

Sustainable Eco-friendly Wire-cut Electrical Discharge Machining: Gas Emission Analysis

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Research Article

Keywords: Gas emission concentration, Material removal rate, relative Emission rate, WEDM, sustainable, near-dry

Posted Date: June 2nd, 2021

DOI: <https://doi.org/10.21203/rs.3.rs-502937/v1>

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1 Sustainable eco-friendly wire-cut electrical discharge machining: 2 Gas emission analysis

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7 Abstract

8 Wire-cut electrical discharge machining (WEDM) is the highly essential unconventional electro-
9 thermal machining process to cut the contour profile of hard materials in modern production
10 industries. The various environmental impacting wastes (by evaporating and reacting hydro-
11 carbon dielectric fluid) are produced during the WEDM process and these are harmful to the
12 machine operators. These wastes are minimized by a near-dry WEDM process wherein the
13 pressurized air mixed with a small amount of water is used as a dielectric substance. In this
14 research, influences, and contributions of machining parameters such as air pressure, mixing water
15 flow rate, spark current and pulse width on gas emission concentration (GEC), materials removal
16 rate (MRR), and relative emission rate (RER) of sustainable near-dry WEDM process have been
17 optimized by Taguchi analysis. RER is investigated to analyze the effects of machining factors on
18 gas emission and machining rate combinedly. It was revealed that the maximum air pressure and
19 flow rate of mixing water have significantly been promoting the sustainable near-dry WEDM
20 process.

21 Keywords: Gas emission concentration; Material removal rate; relative Emission rate; WEDM;
22 sustainable; near-dry.

23 1. Introduction

24 In the recent aerospace and automotive industries, wire-cut electrical discharge machining
25 (WEDM) is an imperative recent cutting process to cut contour, accurate, intricate, and irregular
26 profiles of thermal and electrical conducting sub-components. Furthermore, the best accuracy and
27 highest surface finish of WEDM components are appreciated (Das and Chakraborty 2020). The
28 gas emission from hydrocarbon fluid in the conventional EMD/WEDM process is unavoidable for
29 the expectation of the highest production rate. As per ISO14000 environmental act, the gas

30 emission and hazardous wastes emitted from such modern machining processes should be
31 minimized to save the ecological system. The causes and effects of EDM wastes were analyzed by
32 many EDM research experiments. The hydrocarbon and liquid dielectric fluids caused many
33 harmful contaminants are exposed in the operating environments (Tonshoff et al. (1996). Leao and
34 Pashby (2004)). Hence, the ecological impacts of EDM/ WEDM could be minimized by changing
35 cutting fluids and modifying machining factors. However, the machining performance has been
36 reduced while altering cutting fluid and operating procedures. It affects the production rate and
37 leads to economic losses. Hence, sustainable eco-friendly EDM/WEDM research activities should
38 be focused on improving machining performance and minimize pollutions. The sustainable
39 development researches activities in EDM/ WEDM processes have been explained as follows.

40 The toxicity and flammability of waste streams generated during EDM processes are analyzed
41 and compared. It was concluded that harmful waste produced could be varied by tool, work
42 material, and dielectric fluid (Yeo et al. 1998). After the days, many research activities were
43 promoted to control the waste stream of EDM. It was found that minimum hazardous material was
44 detected from resin dielectric and softer work materials in WEDM and emitting low-level
45 emissions. The energy consumption and waste impacts to the health of human operators, lands,
46 water, and air pollutions have been concentrated and hydro-carbon fluid was replaced by tap water
47 in EDM and WEDM processes(Boopathi and Sivakumar 2014; Tang and Du 2014). However, the
48 machining efficiency has been decreased while replacing such dielectric fluid. In this aspect,
49 ultrasonic, magnetic, and cryogenic assisted gas dielectric EDM processes improve the machining
50 performances(Zhang et al. 2005, 2006; Singh Grewal and Parkash Dhiman 2019;
51 Talebizadehsardari et al. 2020). Various groupings of work materials, tools, and dielectric fluid
52 are affecting the various elements in the gas emissions (Evertz et al. 2006). It was revealed that
53 the plasma zone temperature of EDM will generate the various toxic contaminants while using
54 different work materials(Tonshoff et al. 1996; Valaki et al. 2015).

