time scales. Since the turbidity, TDS, and temperature time series become less  
498 autocorrelated at a time interval of  $\sim 6$  days, this indicates that manual sampling of water quality data in  
499 the reservoir should be conducted at weekly intervals to capture longer-term trends in temporal  
500 variability aside from diurnal variability. However, automated measurements are still required to  
501 characterize shorter-term biogeochemical cycles. As suggested by cycles in the TDS semivariogram  
502 exhibited at time intervals less than the range (Figure 7b), automated sampling is thereby more  
503 important to characterize TDS at shorter time scales than turbidity (Figure 7a). Turbidity (Figure 7a) and  
504 temperature (Figure 7c) time series have a similar range.

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## 507 **Conclusions**

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509 This paper introduced a platform for measurement of water quality with extensible hardware  
510 and software. The platform includes sensors that are often used to measure water quality. The  
511 mechanical, electrical and software designs are released under permissive open-source licenses to  
512 encourage collaboration and reduce the time required to implement a functioning system.

513 The mechanical design, electronics and software were described for educational purposes. The  
514 mechanical design allows for expeditious creation of parts on a 3D printer, enabling parts to be modified  
515 as required. For manufacturing of multiple sensor platforms to provide spatial coverage of a city or  
516 region, the parts could be created using injection molding. Although the initial setup costs of injection

517 molding can be high, the cost per part during production is sufficiently low to allow for the creation of a  
518 network of multiple WaterWatcher systems.

519 The electrical design allows for sensors to be sampled and a complete IoT system to be  
520 constructed around a microcontroller platform associated with the Arduino ecosystem. This reduces the  
521 complexity of updating and editing the code for other associated applications. Moreover, since the basic  
522 system functionality can be setup using the CLI, this allows for system operation to be modified and  
523 calibration coefficients programmed as human-readable transfer functions without the need for  
524 additional computer code to be written. Since the CLI is associated with a virtual serial port, the  
525 possibility exists of a computer program with a Graphical User Interface (GUI) and associated hardware  
526 being used to automatically set up and calibrate the system after construction. This can allow for  
527 multiple sensors to be assembled and quickly tested before deployment.

528 The WaterWatcher system was calibrated in a lab tank. The calibration process demonstrates  
529 the sensor operation and indicates how the system can be calibrated to relate voltages to physical  
530 quantities. Despite the low 12-bit resolution of the microcontroller ADC, the WaterWatcher platform  
531 can provide estimates of turbidity and TDS that coincide with commercial sensors. The circuit board  
532 could be updated in the future with the addition of a higher-resolution ADC and additional sensors that  
533 measure water chemistry for additional assessment of pollution and hazards.

534 The field deployment of the WaterWater demonstrated how the system can be used to collect  
535 data at a field location and characterized circuit operation. The time series data was subjected to  
536 spectrogram and semivariogram analyses to indicate biogeochemical cycles occurring in the North Swale  
537 reservoir.

538 Multiple WaterWatcher platforms have the potential to create a low-cost network of sensors  
539 that report data useful for predictions and forecasts of water quality. The use of open-source hardware  
540 and software reduces cost and allows for systems to be easily extended for civil engineering and  
541 toxicology applications.

542

543

## 544 **Declarations**

545

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547

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553

### 554 *Conflicts of interest/competing interests*

555

556 The authors declare no conflicts of interest and no competing interests.

557

### 558 *Availability of data and material*

559

560 Datasets (<https://doi.org/10.6084/m9.figshare.14439503.v1>) as well as images showing the assembly of  
561 the WaterWatcher and video of the wave testing experiment

562 (<https://doi.org/10.6084/m9.figshare.14428709.v1>) are provided as Figshare downloads and licensed  
563 using a permissive license (<https://creativecommons.org/licenses/by-sa/4.0/>). The hardware as

564 designed by the authors is licensed using the CERN open hardware license (CERN-OHL,  
565 <https://www.ohwr.org/cernohl>)

566  
567

568 *Code availability*

569

570 All data, design files and programs used for this study can be downloaded from Figshare  
571 (<https://doi.org/10.6084/m9.figshare.14444672.v1>) and Github  
572 (<https://github.com/nkinar/WaterWatcher>). The software is licensed using the GNU GPL v3  
573 (<https://www.gnu.org/licenses/gpl-3.0.en.html>).

574  
575

576 *Authors' contributions*

577

578 Both authors (N.K. and M.B.) contributed equally to this paper.

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580

581 *Ethics approval*

582

583 Ethics approval is not applicable for this study.

584  
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586 *Consent to participate*

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588 Consent to participate is not applicable for this study.

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591 *Consent for publication*

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593 Both authors consented to the publication of this manuscript.

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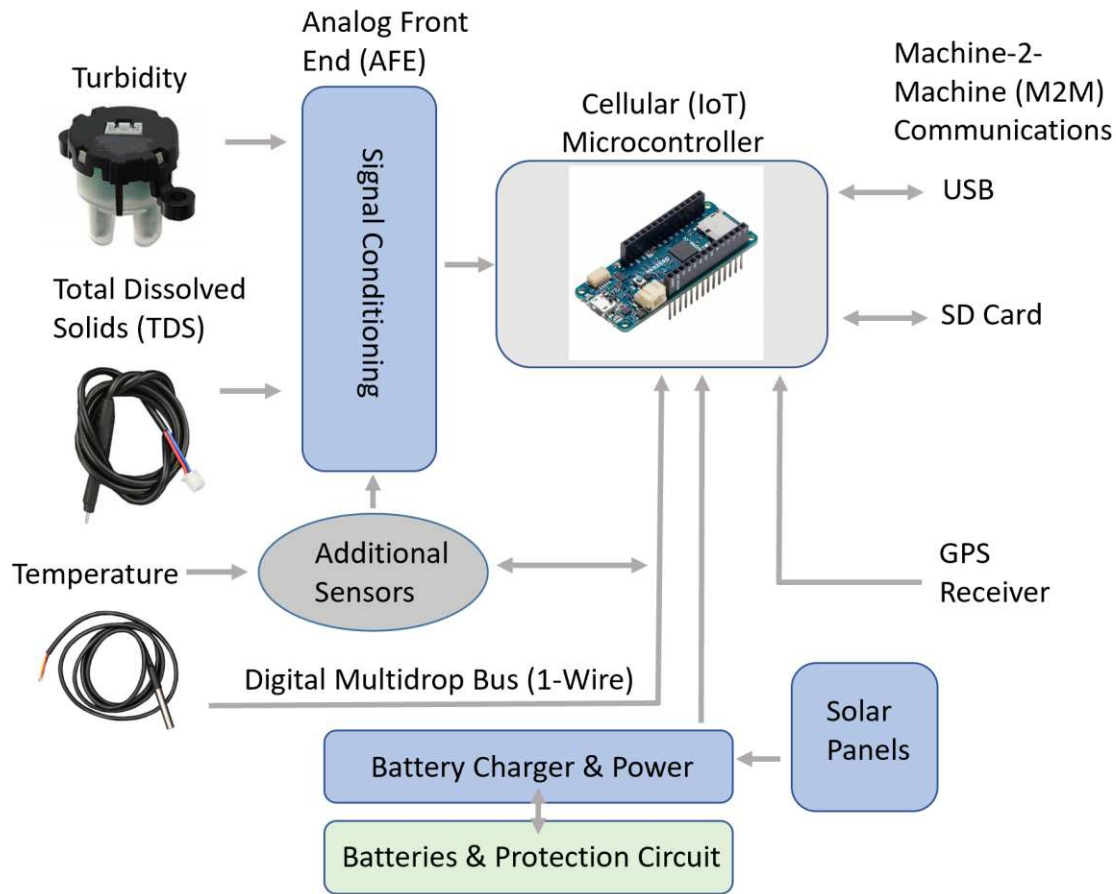
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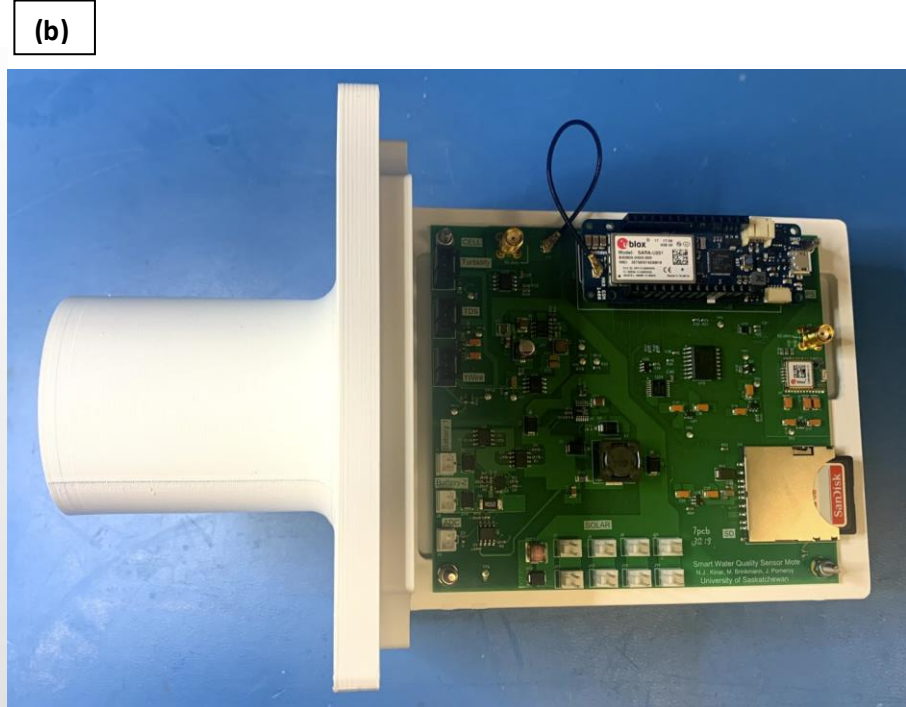
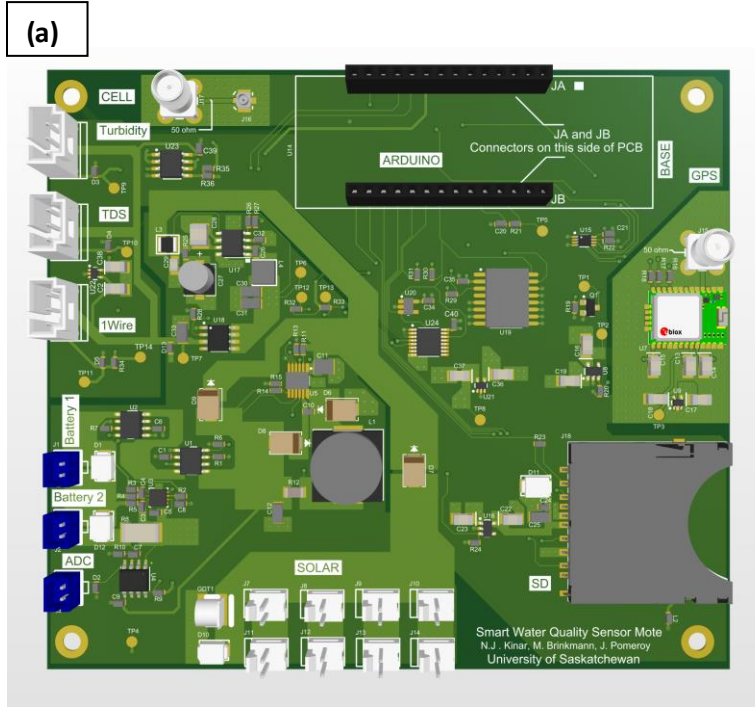
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834  
835 **Appendices**  
836  
837 Appendix A and B are provided as PDF files as Supplementary Information (SI).

