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The influence of the multi-level structure under high drawing on the preparation of high strength Lyocell fiber

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Abstract:

In order to research the multi-level structure of Lyocell fiber at different draw ratios and to reveal the limiting factors for preparing the high strength Lyocell fiber, the paper reports on the effect of draw ratio including low drawing (1-5), high drawing (6-11) and excessive drawing (12-20) on the multi-level structure and the mechanical properties of Lyocell fiber. The structure was determined by wide-angle X-ray diffraction, small-angle X-ray scattering and fibrillation test, and the result showed that, at low draw ratio stage, the breaking strength, yield strength and modulus of the fiber increased with the draw ratio owing to crystallinity as well as orientation increased while the micropore decreased, and there are almost no microfibrils on the fiber surface. At high draw ratio stage, the orientation of amorphous region increasing was the principal reason for the increase of fiber mechanical properties, and the micropores continued to decrease and a few short and thick microfibril was formed. At excessive draw ratio stage, the breaking strength remained constant mainly due to the basically unchanged crystallinity and orientation of the fibers, the yield strength and modulus decreased due to the slip of the highly crystallized and oriented elementary fibril. Meanwhile, the micropores still decreased and became much slenderer, the number of microfibrils increased and the microfibrils showed tenuous structure. It could be summarized that Lyocell fiber had the characteristics of multi-level structure, and the fundamental reason limiting the improvement of mechanical properties with draw ratio increase was the slip of elementary fibril.

Keywords: *Lyocell, draw ratio, multi-level structure, WAXD, SAXS*

Introduction

Lyocell fiber is known as one of the most representative green fiber in the 21st century due to its natural and renewable resource advantages, clean processing technology and degradable environmental friendliness. Lyocell fiber has the advantage of antistatic, hygroscopicity and comfortable wearing, and it is widely used in clothing, home textile and medical field (Ibrahim 2002; Medronho et al. 2012; Klemm et al. 2005; Chen et al. 2015). Furthermore, Lyocell fiber has much higher strength and modulus, especially the outstanding wet strength and wet modulus compared to ordinary viscose fiber since its invention due to its dry jet wet spinning forming process (Röder et al. 2013; Woodings 1995; Ganster et al. 2006). It can be inferred that Lyocell fiber could have made a further strength in mechanical properties, however, there is no Lyocell

43 fiber product with much more outstanding properties than high-strength viscose fiber up to now,
44 which seems to be a subject worthy of further discussion.

45 There has been considerable research in Lyocell fiber to improve the mechanical properties
46 during the past decade by using high degree of polymerization cellulose pulp, adding modifier to
47 the solution and carrying thermal treatment on the fiber et al (Fink et al. 2014; Zhang et al. 2010a,
48 b). However, cellulose pulp with high degree of polymerization makes dissolving and spinning
49 difficult, and the addition of modifier may affect the recovery of NMMO (Zhang e al. 2010;
50 Wendler et al. 2005; Wendler et al. 2008a, b). With regard to spinning process conditions, although
51 there are many factors (such as air gap length, temperature and concentration of coagulation bath,
52 spinning speed and so on) affecting properties of Lyocell fiber (Mortimer et al. 1996a, b; Duan et
53 al. 1999; Shao et al. 2000), the most significant factor is the draw ratio under the premise of other
54 process optimization. It is a common understanding of fiber preparation technology to obtain high
55 crystallinity and high orientation fibers by increasing the draw ratio, so as to achieve the goal of
56 high strength and high modulus. Is it the same for Lyocell fibers? Many researchers have studied
57 the relationship between the draw ratio and the structure behaviors of Lyocell fiber (Loubinoux et
58 al. 1987; Mortimer et al. 2008; Kong et al. 2005; Hauru et al. 2014, Jiang et al. 2012). Mortimer
59 and his coworkers have made great effort to investigate the influence of physical process
60 parameters on the structure formation of Lyocell fiber (Mortimer et al. 2008). It was found that the
61 breaking strength and modulus increase to a plateau region with draw ratio increase and they
62 attributed this change to the maximum crystallization and orientation, which was same to Kong
63 and Lauri' results (Kong et al. 2005; Hauru et al. 2014). However, it obviously cannot explain the
64 fact that the fiber diameter (or fineness) decreases with draw ratio increase. It has long been known,
65 different types of regenerated cellulose fibers (such as viscose fiber, modal fiber and Lyocell fiber) are
66 composed of elementary fibril which is consisted of cellulose II lamellar crystal and low ordered
67 cellulose molecules in the form of string beads, and the microfibrils are comprised of elementary fibril
68 and the micropores between the elementary fibril (Lenz et al. 1988; O'Sullivan 1997; Blackwell et al.
69 1975; Schurz et al. 1994; Statton 1956; Moss et al. 2010); it means that there are some other
70 structure variations at different levels besides crystallization and orientation, which have a very
71 remarkable impact on the mechanical properties in the process of spinning.