55 The dielectric level, current, pulse time, and flushing pressure were taken as factors to control
56 the concentration of aerosol and optimum parameters setting had been predicted to optimize the
57 lowest aerosol exposure(Mathew et al. 2010). It was also found that the maximum current and
58 pulse time settings will increase toxic aerosol emission in the operating zone (Jose et al. 2010).
59 The water dielectric in EDM processes has been reducing the toxic gas emission as compared to

60 the existing process. Three sustainability indicators EDM have been identified as ecological
61 impact, operator's health, and working safety. It was analyzed and concluded that dry EDM is an
62 environment and operator-friendly sustainable process (Valaki et al. 2015). The sustainable EDM
63 process has been investigated using canola and sunflower Biodiesel to promote clean and emit
64 much less harmful emissions (Ng et al. 2017). Generally, the gas-assisted EDM was performed
65 with low performance with a good environmentally supported process. The reducing negative
66 impact of this process could be improved by replacing a minimal amount of eco-friendly fluids
67 such as water mixed with gas mixed with air as dielectric fluid(Leppert 2018). The carbon
68 emissions and machining noises of the magnetic flux assisted technique EDM process have been
69 experimentally investigated to identify the machining setting for improving both environment and
70 machining performances(Zhang et al. 2018). The economic and environmental factors (energy,
71 electrode, and treatment of dielectric fluid) are experimented to analyze the harmful discharges
72 and discarding of the dielectric medium by three pillars sustainability approach(Zia et al. 2019).
73 The typical tap water dilutes in deionized water as a protecting medium in EDM experiments was
74 attempted to reduce the machining pollution. It was concluded that the toxic contaminants have
75 been reduced by diluted dielectric medium using Taguchi-grey analysis(Muthuramalingam 2019).
76 The suitable EDM process had also experimentally been attained by water-in-oil (nano-emulsion)
77 as insulation fluid. It has revealed that machining performance was also improved by that
78 method(Dong et al. 2019). A study exhibited that the near-dry green EDM process decreased the
79 97% fume emission with maximum debris when compared to existing liquid EDM (Dhakar et al.
80 2019). It was reviewed that the water, gas, bio- dielectric have been utilized to promote sustainable
81 development of dry and near-dry EDM processes(Singh et al. 2020). The vegetable oil-based
82 dielectrics in wet, near-dry EDM processes was experimentally justified that the eco-friendly EDM
83 performance had significantly been improved(Das et al. 2020). The electrode wear, energy, vapour
84 density, current, and dielectric contaminants had been investigated superiority and inferiority
85 ranking (SIR) method. It has been observed that to predict the best process parameter to improve
86 the overall performance(Das and Chakraborty 2020).

87 In the above-mentioned literature, the gas emission analysis of near-dry WEDM investigations
88 was not experimentally investigated. In this paper, the gas emission concentration, material
89 removal rate, and relative emission rate of near-dry WEDM (small quantity of water and

90 compressed air as dielectric) by Taguchi technique to predict the best machining setting for
91 minimizing gas emission and relative emission rate with MRR.

92 <Insert Figure 1 about here>

93 **2. Experimental method**

94 **2.1. Experimental setup**

95 The fuzzy logic CNC-controlled WEDM machining is used to cut AISI D2 tool materials by
96 0.18mm molybdenum wire electrode. The sustainable near-dry WEDM conditions are listed in
97 Table 1. The pictorial representation of the near-dry WEDM experimental arrangement is
98 displayed in Figure 1. 7 mm thickness of the wire tool has been used to conduct the experiments.
99 The wire tool is reciprocating with help of a servo motor and rollers. The compressed air and small
100 quantity of water mixed is called air-mist instead of hydrocarbon as a dielectric fluid. The
101 compressed air pressure and mixing water flow rate are measured by this special experimental
102 setup. The machining parameters pulse duration and spark current have been controlled and
103 observed by the WEDM control unit monitor. The pulse interval and gap voltage and wire tension
104 are constantly maintained as 48 micro-second, 75V, and 10 N respectively. In the experimental
105 setup, the complete WEDM machining zone is covered by a vacuum chamber in which the small
106 holes are provided to enter the atmospheric air (Figure 1). The outlet pipe is connected to a dust
107 collector which is made of paper material. The dust collector/ filter is connected to a vacuum pump
108 to suck the gas from the machining zone. Thus, the dust particles emitted during the cutting process
109 are collected in a filter (dust collector).