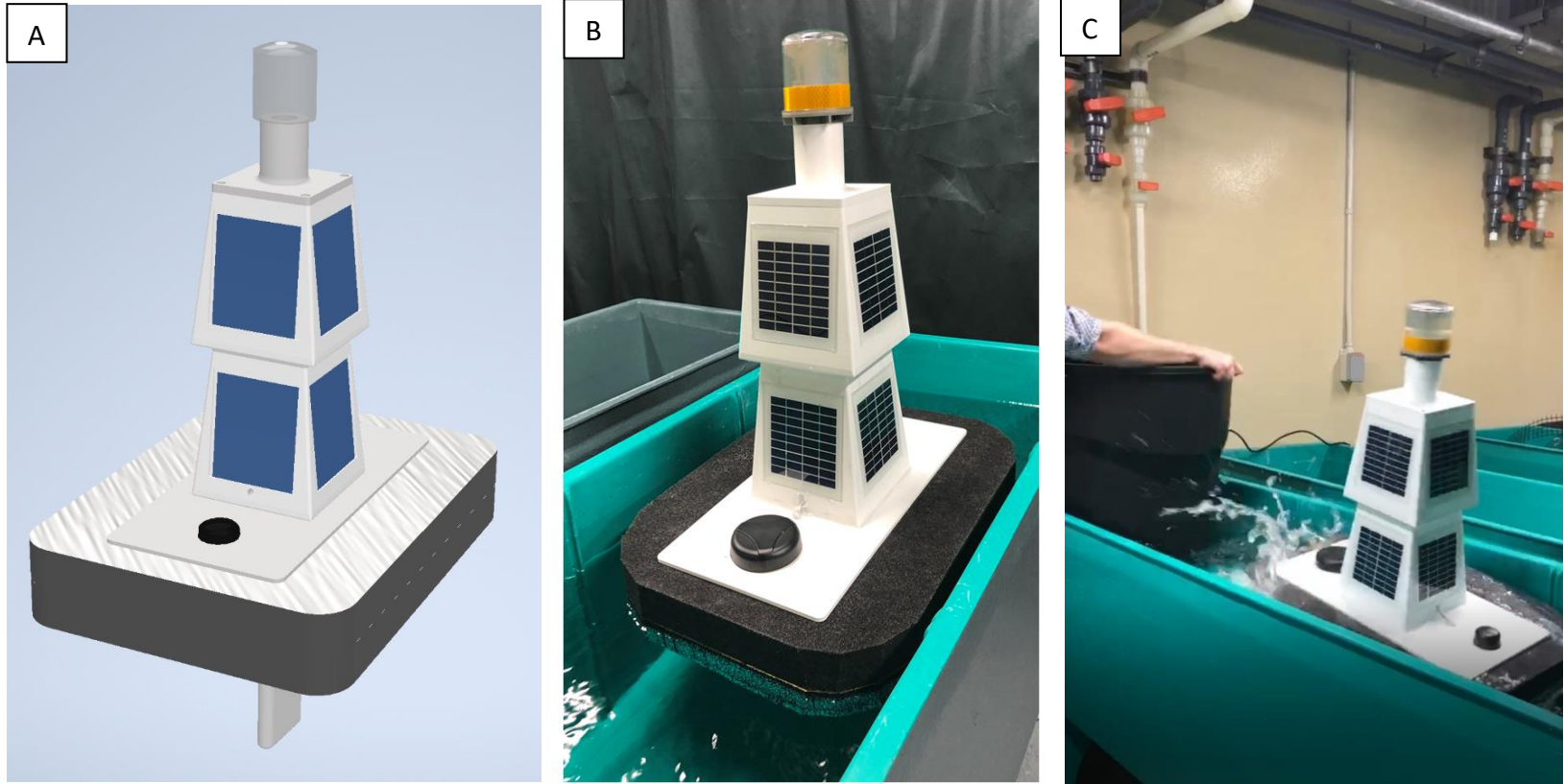




**Figure 1.** Block diagram of WaterWatcher system showing sub-systems. Photographs courtesy Digikey Incorporated (Thief River Falls, Minnesota, USA) and are used with permission.



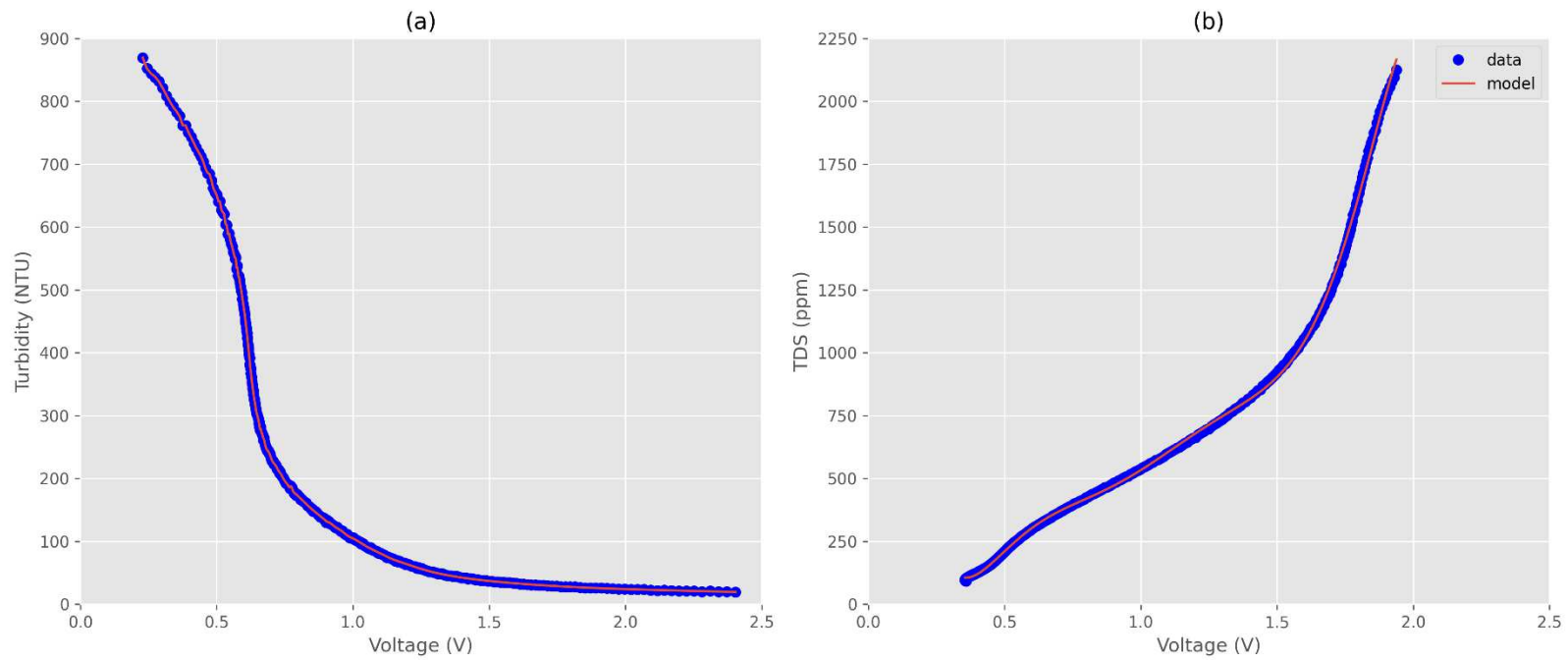
**Figure 2.** (a) 3D rendering of the electronic printed circuit board (PCB) for the WaterWatcher system. System components are labeled on the PCB. (b) Picture of constructed PCB mounted with mechanical fasteners on a 3D printed plastic part.



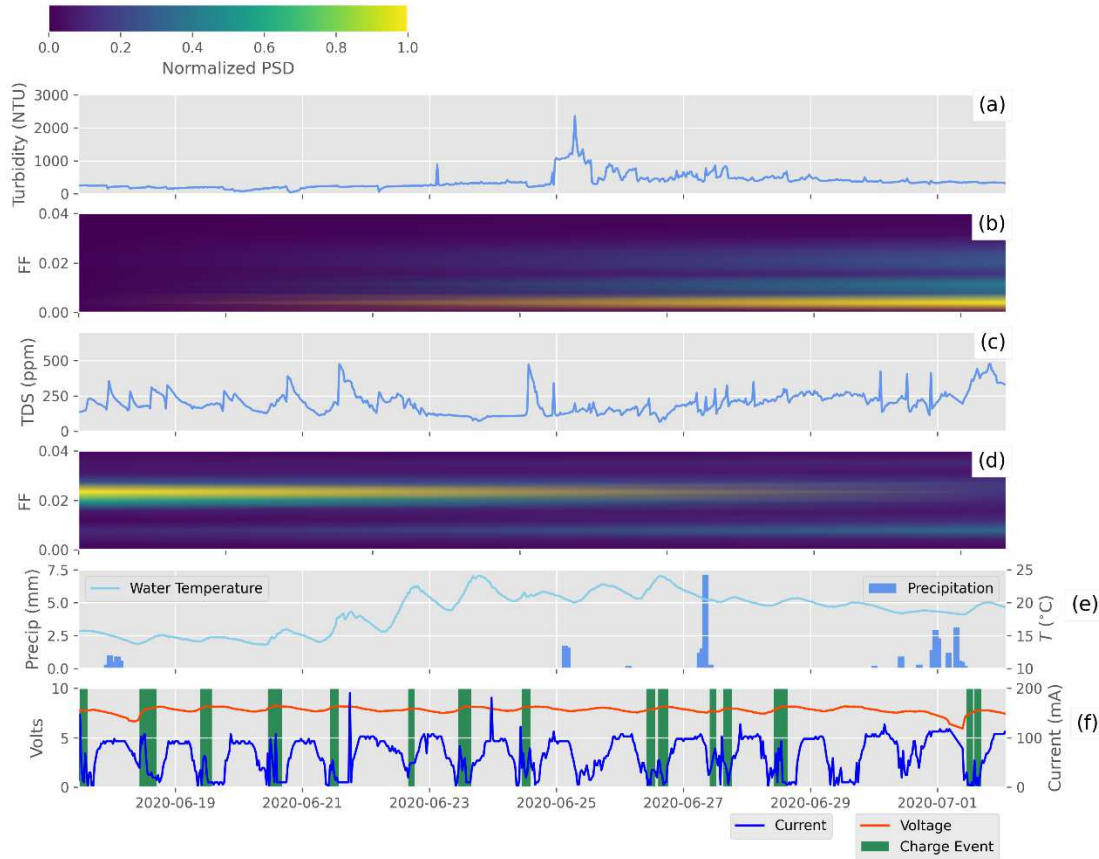
**Figure 3.** (a) CAD software rendering of mechanical WaterWatcher enclosure. The 3D model includes all mechanical parts that comprise the system. (b) Actual photograph of the WaterWatcher system tested in a tank. (c) Photograph of tank test to check for buoyancy and stability.