72 High performance regenerated cellulose fiber can be used in tire cord, carbon fiber precursor
73 and other industrial fields, however, the mechanical properties are still the bottleneck for the
74 application in industrial field of Lyocell fibers (Zhang et al. 2010; Peng et al. 2003). The
75 investigated on the multi-level structure change of Lyocell fiber with draw ratio increasing is of
76 great importance to understand the essential reason that limit the mechanical properties
77 improvement, meanwhile, it can provide guidance for the improvement of Lyocell preparation
78 process and fiber properties. The present study aimed at determining the multi-level structure of
79 Lyocell fiber with draw ratio increasing, providing a basis for understanding the change of
80 mechanical properties in terms of structural features. The structure evolution mechanism in terms
81 of low drawing, high drawing and excessive drawing was proposed according to wide angle X-ray
82 scattering (WAXD), small angle X-ray scattering (SAXS), birefringence, scanning electron
83 microscope (SEM) combined with fibrillation test.

84 Experimental

85 Materials

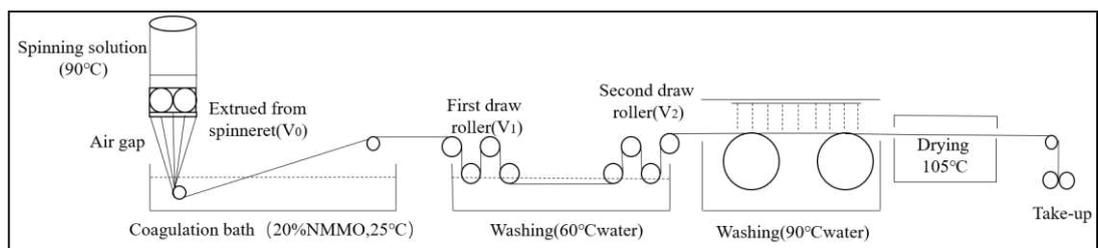
86 Wood pulp (7.15 w t% water content, DP=550, α -cellulose content was 91%) was provide by
87 COSMO Specialty Fibers, Inc, and N-methylmorpholine-N-oxide (NMMO) aqueous solution was
88 bought from Amines & Plasticizers Limited with initial water content of 50 w t%. The propyl
89 gallate (PG) was used as a stabilizer and was bought from Aladdin Industrial Corporation.

90 Preparation of cellulose solution

91 The NMMO aqueous solution was mixed with cellulose pulp and propyl gallate (PG), after
92 swelling at 50 °C for one hour, the mixture was dissolved at 90 °C in a planetary stirred tank with a
93 vacuum pressure was -99 kpa. The final solution was composed of 10 w t% cellulose, 78 w t%
94 NMMO and 12 w t% water.