110 <Insert Table 1 about here>

111 **2.2. Machining responses measurement**

- 112 (i) The gas emission concentration (GES) is calculated by the ratio of the weight of filter
113 after cutting process in specific time to initial weight of filter by Equation (1)
114 (Thiyagarajan et al. 2014).

$$115 \quad GES = (wt_a - wt_b)/T \text{ mg/min} \quad (1)$$

116 Where wt_a - the initial weight of filter/dust collector paper before cutting process
117 in milligram, wt_b -the weight of filter paper before the cutting process in
118 milligram, T – time of machining duration in minutes.

119 (ii) The material removal rate (MRR) is calculated by Equation (2) as follows.

$$120 \quad MRR = (wt_m - wt_n)/T \text{ mg/min} \quad (2)$$

121 Where wt_m - the initial weight of work materials\ before cutting process in
122 milligram, Wt_n - Weight of work material before the cutting process in milligram,
123 T – time of machining duration in minutes.

124 (iii) The relative emission rate (RER) of the machining processes is calculated from the
125 ratio of GES and MRR as following Equation (3) (Thiyagarajan et al. 2014). It is used
126 to observe the quantity of gas emission to quantity of material removal during the
127 specific time of the cutting process.

$$128 \quad RER = \frac{GES}{MRR} \quad (3)$$

129 <Insert Table 2 about here>

130 <Insert Table 3 about here>

131 **2.3. Experimental design**

132 The Taguchi L27 orthogonal array is applied to conduct the near-dry WEDM experiments by
133 varying the machining parameters and making response observations. It is an effective design of
134 the experimental (DOE) method to identify the influences of each factor with minimum numbers
135 of the test. Initially, the trial tests were conducted to finalize the machining parameters levels. The
136 value of each parameter level is shown in Table 2. The values of each parameter level have been
137 finalized based on permitted ranges of parameters and the combination of parameters setting is
138 implemented to measure the required results. The levels combination of air pressure, the flow rate
139 of mixing water, spark current and pulse width are used to conduct the 27 trials of experiments as
140 listed in Table 3. In this paper, the mean effect of parameters is considered to study the response
141 variations. The influences and contributions of each parameter on gas emission concentration,
142 material removal rate, and relative emission ratio are predicted by Taguchi analysis. The analysis
143 of variance (ANOVA) is performed for the mean values of each factor. The Taguchi analysis of

144 GES, MRR, and RER are shown in Tables 4,5, and 6 respectively. The following formulae
 145 (Equations (4) – (8)) are employed to find the internal terms of Taguchi analysis.

146 Total sum of Square $SS_T = \sum_{i=1}^k (m_i^2 - (k \times m_t^2))$ (4)

147 Parameter sum of Square $SS_P = \sum_{i=1}^r \left(\frac{sm_i^2}{r} - \frac{1}{k} (\sum_{i=1}^k m_i) \right)$ (5)

148 Variance $V_p = \frac{SS_P}{df_p}$ (6)

149 Corrected sequential sum of square $SS_C = SS_P - (df_p)(V)$ (7)

150 Percentage of contribution $C_{\%} = \frac{SS_P}{SS_C}$ (8)

151 Where ‘k’ represents the number of parameters, ‘j’ as the parameter level, m_i as the mean value
 152 of ith experiment, m_t as the total mean value, sm_j as the sum of the value of j^{th} as level of the
 153 parameter, ‘r’ as the number of repetition, and df_p as the degree of freedom.

154 **3. Results Analysis and Discussions**

155 **3.1 Analysis of GEC**

156 It was observed from Taguchi analysis that the spark current and air pressure significantly
 157 affect the mean value of GEC. The percentage (%) contribution of machining factors, i.e., spark
 158 current (45.78%), air pressure (32.03%), and pulse width (18.15%) have been higher than the flow
 159 rate of mixing water (2.79%) on GEC.