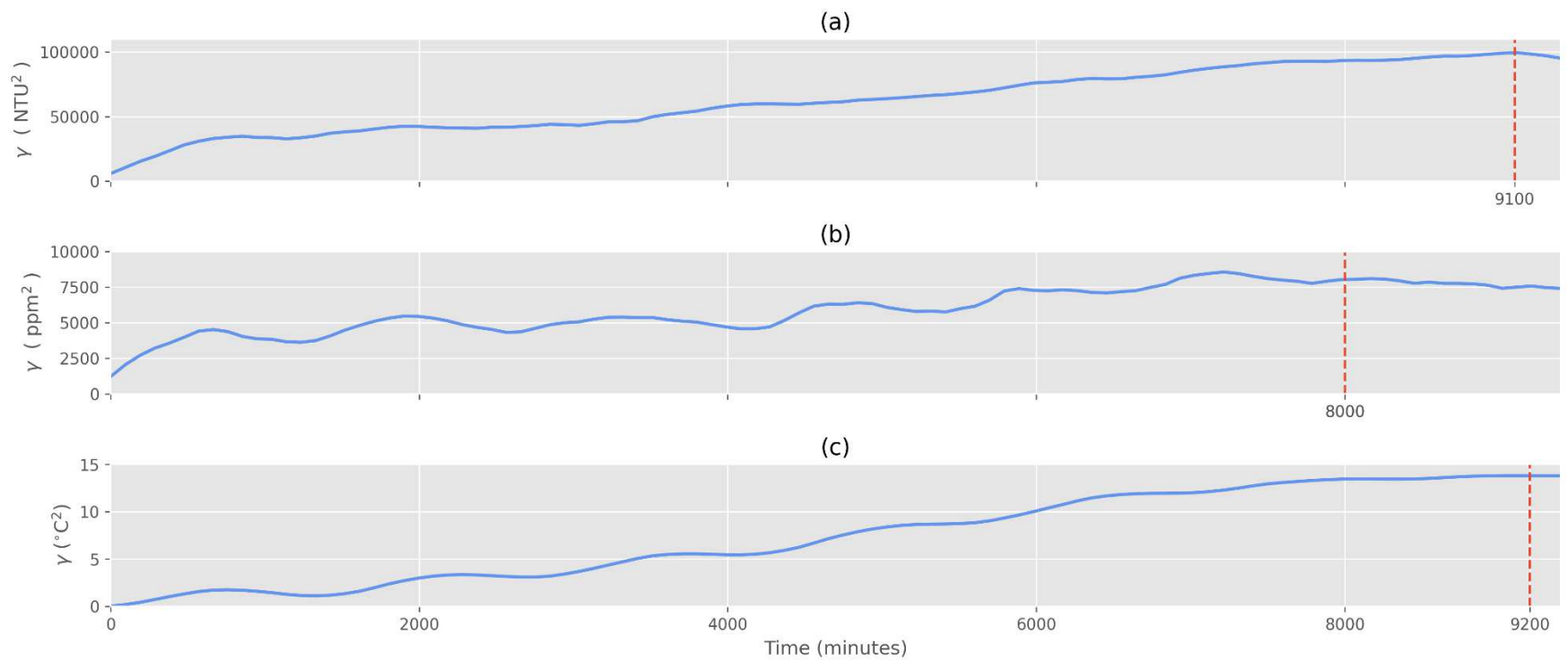
**Figure 4.** Deployment of WaterWatcher at an urban reservoir (Aspen Ridge Forebay, City of Saskatoon, Saskatoon, Saskatchewan, Canada).



**Figure 5.** Calibration experiments to relate sensor output voltages to (a) turbidity and (b) TDS. The data are shown as circle markers, whereas the model is shown as a line on each plot.



**Figure 6.** Field data collected at the Aspen Ridge Forebay location. (a) Turbidity time series; (b) spectrogram of turbidity time series with fractional frequency (FF); (c) TDS time series; (d) spectrogram of TDS time series with fractional frequency (FF); (e) precipitation events as measured at Saskatoon by Environment and Climate Change Canada along with reservoir water temperature  $T$  ( $^{\circ}\text{C}$ ); (f) time series of battery voltage showing discrete battery charging events associated with operation of the solar panel battery charger and battery current consumption. As shown by the colorbar at the top of the figure, the spectrogram Power Spectral Density (PSD) has been normalized with respect to the maximum power of the time series signals associated with spectrograms (b) and (d).



**Figure 7.** Semivariance  $\gamma$  of (a) turbidity, (b) TDS and (c) water temperature time series. The range is marked on the x-axis as a vertical dashed line to indicate temporal autocorrelation at time intervals less than the range.

**Table 1.** Arduino setup code for WaterWatcher platform showing how system functionality is encapsulated by a WaterWatcher object. Some other functionality is provided by the CLI (Table 2), thereby reducing the amount of code required to be written by the user. The *Arduino.h* header file is only to be included when using an alternate IDE such as provided by Platform.io and is not required for the official Arduino IDE.

```
1. #include <Arduino.h>
2. #include <WaterWatcher.h>
3. #include "WaterWatcherOptions.h"
4.
5. class MyWaterWatcherOptions : public WaterWatcherOptions
6. {
7.     public:
8.
9.     MyWaterWatcherOptions()
10.    {
11.        sample_a0(true);        // sample a0
12.        sample_a1(true);        // sample a1
13.        sample_a2(false);       // do not sample a2
14.        sample_temp0(true);     // sample temp0
15.    } // end
16.
17.    //-----
18.    // TRANSFER FUNCTION OUTPUTS
19.    // EDIT THESE FUNCTIONS IF REQUIRED
20.    //-----
21.    float get_a0_out()
22.    {
23.        float out = get_a0_raw();
24.        return out;
25.    } // end
26.
27.    float get_a1_out()
28.    {
29.        float out = get_a1_raw();
30.        return out;
31.    } // end
32.
33.    float get_a2_out()
34.    {
35.        float out = get_a2_raw();
36.        return out;
37.    } // end
38.
39.    float get_temp0_out()
40.    {
41.        float out = get_temp0_raw();
42.        return out;
43.    } // end
44.
45. }; // end
46.
47. // Create an instance of the WaterWatcher object
48. WaterWatcher ww;
49.
50. // Create an instance of the options object
51. MyWaterWatcherOptions opt;
52.
53. // Required Arduino setup function
```



```

54. void setup()
55. {
56.   ww.setup(&opt);
57. } // end
58.
59. // Required Arduino main loop
60. void loop()
61. {
62.   ww.checkState();
63. } // end

```

**Table 2.** Commands for the Command Line Interface (CLI) listed along with examples. The CLI controls the state machine implemented in software and allows for system functionality to be set. Example functionality of commands are also given in the table. After the sampling rate is set, the write-flash command should be used to save the state into non-volatile memory. As demonstrated by the commands, the CLI allows for system functionality to be easily configured.

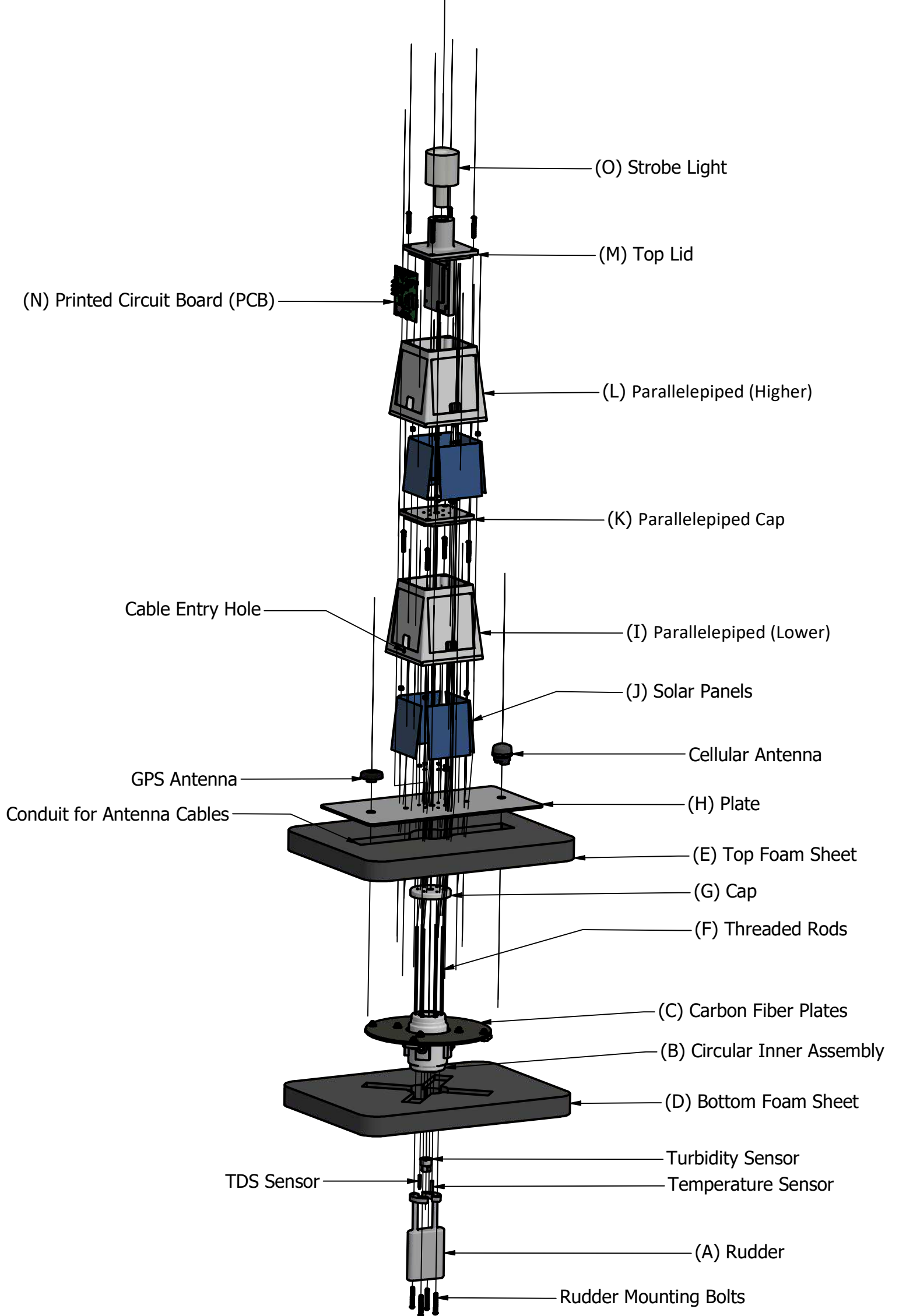
Software Commands	
on-5v	Turn on 5V power on circuit board
off-5v	Turn off 5V power on circuit board
print-serial	Print serial number
bstate	Print battery state
rtemp	RTC clock temperature
time	Print the current time
time dd/mm/yyyy hh:mm:ss	Set the current time (24 hour clock)
rtc-control	Read the status of the RTC control register
rtc-default	Set the RTC to defaults
sam [n]	Set alarm every n minutes (alarm is on after command)
oa	Turn off alarm
iao	Is alarm on?
print-coeff	Print flash coefficients
set-name [name]	Set the name of the device
write-flash	Write non-volatile vars into flash
read-flash	Read non-volatile vars
mem-defaults	Clear the memory to defaults
bmon-addr	Print the battery monitor addresses
print-bmon	Print the battery monitor information
reset	Reset the device (i.e. powercycle)
print-gps	Print the GPS coordinates
on-sd	Turn on the SD card
off-sd	Turn off the SD card
ls	List the contents of the SD card
cat [filename]	List the contents of a file on the SD card
rm [filename]	Remove a file from the card