95 Preparation of regenerated cellulose fibers

96 A customized spinning equipment was used to prepared the Lyocell fibers and the schematic
97 diagram of spinning process is shown in Fig.1. The spinning temperature was 90 °C, the
98 specification of spinneret is 60 holes * 0.1mm, and the air gap length was 50 mm with a relative
99 humidity of 65% and temperature of 25 °C. The concentration of NMMO in coagulation bath is 20
100 w t% and temperature of coagulation bath is 25 °C. Then, the solvent in filament was washed out
101 in 60 °C hot water bath and 100 °C boiling water bath, and finally dried in 105 °C for 30 min to
102 obtain fiber samples. 20 samples were prepared with different draw ratios by keeping the extrusion
103 speed (6m/min) constant, adjusted the speeds of the first drawing roller.
104



105 Fig. 1 Schematic diagram of Lyocell fiber spinning process
106
107

108 Measurements

109 The diameter of single filaments of all samples was measured by optical microscope
110 (8XB-PC, China), and the breaking strength, yield modulus and initial modulus of Lyocell fibers
111 were measured on a monofilament strength tester at least 30 measurements for each sample, and
112 the drawing rate was 20 mm/min.

113 The fiber cross-section was observed on a scanning electron microscope, and the
114 cross-sections of the fibers were observed after gold spraying treatment.

115 The WAXD measurements of the fibers were performed on the BL14B1 beam line of
116 Shanghai Synchrotron Radiation Facility at a wavelength of 0.124 nm (Yang et al., 2015). The

117 distance between sample and detector of WAXD is 329.4mm. And the X-polar (Precision works
 118 NY, Inc., USA) was used to analysis the data include background correction, radial and azimuth
 119 integration. (Jiang et al 2012; Yuan et al; Chen et al., 2019).

120 The crystallinity is determined by the equation (1):

$$121 \quad X_c = \frac{S_c}{S_a + S_c} \times 100\% \quad (1)$$

122 where X_c , S_c and S_a represent the crystallinity, the peak areas of crystalline phases and the
 123 peak areas of amorphous phases respectively.

124 The Scherrer equation was used to calculate the crystal size of Lyocell fibers (Jiang et al.
 125 2012).

$$126 \quad L_{hkl} = \frac{K\lambda}{\beta \cos\theta} \quad (2)$$

127 where L_{hkl} represents the crystal size of (hkl) plane, λ is 0.124 nm in this experiment, 2θ is
 128 the diffraction angle (2θ), β is the integral width corresponding to the diffraction peak of crystal
 129 plane and K is 0.9 in this experiment.

130 The orientation of crystal region was determined from the equation (3) (Klug and Alexamder
 131 1954):

$$132 \quad f_c = (3\langle \cos^2\varphi_{c,z} \rangle - 1)/2 \quad (3)$$

133 where $\langle \cos^2\varphi_{c,z} \rangle$ is orientation parameter of crystal axis (c) relative to the fiber axis (Z).

134 The orientation parameter $\langle \cos^2\varphi_{c,z} \rangle$ was obtained according to the Wilchinsky Model
 135 (1959) and crystal symmetry of regenerated cellulose fibers (Kolpak and Blackwell 1976). For
 136 Lyocell fiber, the reflections in equatorial (110), (020) and (-110) were used to calculate the
 137 orientation parameter $\langle \cos^2\varphi_{c,z} \rangle$, and for each reflection (hkl) , the orientation parameter \langle
 138 $\cos^2\varphi_{hkl} \rangle$ can be determined by equation (4) and (5) (Klug and Alexamder 1954):

$$139 \quad \langle \cos^2\varphi_{hkl} \rangle = \cos^2\theta \langle \sin^2\varphi_{hkl} \rangle \quad (4)$$

$$140 \quad \langle \sin^2\varphi_{hkl} \rangle = \frac{\int_0^{\pi/2} I(\varphi_{hkl}) \sin^2\varphi_{hkl} \cos\varphi_{hkl} d\varphi_{hkl}}{\int_0^{\pi/2} I(\varphi_{hkl}) \cos\varphi_{hkl} d\varphi_{hkl}} \quad (5)$$

141 where φ_{hkl} is the azimuthal angle and $I(\varphi_{hkl})$ is the diffraction intensity along the
 142 reflection plane (hkl) .