160 <Insert Table 4 about here>

161 It was observed from Table 4 that the percentage contribution of spark current on GEC was
 162 45.78%. It revealed that current is providing an important impact on the GEC of the reacting
 163 dielectric fluid as shown in Figure 2. While increasing current, the gas emission is also increased
 164 due to an increase in the concentration of spark energy in the cutting zone(Thiyagarajan et al. 2012;
 165 Dhakar et al. 2019). It is caused by the increasing thermal reaction between work material and a
 166 wire tool. Thus, the gas emission will be increased in the machining atmosphere/ zone. The air
 167 pressure has the second-highest contribution on the GEC by increasing the dielectric strength and
 168 reducing evaporation of dielectric fluid due to minimum reaction of water with burned metal.
 169 While increasing the air pressure, the machining performance will be improved and material debris
 170 also increased(Boopathi and Sivakumar 2014). However, a small amount of mixing water is only
 171 evaporated and metal is completely burned during the cutting process. It caused the gas emission

172 mixing with the surrounding air is decreasing while increasing air pressure (Suthangathan
173 Paramashivan et al. 2012).

174 <Insert Figure 2 about here>

175 The emission concentrations increased by the increase in pulse width due to high heat energy,
176 evaporation, and metal melting are directly varied to the quantity of pulse heat by pulse time(Evertz
177 et al. 2006; Sivapirakasam et al. 2011; Suthangathan Paramashivan et al. 2012; Thiagarajan et al.
178 2012). The high heat debris particles will react with water which causes the smoke by long
179 availability of spark in the cutting zone(Spedding and Wang 1997; Pandey et al. 2015; Sadagopan
180 and Mouliprasanth 2017). The flow rate of water mixing with air was less contribution on GEC
181 (2.79%) due to mixing water had atomized by high-pressure air in the cutting zone. While
182 increasing flow rate from 8 to 12 ml/min, the maximum portion of water has been perfectly mixed
183 with pressurized air and from 12 to 16 ml/min, un-atomized water particle reaction with debris,
184 then the GEC is getting increased. In the near-dry WEDM process, the gas emission by the burning
185 of dielectric fluid will be decreased at the flow rate of 12 ml/min. thus, the near-dry WEDM process
186 is representing as a Green machining process(Pandey et al. 2015; Valaki et al. 2015; Dhakar et al.
187 2019; Singh et al. 2020).

188 <Insert Table 5 about here>

189 **3.2 Analysis of MRR**

190 It was revealed from Table 5 that the percentage of contributions of spark current, pulse width,
191 air pressure, and flow rate of mixing water on MRR is 33.71%), 23.42%, 31.78%, and 8.68%
192 respectively.

193 <Insert Figure 3 about here>

194 It was indicated from Taguchi analysis (Figure 3) that the moderate air pressure (5 bar)
195 improves the MRR due to efficient flushing and sufficient cooling effect in the near-dry WEDM
196 process(Boopathi and Sivakumar 2012; Boopathi and Myilsamy 2021). At the low air pressure (3
197 bar), the metal debris is reduced due to insufficient spark in the plasma zone. The spark transfer
198 between wire and workpiece materials has been disturbed by increasing pressure to 7 bar (Boopathi
199 and Sivakumar 2013, 2014, 2016). While increasing the mixing water flow rate, the MRR is
200 increased due to effective cooling and an increase in dielectric strength in the cutting
201 zone(Boopathi and Sivakumar 2012). The spark current and pulse width are significantly

202 contributing to improving the MRR due to high thermal energy, high melting, and vaporization of
203 metal in the cutting zone(Abbas et al. 2012; Kumar et al. 2020).

204 <Insert Table 6 about here>

205 **3.3 Analysis of RER**

206 The effects of machining parameters on the RER of near-dry WEDM are shown in Figure 4. It was
207 also revealed from Table 6 that the percentage of contributions of air pressure, the flow rate of
208 mixing water, spark current, and pulse width on RER are 85.01%, 9.36%, 3.52%, and 0.81%
209 respectively.

210 It was observed from Table 6 that air pressure has the highest contribution than mixing water flow
211 rate, pulse width and spark current on RER. the pressure is directly proportional to expectations of
212 both responses (MRR and gas emission) due to high air pressure promotes green machining
213 processes(Dhakar et al. 2019; Ming et al. 2021). It was also revealed from the literature the
214 dielectric medium is a significant factor in gas emission in EDM processes(Leão and Pashby 2004;
215 Chakraborty et al. 2015; Ng et al. 2017; Singh et al. 2018). In the near-dry WEDM processes, the
216 liquid/ hydrocarbon dielectric fluid has been replaced by air or air mixed with a small amount of
217 water to control the emission.