echo [filename] [message]	Echo a message to file
key [number]	Set a key for communications with the server
cell [string]	Send a string over the cellular network to the server
on-cell	Turn on the cellular modem
off-cell	Turn off the cellular modem
powersave-on	Turn on powersave (i.e. shutdown modem and rails)
powersave-off	Turn off powersave
sendcell-on	Turn on sending of the cellular device
sendcell-off	Turn off sending of the cellular device
sample	Manually trigger a sample

**Table 3.** Calibration model accuracies for the WaterWatcher obtained from laboratory experimentation. The Root Mean Squared Difference (RMSD) is listed along with the Mean Bias (MB). The resolution is calculated as per the discussion in Section 3.1.

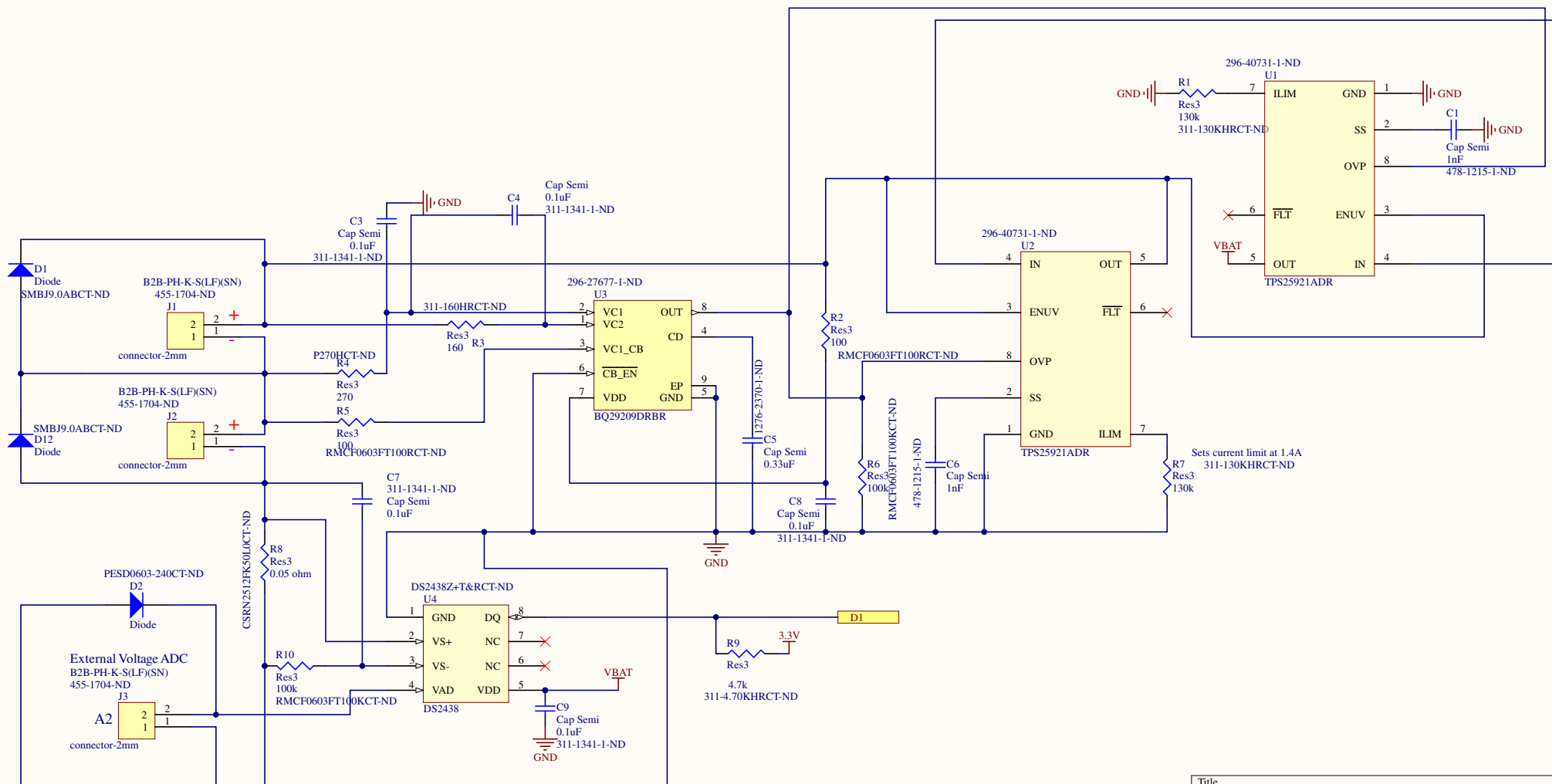
Measure	Turbidity (NTU)	TDS (ppm)
RMSD	1.0	11.38
MB	1.753e-13	-0.01348
Sensor Resolution	0.7454	1.007

## Appendix A

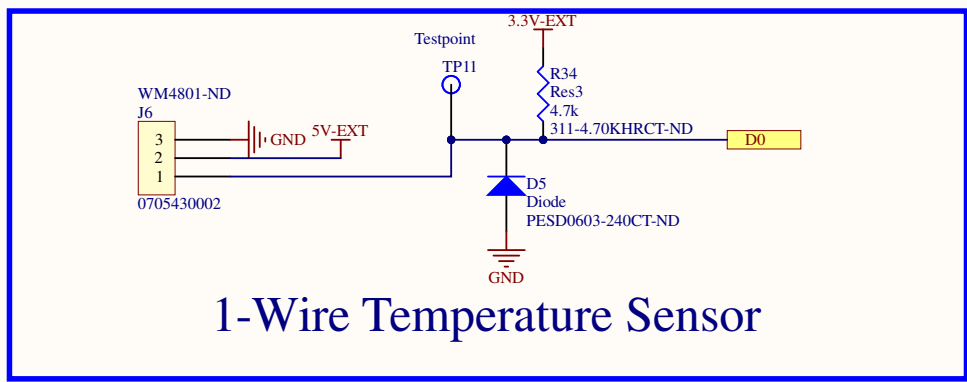
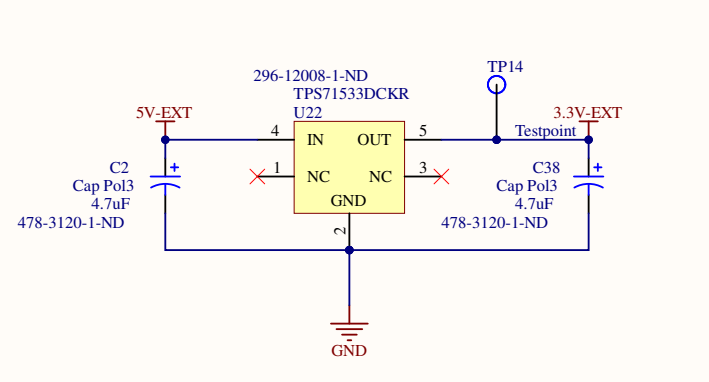
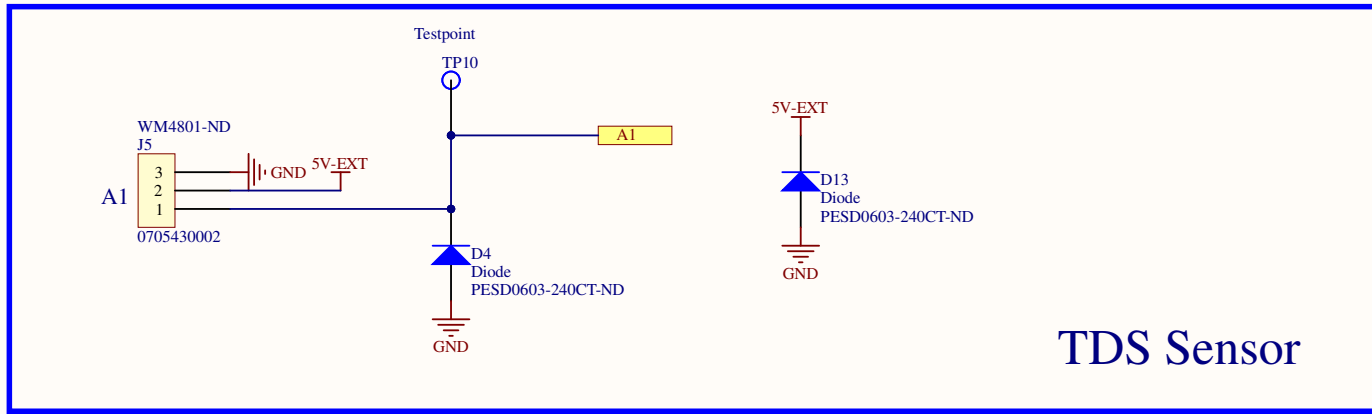
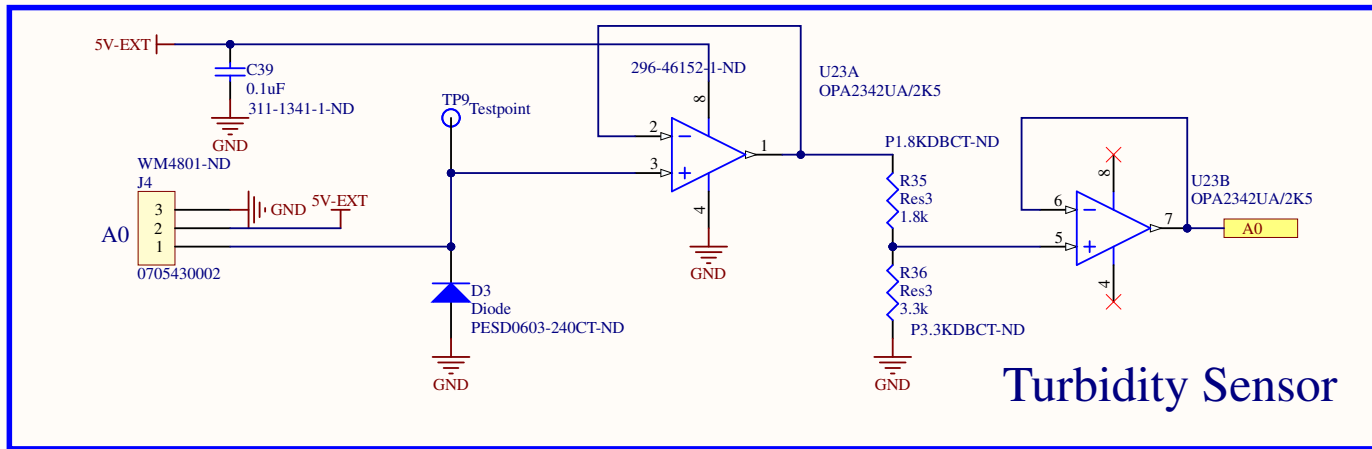