143 The birefringence (Δn) was determined on polarizing microscope (type SSY-C).

144 The orientation factor (f_a) of amorphous region was calculated by Stein equation (6):

$$145 \quad f_a = \frac{\Delta n - X_c \Delta n_c^0 f_c}{(1 - X_c) \Delta n_a^0} \quad (6)$$

146 where Δn represents the birefringence of Lyocell fibers, X_c represents the crystallinity, Δn_{co} is
 147 the birefringence index of the crystalline regions with a value of 0.0545, and Δn_{ao} is the
 148 birefringence index of amorphous regions as 0.0545 (Peng et al. 2003).

149 The SAXS measurements were determined at BL16B beamline of Shanghai Synchrotron
 150 Radiation Facility with X-ray wavelength of 0.124 nm and a distance between sample and detector
 151 of 1,920 mm (Zeng et al. 2017). The detailed structure parameters of the fibers were obtained by
 152 the X-polar referred to the previous methods (Murthy and Grubb 2010; Wu et al. 2000; Jiang et al.
 153 2007; Colombe et al. 2011).

154 For Lyocell fiber, it is generally accepted that the striae on the equator in the SAXS is caused
 155 by the scattering of the micropores along the fiber axis (Crawshaw et al. 2000; Vickers et al. 2001;

156 Chen et al. 2007). Therefore, Guinier functions can be used to calculate the transverse dimension
157 of micropore as shown in equation (7) (Guinier and Fournet 1955):

$$158 \quad I(q) = I(0) \exp(-q^2 R^2/5) \quad (7)$$

159 where R is the radius of micropores, q ($q = 4\pi \sin \theta/\lambda$) represents the scattering vector, θ
160 is half of the scattering angle and λ is 0.124 nm in this experiment.

161 And the average micropore length (L) and orientation deviation angle (B_ϕ) which relative to
162 fiber axis were obtained according to the method of Ruland (Ruland 1969).

163 The real density of the fiber is calculated by the crystallinity of Lyocell fiber (the crystal
164 region density of Lyocell fiber is 1.585, the amorphous region density is 1.483), and the real
165 density of the fiber is calculated from equation (8):

$$166 \quad \rho_0 = 1.585 * X_c + 1.483 * (1 - X_c) \quad (8)$$

167 where X_c is the crystallinity of the fiber.

168 The apparent density of the fiber is calculated equation (9):

$$169 \quad \rho_l = (4 * D) / (10000 * \pi * d^2) \quad (9)$$

170 where D is the linear density of the fiber, and d is the fiber diameter.

171 The fibrillation behavior was determined by observing the morphology of the treated Lyocell
172 fibers with an optical microscope after radiating the fiber surface for 30 min by ultrasonic wave
173 (Yuan et al, 2019). The average length of fibril is obtained by processing the image and
174 quantitatively calculated by equation (10):

$$175 \quad L_f = \frac{1}{n} \sum_{i=1}^n l_i \quad (10)$$

176 Where L_f is the average fibril length, l_i is the fibril length, n is the total number of fibrils.

177 **Results and discussion**

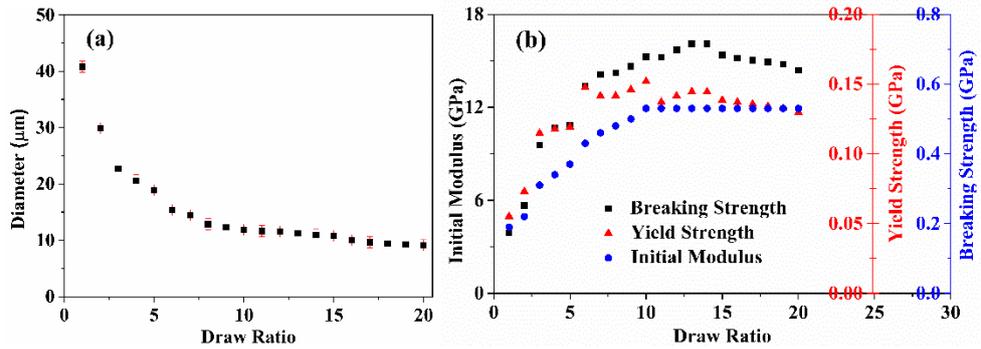
178 **Mechanical properties of Lyocell fibers with different draw ratios**