218 <Insert Figure 4 about here>

219 While increasing the flow rate of mixing water, the RER also decreased due to effective cooling,
220 good dielectric strength and flush-out debris effectively in the cutting zone. The highest quantity
221 of water (16 ml/min) provides sufficient dielectric strength and cooling effect in the cutting zone.
222 The spark current and pulse width parameters are giving inverse influences on gas emission and
223 MRR. Thus, these factors were insignificant and less contribution to RER. However, the lowest
224 values of spark current and pulse time will promote the eco-friendly machining process (Figure 4).

225 <Insert Table 7 about here>

226 **3.4 Prediction and confirmation experiments**

227 The optimum machining parameter settings for minimizing the gas emission and RER, and
228 maximize the MRR are shown in Table 7. The optimum machining parameter settings to minimize
229 GEC (0.179 mg/min) were air pressure (7 bar), flow rate (12 ml/min), spark current (3 A), and

230 pulse width (16 μ s), and predicted value was at best parameter setting. The predicted GEC value
231 was validated by a confirmation experiment (0.181 mg/min). The optimal machining parameter
232 settings to maximize the MRR (105 mg/min) were air pressure (5 bar), flow rate (16 ml/min), spark
233 current (5 A), and pulse width (28 μ s). The predicted MRR value was validated by a confirmation
234 experiment (106 mg/min). The best machining parameter setting to minimize the RER (0.0057)
235 were air pressure (7 bar), flow rate (16 ml/min), spark current (3 A), and pulse width (16 μ s). The
236 predicted RER value was validated by a confirmation experiment (0.006).

237

238 **4 Conclusions**

239 In this research, the GEC, MRR, and RER of sustainable near-dry wire-cut EDM process have
240 been analyzed using the Taguchi method. The following conclusions were derived as follows.

- 241 • The gas emission concentration (GEC) has been reduced by minimizing pulse width,
242 spark current, and flow rate of mixing water and maximizing air pressure. Air pressure
243 increases the dielectric strength and reducing the evaporation of dielectric fluid due to
244 the minimum reaction of water with burned materials. The moderate flow rate of water
245 gives the lowest emission due to avoiding the chemical reaction of unburned materials.
246 The current and pulse width enhance the gas emission rate because of the highest
247 debris by maximum intensity of long spark energy in the cutting zone.
- 248 • The MRR has been improved by increasing pulse width, spark current, and flow rate
249 of mixing water. It is maximum at moderate air pressure (5 bar) due to efficient
250 flushing and sufficient cooling effect in the cutting zone. The pulse width and current
251 improved the MRR because of the highest debris by the good intensity of a long spark.
252 The highest flow rate of water improves the MRR due to sufficient dielectric strength
253 with good flushing efficiency.
- 254 • The relative emission rate (RER) was reduced by the lowest input of spark current,
255 pulse width, and highest value of air pressure and mixing water flow rate due to
256 sufficient dielectric strength and chilling effect in the cutting zone. While increasing
257 air pressure, RER is getting reduced due to the complete burning of materials at
258 maximum pressure. RER is reduced by the minimum intensity of spark at the low
259 value of pulse width and spark current levels.

- 260 • The air pressure was the highest contribution (85.01%) on relative emission rate by
261 increasing pressure minimize the gas emission and improves the materials debris.
262 Hence the air pressure is one of the key parameters to enhance the sustainable near-
263 dry wire-cut EDM process.
- 264 • The predicted values of GEC, MRR, and RER from Taguchi analysis have been
265 validated by a set of confirmation experiments.

266 **Acknowledgment Author**

267 The author thanks Mechanical Engineering at Bannariamman Institute of Technology,
268 Sathayamanagalam, Erode, Tamilnadu, India. for helping to carry out this research work.

269 **Ethics approval**

270 Not Applicable

271 **Consent to participate**

272 Not Applicable

273 **Consent for publication**

274 Not Applicable

275 **Authors Contributions**

276 Dr. Boopathi Sampath contributed to conducting experiments, experimental design, analyzing
277 and interpreting the data regarding the near-dry WEDM Process.

278 **Funding**

279 No fund received.

280 **Competing Interests**

281 The author declares that he has no competing interests.

282 **Availability of data and materials**

283 The datasets generated during and/or analyzed during the current study are available from the
284 corresponding author and included in this article.