## Appendix B

# Battery Protector / Charge Balancing / Fuel Gauge

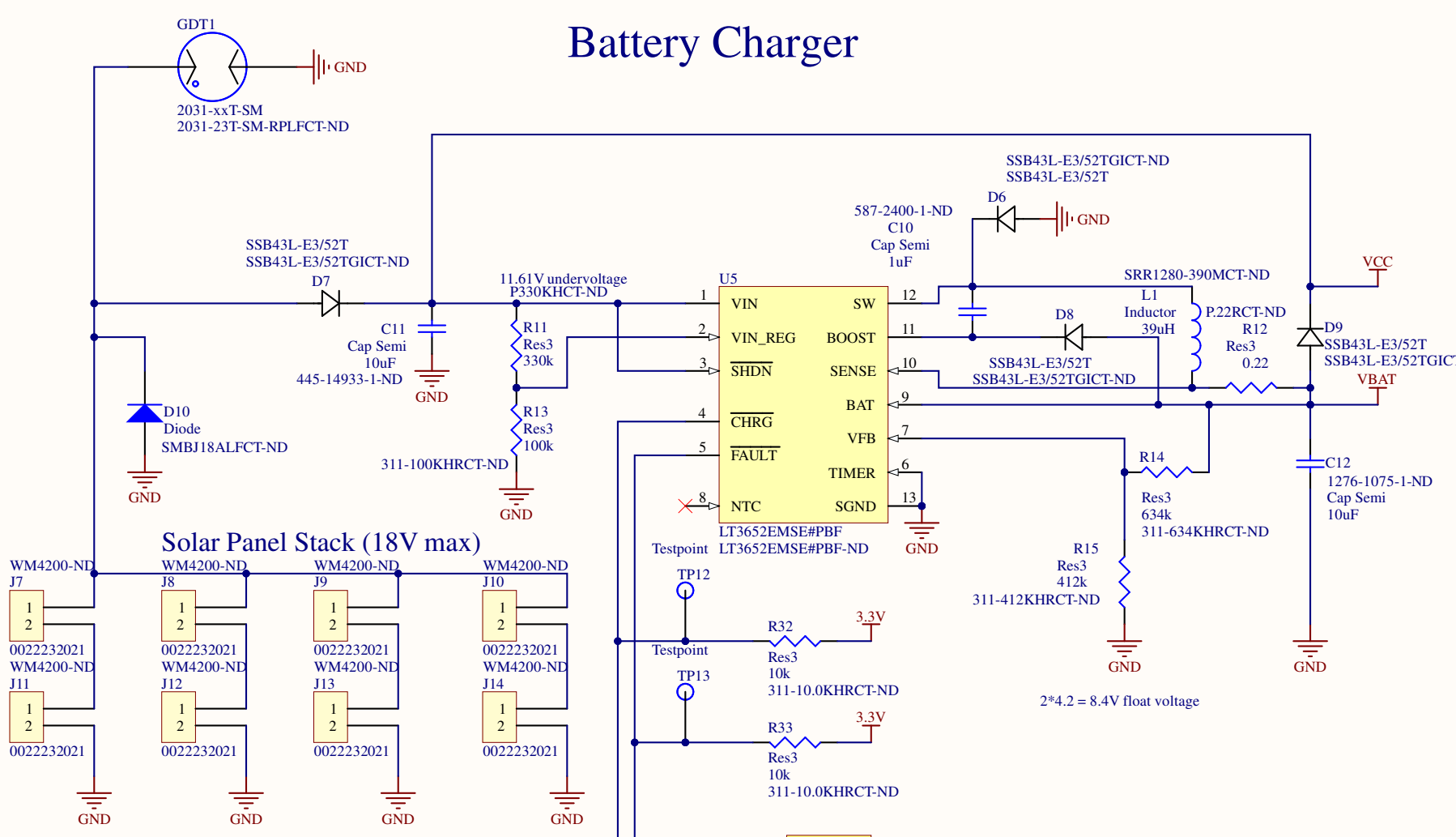


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# Battery Charger

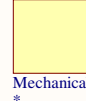


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Control impedance of antenna trace with width 0.75 mm. Control impedance to 50 ohms. Starting trace width at 0.75 mm and trace gap at 0.15 mm with surrounding GND plane. Adjust trace width and gap accordingly to attain specified impedance.

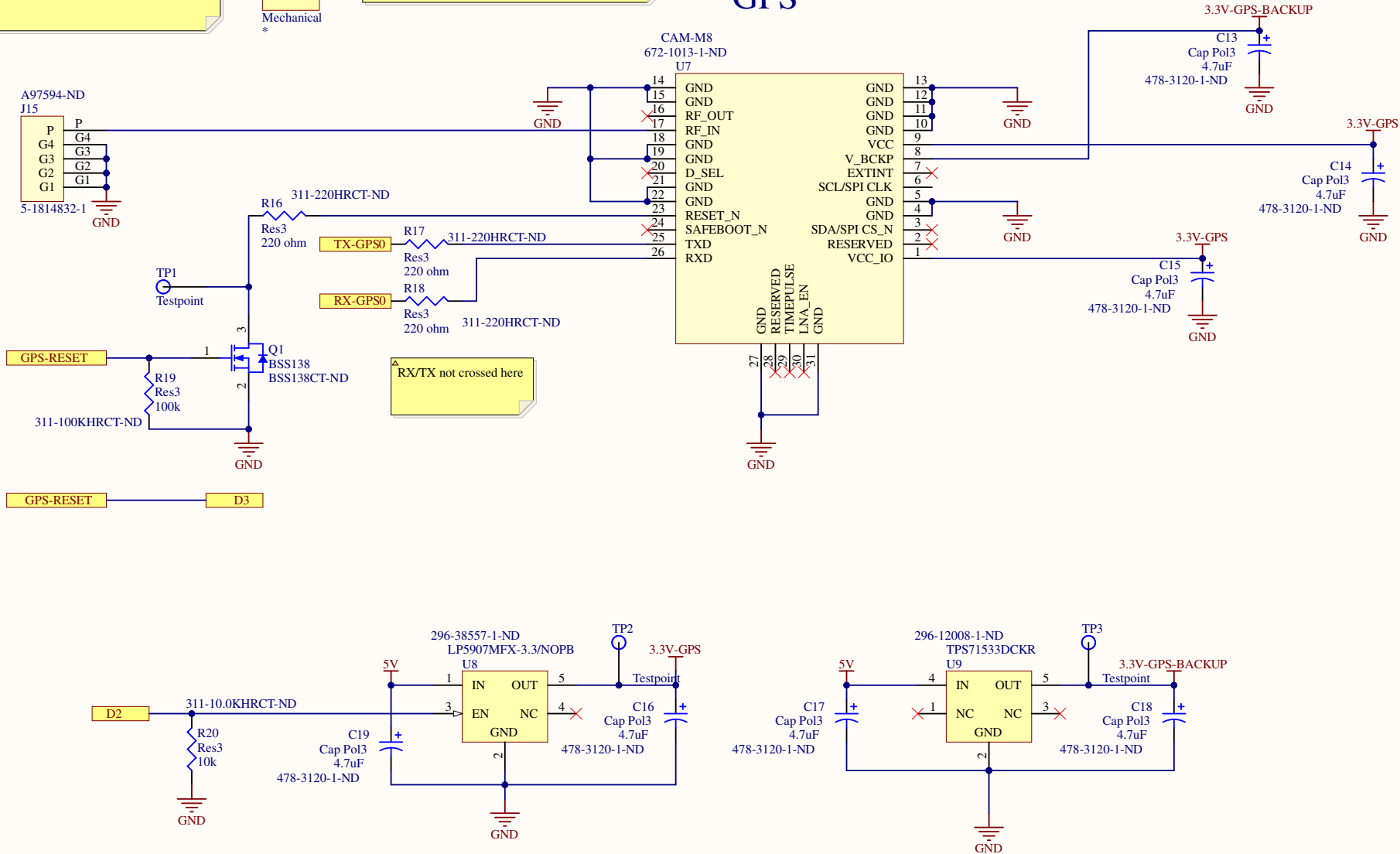
A.80.A.101111  
931-1528-ND  
U6



Mechanical  
\*

An external bias tee is required for the RF antenna to work. On an updated version of the PCB, the bias tee should be present on the PCB.