179 As we all known, the diameter of the fiber decreased as the draw ratio increasing during
180 spinning, which help to improve the mechanical properties of the fiber. It can be seen from Fig. 2(a)
181 that the diameters of the fibers decreased non-linearly, and the data can be fitted according to the
182 model proposed by Mortimer (Mortimer 1996), and a theoretical prediction of fiber diameter (d)
183 could be calculated according to the draw ratio (D_R) as follows:

$$184 \quad d = d_0 * D_R^{-a} \quad (11)$$

185 Where d_0 is the diameter of the spinneret, and the value of a is 0.50. The model is consistent
186 with the data of this paper, and gave the value of d_0 and a is 41 μm and 0.51, respectively, which is
187 basically the same as the value measured by Mortimer. Additionally, it can be seen that the
188 diameter decreases obviously at first and then slowly with draw ratio increase.

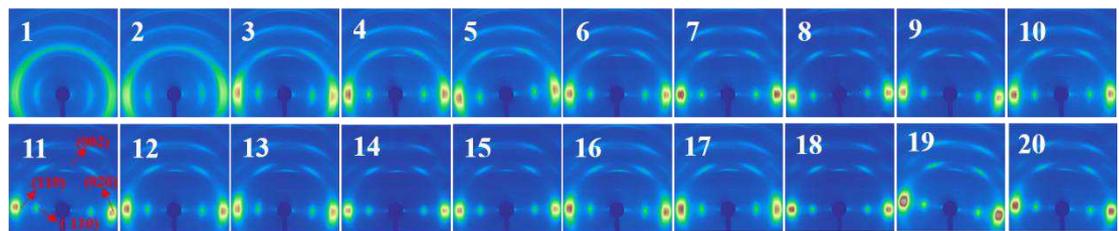
189



190
191 Fig. 2 Diameter (a) and mechanical properties (b) of Lyocell fibers with different draw ratios
192 (1-20)
193

194 The mechanical data obtained from stress-strain curves (as shown in supporting information
195 (Fig. S1)) of Lyocell fibers with different draw ratios are shown in Fig. 2(b). It can be seen that the
196 breaking strength of Lyocell fiber gradually increases to a plateau area with draw ratio increasing
197 to 12, while the modulus and yield strength increase first and then decrease slightly. Combined
198 with the results of fiber diameter, the decrease of fiber diameter means the improvement of
199 orientation and density, the mechanical properties of fibers should increase, but the actual result is
200 obviously not like this. Normally, the mechanical properties of fibers are directly related to the
201 structure, the difference between breaking strength, modulus and yield strength reflects the
202 diversity of fiber structure, it can be said that there are some uncertain structures different from
203 previous studies, which result in diameter of the fiber decrease with draw increase, while the
204 breaking strength increases to a plateau and the modulus and yield strength increase first and then
205 decrease. This paper will make a detailed study of its structural changes in the following.

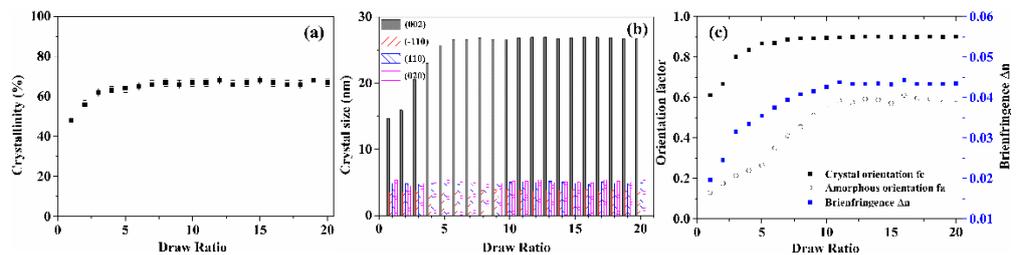
206 **Evolution of supramolecular structure of Lyocell fiber**