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404

Figures

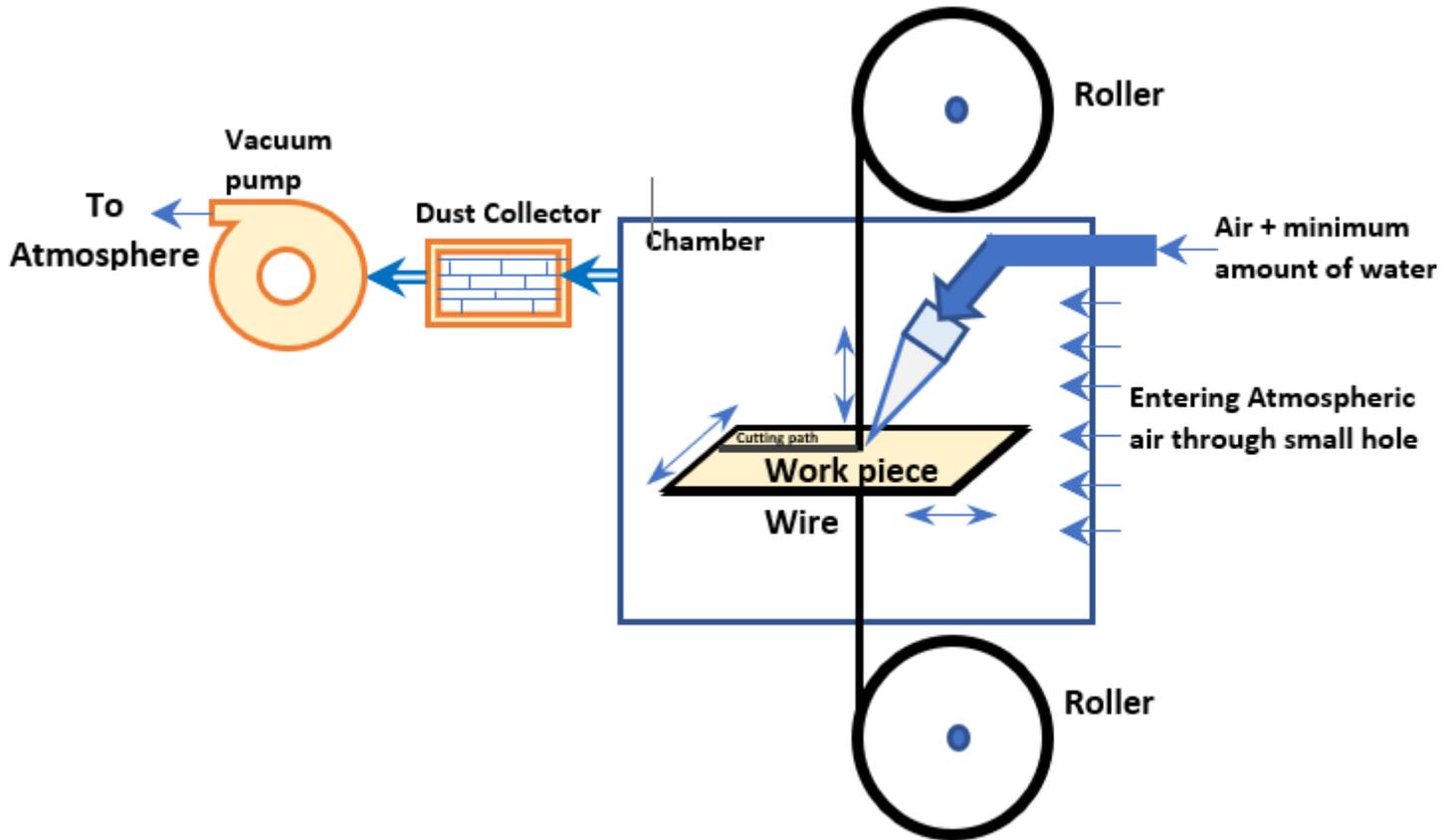


Figure 1

Graphic drawing of near-dry wire-cut EDM experimental arrangement to measure the gas emission concentration