# GPS



RX/TX not crossed here

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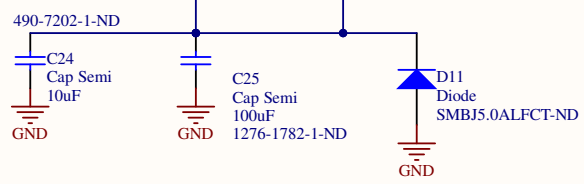
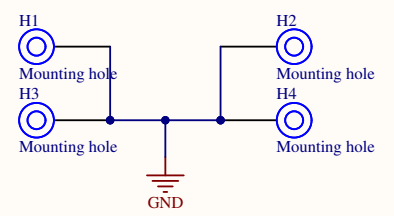
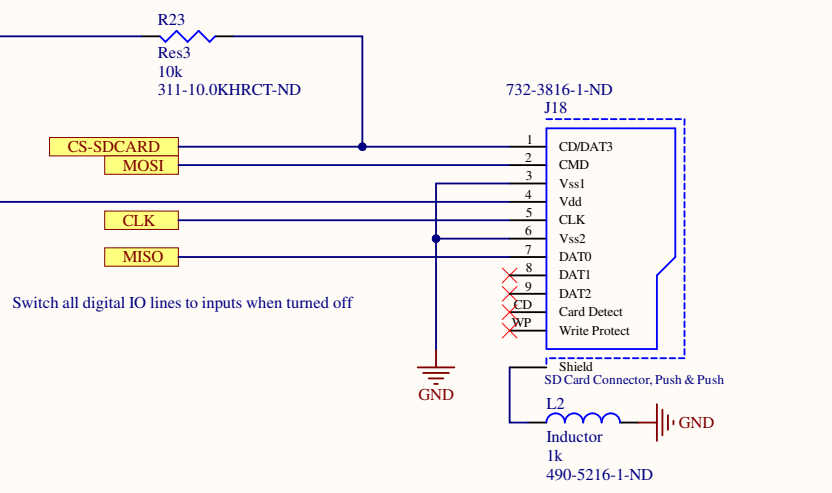
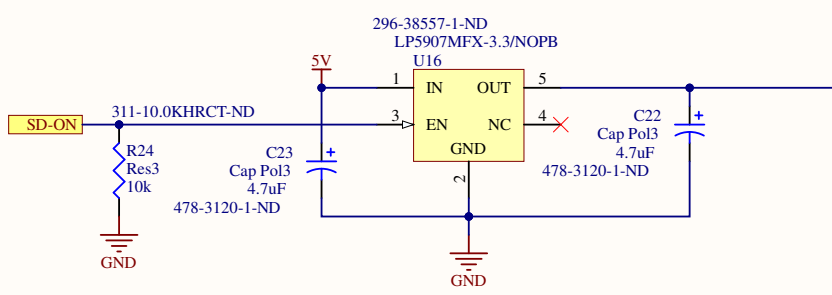
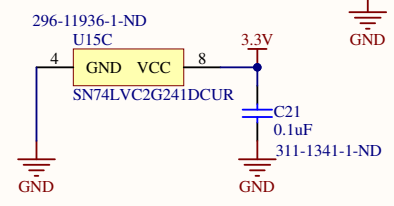
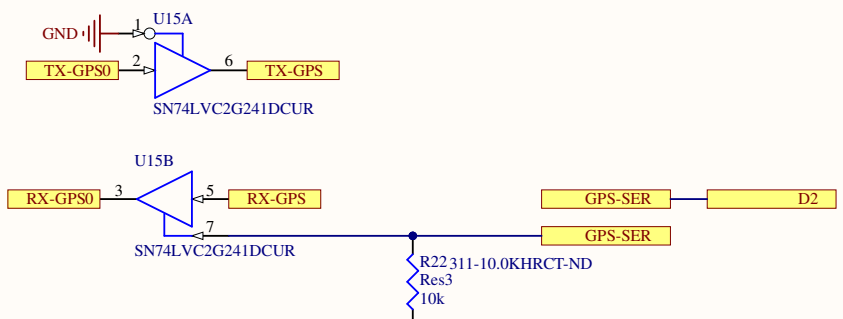
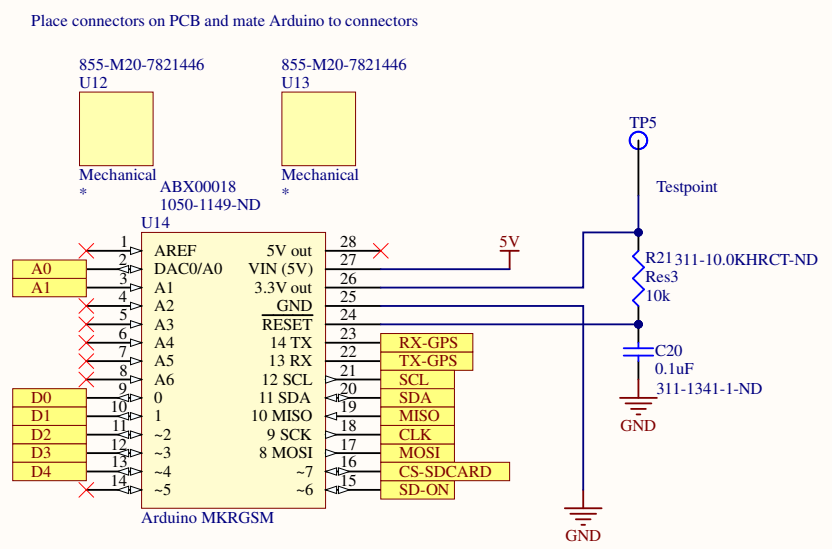
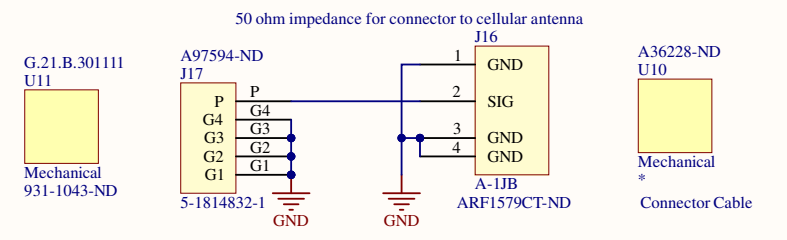
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C

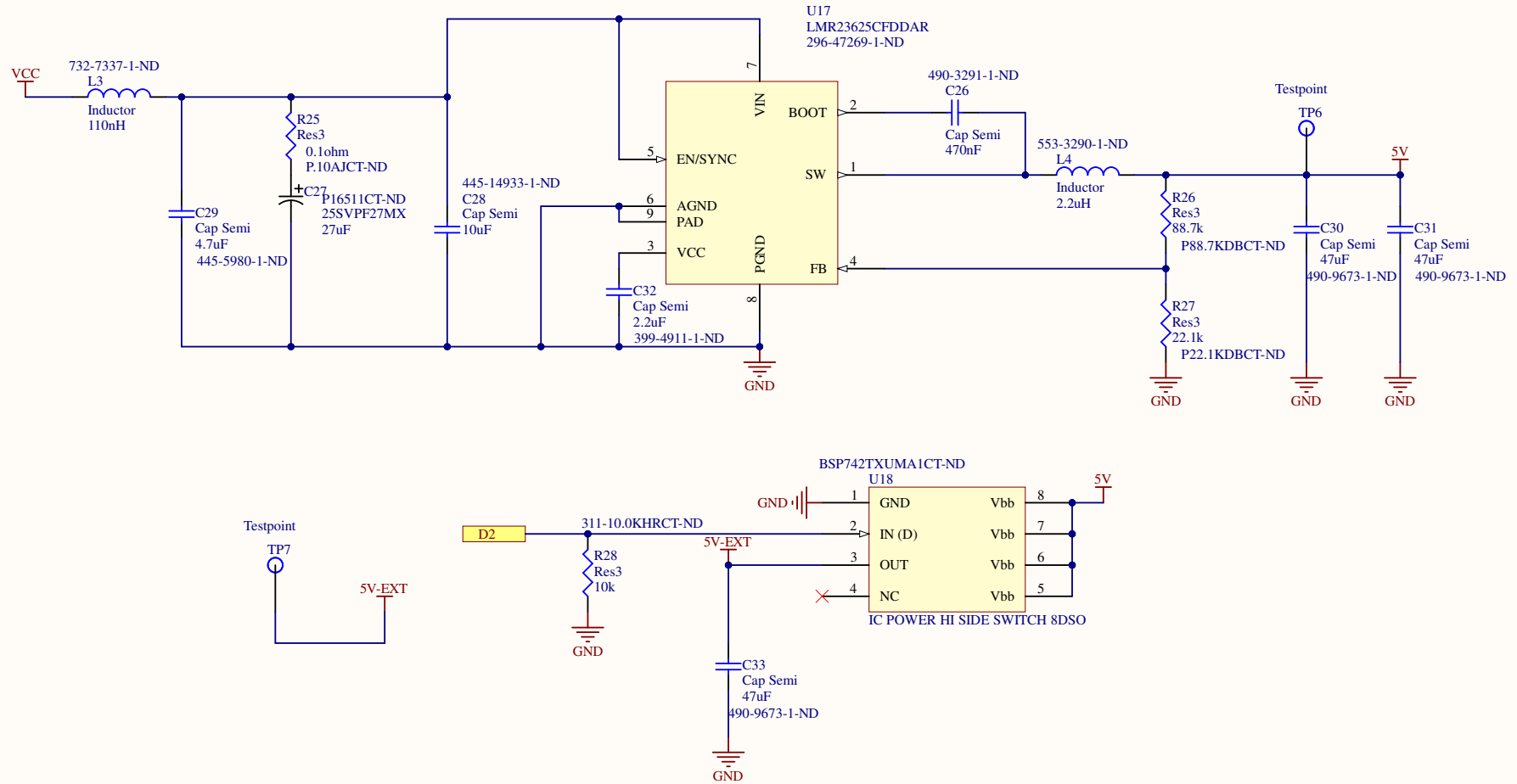
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D

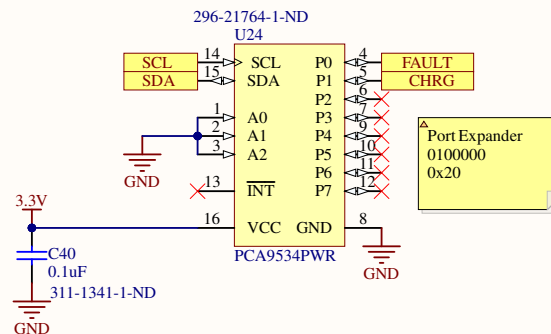
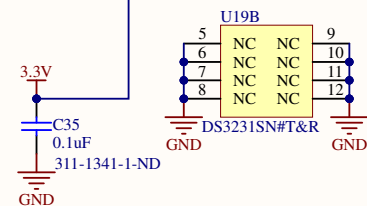
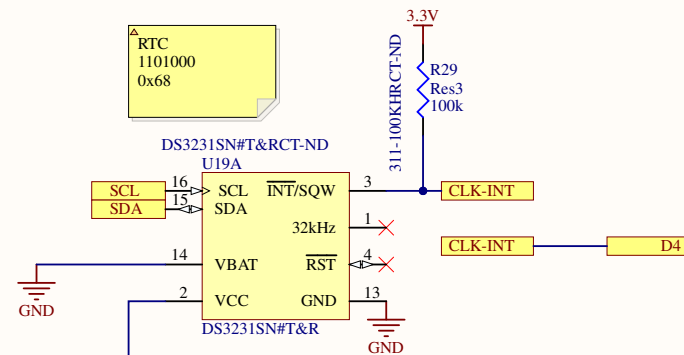
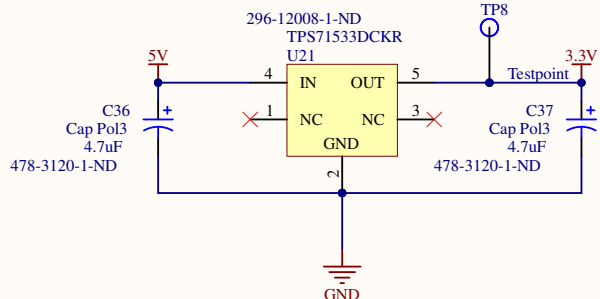
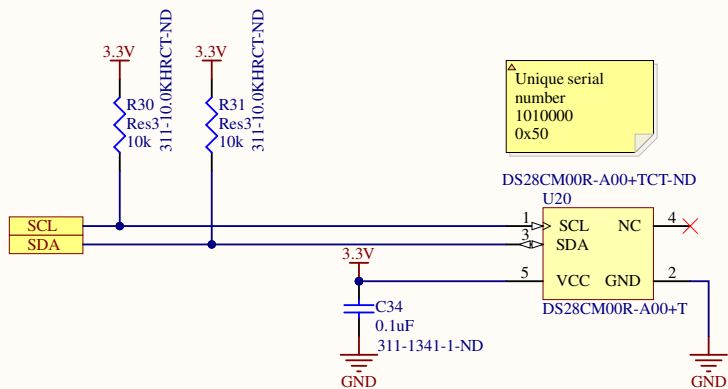