208
209 Fig. 3 WAXD patterns of Lyocell fibers with different draw ratios (1-20)
210

211 The crystal structural parameters of Lyocell fibers prepared at different draw ratio were
212 calculated by analyzing the 2D WAXD patterns and the result was shown in Fig. 3. It can be seen
213 that Lyocell fiber showed typical cellulose II crystalline structure and the diffraction pattern shown
214 with the characteristic reflections of (-110) , (110) and (020) crystal plane on the equator and the
215 (002) crystal plane reflection in meridian. From Fig. 3, diffraction arcs became shorter as draw
216 ratio increased which illustrates that the orientation of crystal region relative to fiber axis get better
217 with draw ratio increasing, resulting in a higher orientation of Lyocell fibers. Subsequently, in
218 order to further analyze the microstructure change, one-dimensional integral curves were obtained

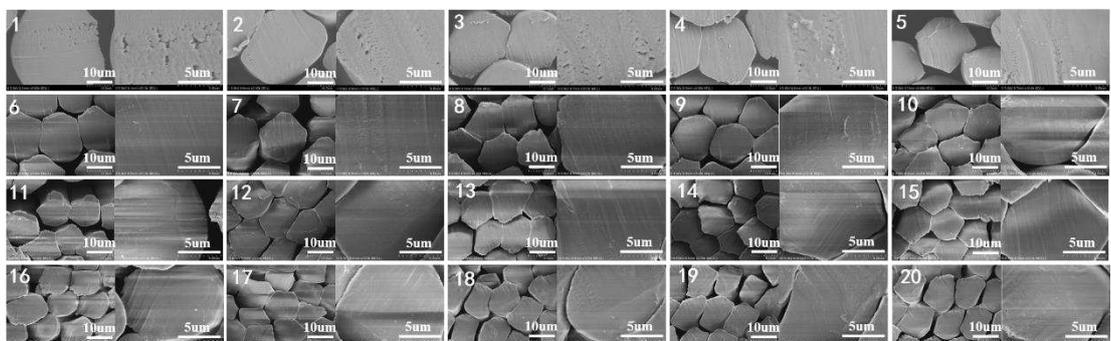
219 by processing the two-dimensional WAXD patterns as shown in supporting information (Fig. S2),
 220 and the information of crystal and amorphous structural parameters as depicted in Fig. 4 were
 221 determined by fitted the one-dimensional intensity curves with six crystal peaks with the strongest
 222 diffraction and an amorphous peak according to the cellulose II crystalline structure which was
 223 shown at supporting information (Fig. S3). The crystallinity and crystal size of the fibers as shown
 224 in Fig. 4(a) and (b) indicated that the crystallinity of fibers increased with draw ratio increasing at
 225 low drawing stage, but remained constant at high and excessive drawing stage. The crystal size of
 226 (-110), (110) and (020) crystal plane on the equatorial line does not change significantly, while the
 227 crystal size of (002) crystal plane on the meridian direction increases significantly at low drawing
 228 stage, which was the principal reason for the raise of crystallinity
 229



230
 231 Fig.4 The supramolecular structure parameters of Lyocell fibers with different draw ratios (1-20):
 232 (a) crystallinity; (b) crystal size; (c) crystal orientation factor (f_c), amorphous orientation factor (f_a),
 233 birefringence index (Δn)
 234

235 The orientation factor of crystal region (f_c), orientation factor of amorphous region (f_a) and
 236 birefringence index (Δn) were also obtained and shown in Fig. 4(c). The orientation of crystal
 237 regions and amorphous regions of Lyocell fibers as well as the birefringence index also increase
 238 with the draw ratio increasing. However, the increase of crystal orientation is mainly occurred at
 239 low drawing stage which is consistent with the change of crystallinity, while the increase of
 240 amorphous orientation and birefringence occurred at low and high drawing stage.