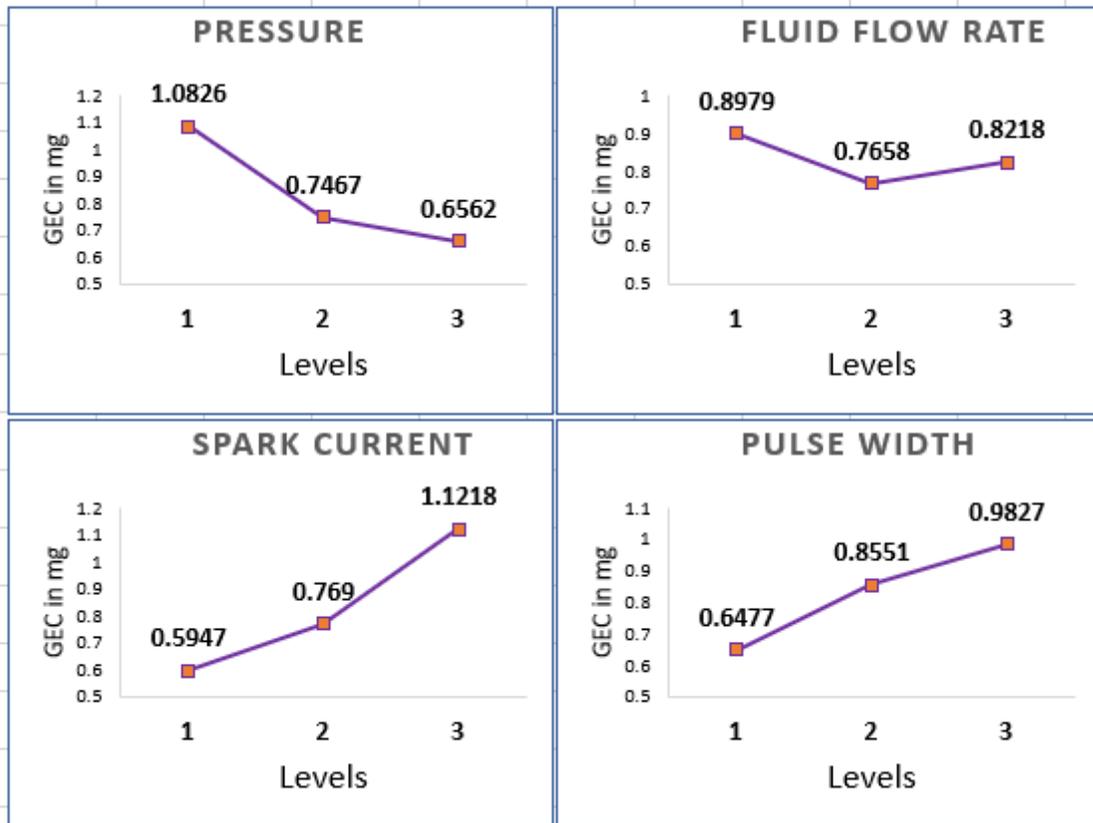


Figure 2

Impact of machining parameters of near-dry WEDM on GEC

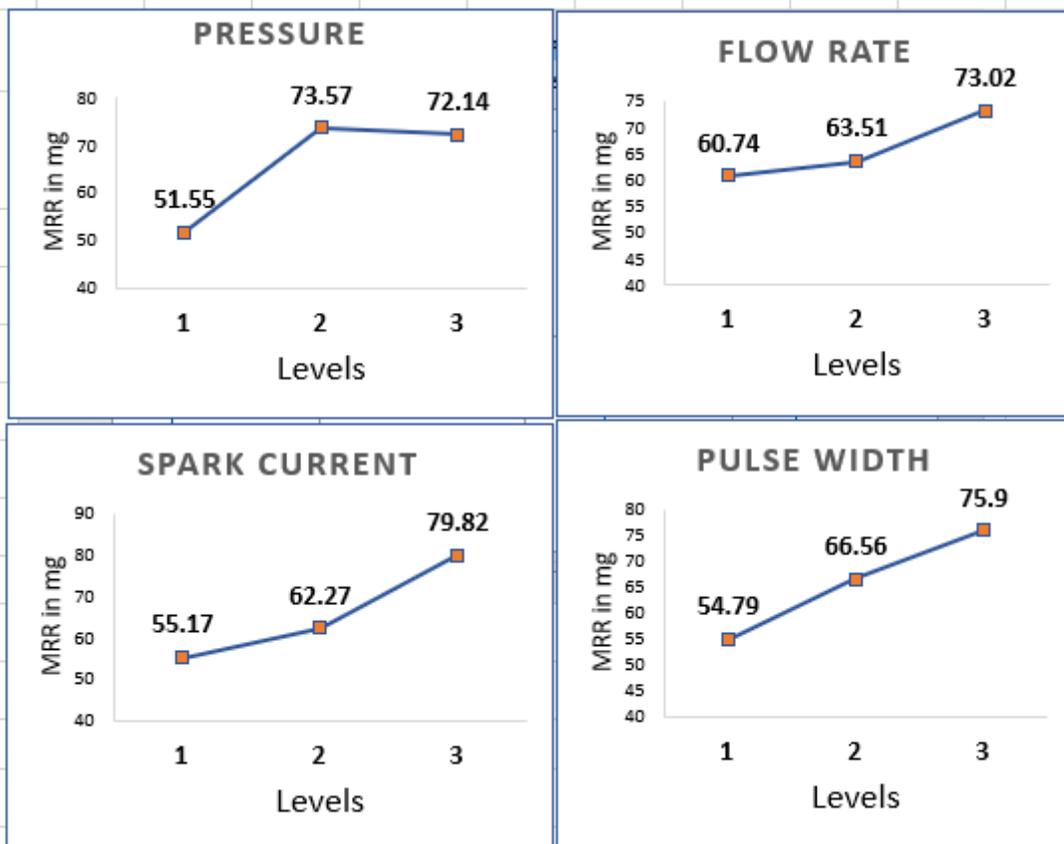


Figure 3