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# 5V Power Supply

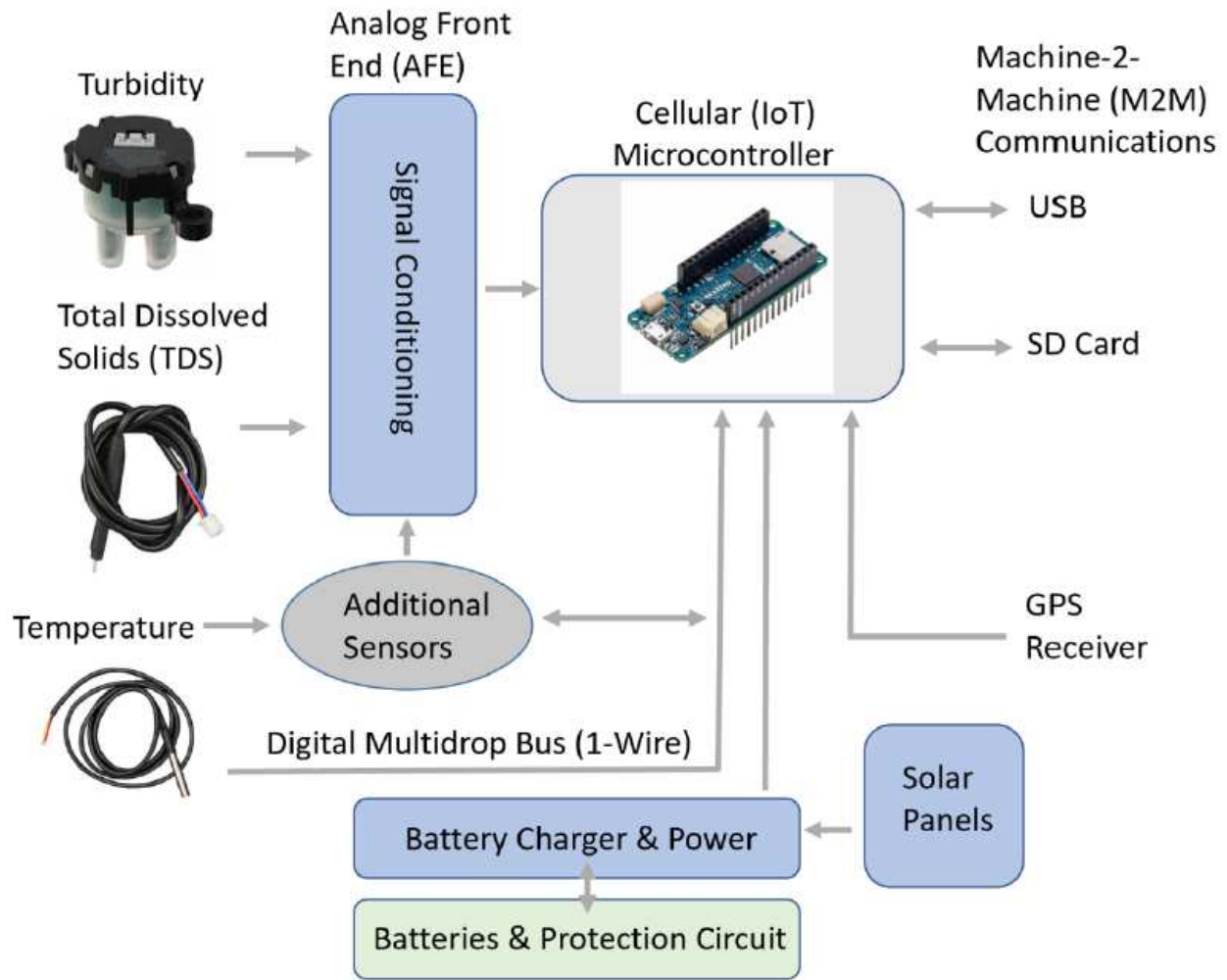


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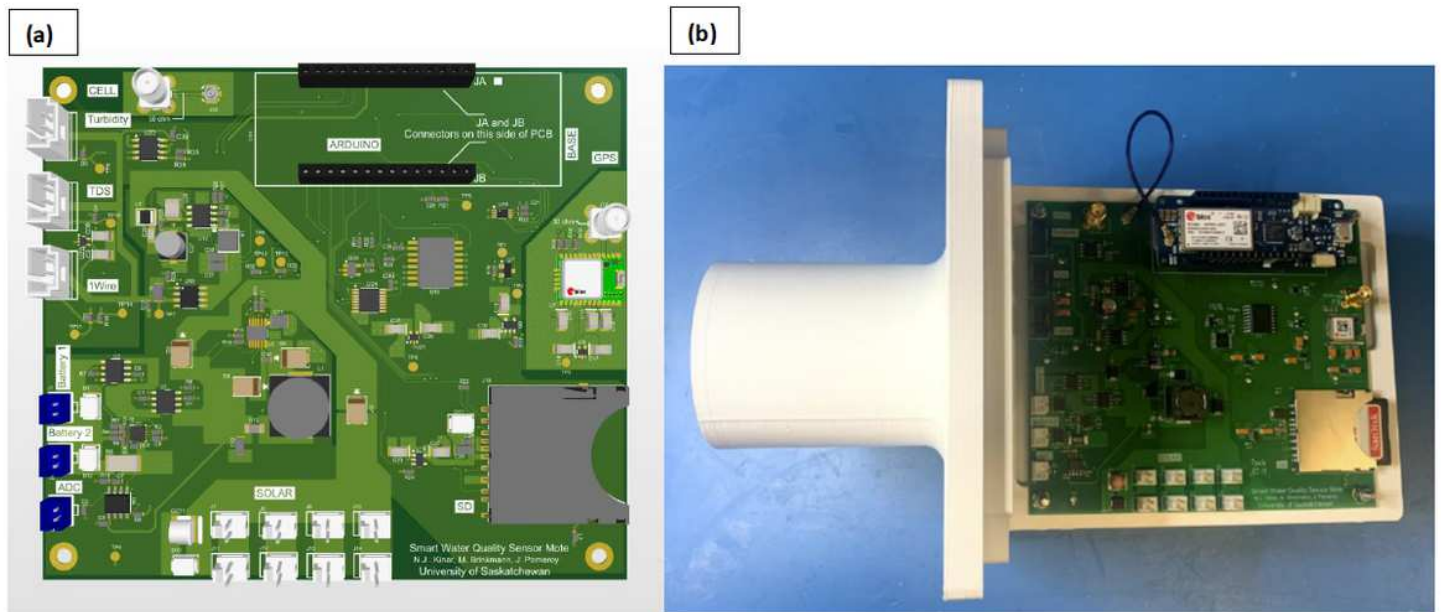
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# Figures



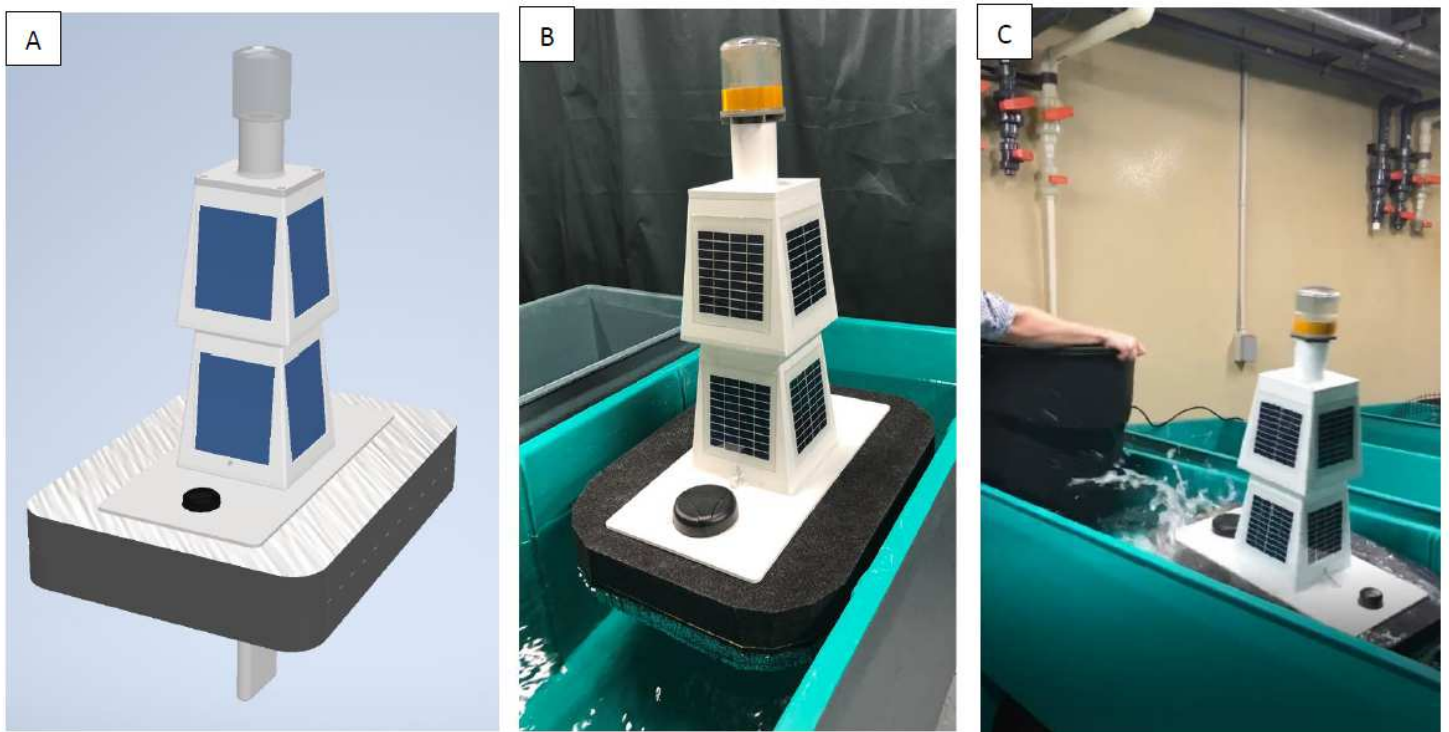
**Figure 1**

Block diagram of WaterWatcher system showing sub-systems. Photographs courtesy Digikey Incorporated (Thief River Falls, Minnesota, USA) and are used with permission.



**Figure 2**

(a) 3D rendering of the electronic printed circuit board (PCB) for the WaterWatcher system. System components are labeled on the PCB. (b) Picture of constructed PCB mounted with mechanical fasteners on a 3D printed plastic part.



**Figure 3**

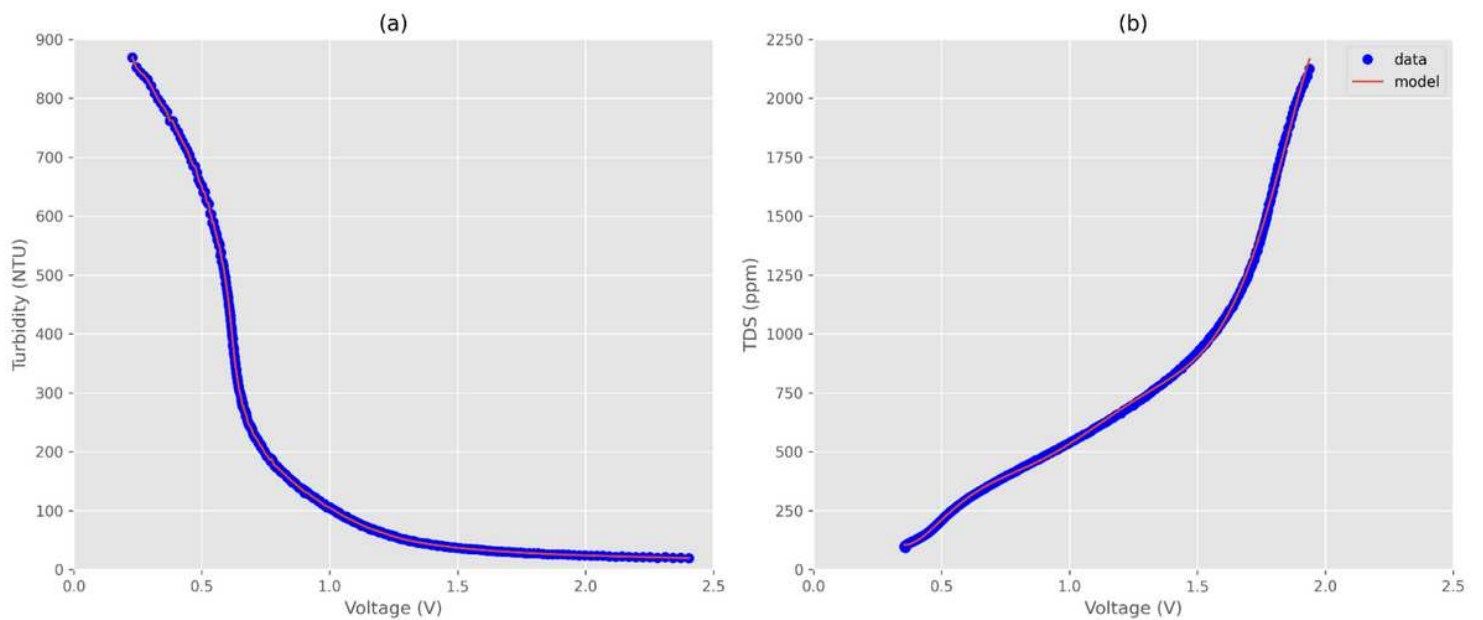
(a) CAD software rendering of mechanical WaterWatcher enclosure. The 3D model includes all mechanical parts that comprise the system. (b) Actual photograph of the WaterWatcher system tested in

a tank. (c) Photograph of tank test to check for buoyancy and stability.



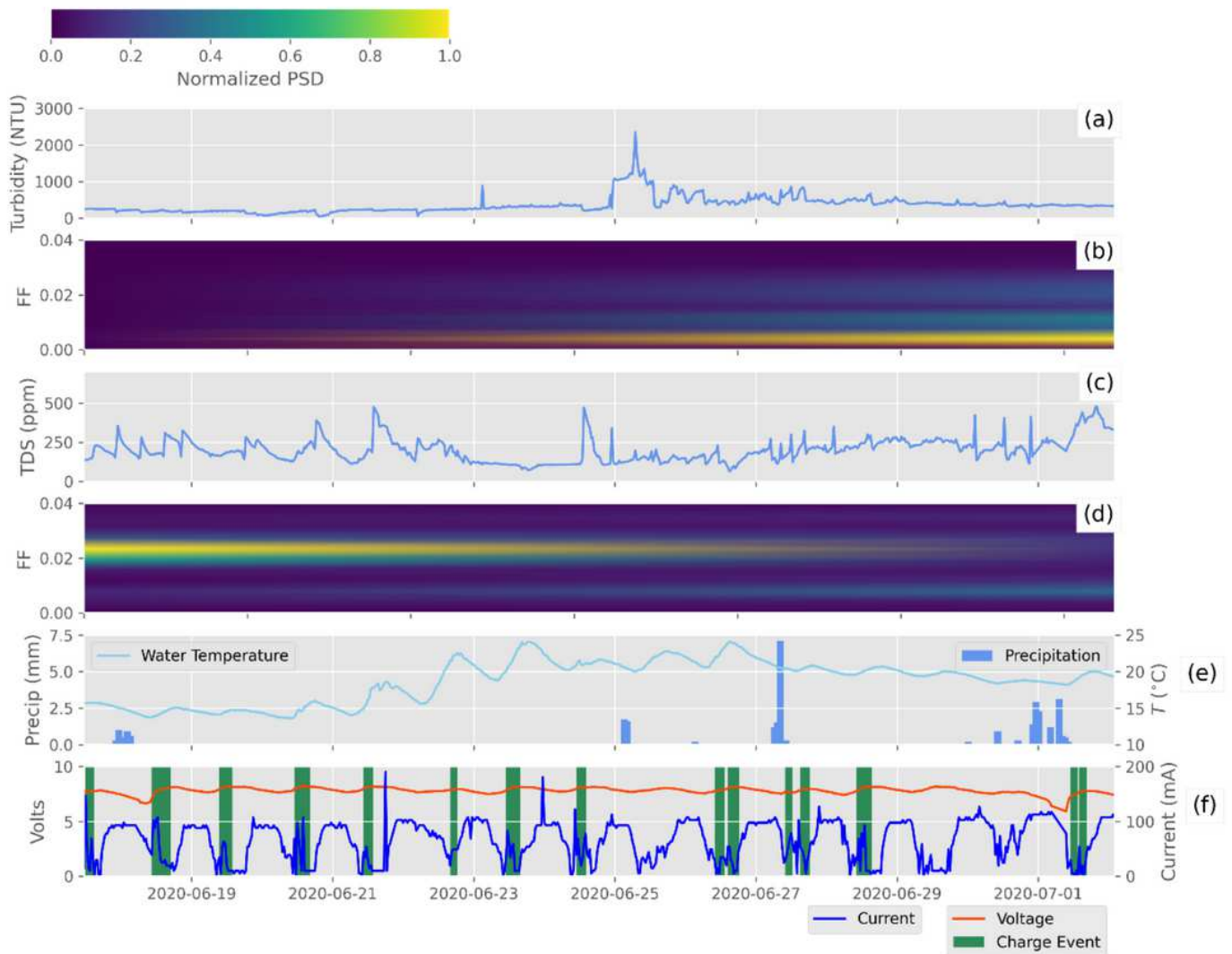
**Figure 4**

Deployment of WaterWatcher at an urban reservoir (Aspen Ridge Forebay, City of Saskatoon, Saskatoon, Saskatchewan, Canada).



**Figure 5**

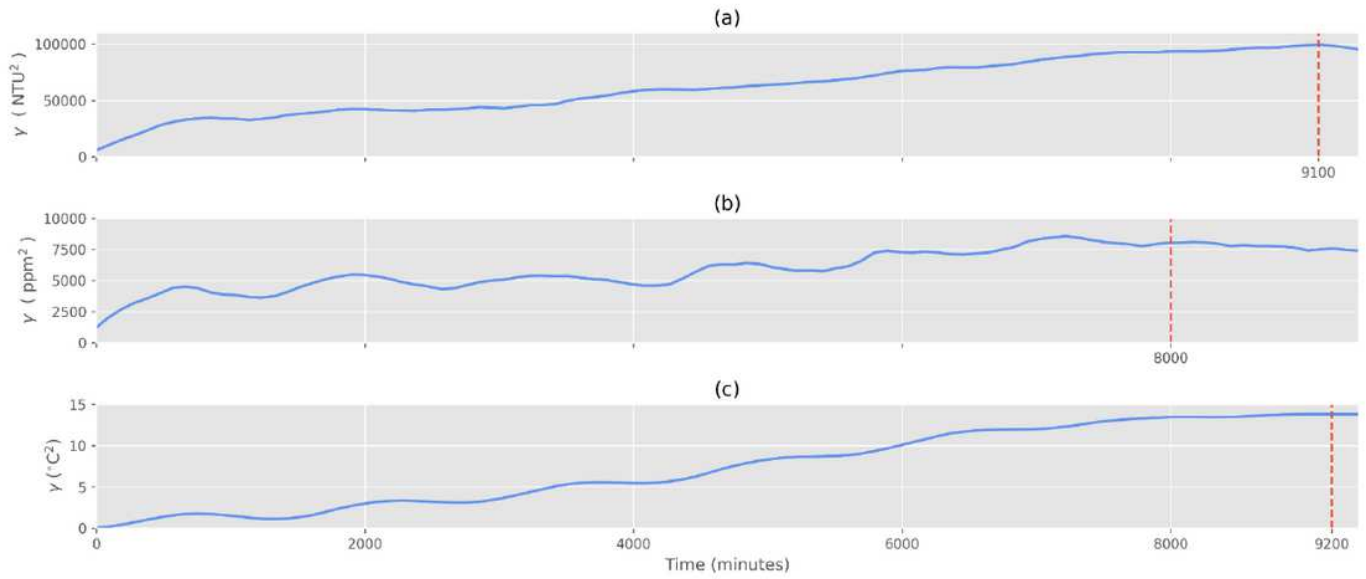
Calibration experiments to relate sensor output voltages to (a) turbidity and (b) TDS. The data are shown as circle markers, whereas the model is shown as a line on each plot.



**Figure 6**

Field data collected at the Aspen Ridge Forebay location. (a) Turbidity time series; (b) spectrogram of turbidity time series with fractional frequency (FF); (c) TDS time series; (d) spectrogram of TDS time series with fractional frequency (FF); (e) precipitation events as measured at Saskatoon by Environment and Climate Change Canada along with reservoir water temperature  $T$  ( $^{\circ}\text{C}$ ); (f) time series of battery voltage showing discrete battery charging events associated with operation of the solar panel battery charger and battery current consumption. As shown by the colorbar at the top of the figure, the spectrogram Power Spectral Density (PSD) has been normalized with respect to the maximum power of the time series signals associated with spectrograms (b) and (d).





**Figure 7**

Semivariance  $\gamma$  of (a) turbidity, (b) TDS and (c) water temperature time series. The range is marked on the x-axis as a vertical dashed line to indicate temporal autocorrelation at time intervals less than the range.