Impact of machining parameters of near-dry WEDM on MRR

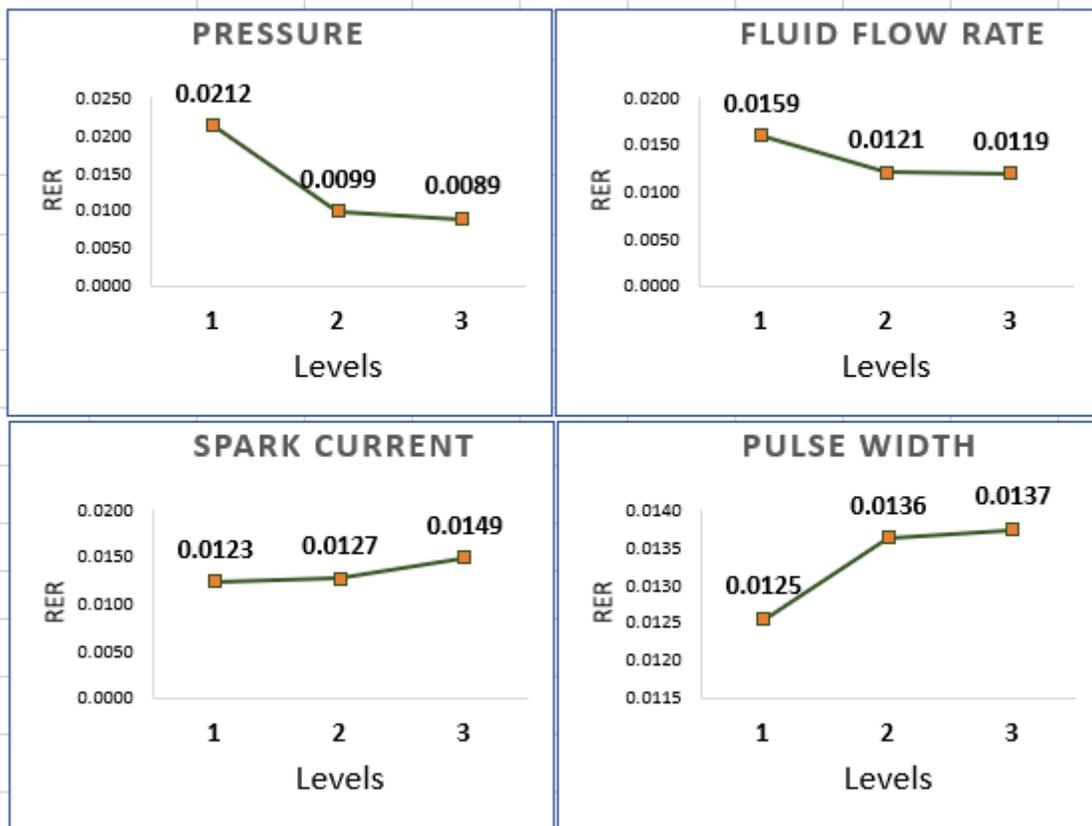


Figure 4

Impact of machining parameters of near-dry WEDM on RER