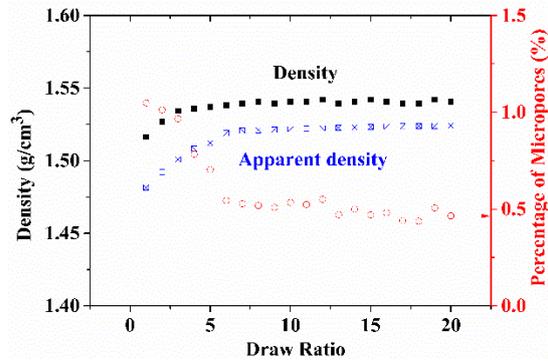
241 Evolution of fibril and micropore structure of Lyocell fiber



242
 243 Fig. 5 SEM images of Lyocell fibers with different draw ratios (1-20)
 244

245 In addition to the crystalline and orientation structure, the microstructure (such as hollows,
 246 micropores and microfibrils) in Lyocell fiber also has a very important impact on the mechanical
 247 properties (Blackwell and Kolpak 1975; Schurz and Lenz 1994; Statton 1956; Moss et al. 2010). The

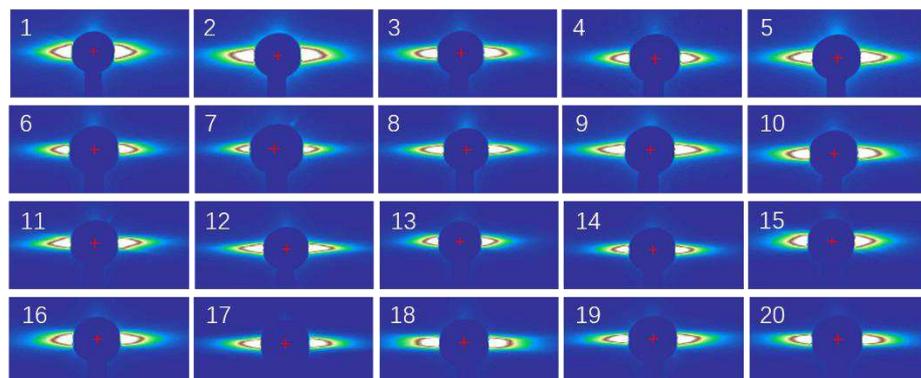
248 morphological structure of the cross-sections of fibers was presented in Fig. 5. It can be observed that
249 there were a few hollows with micron size in the fiber at low drawing stage, and the size of
250 hollows gradually decreased at high and excessive drawing ratio, leading to the formation of the
251 dense cross-section.
252



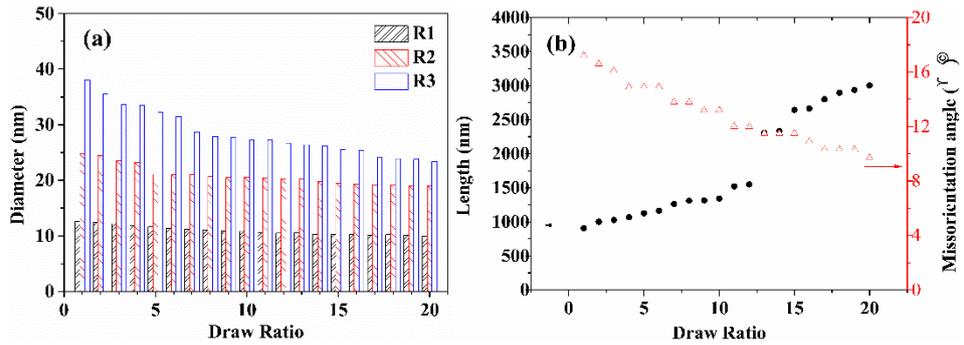
253
254 **Fig. 6** The changes of the density and apparent density of Lyocell fibers with increasing draw
255 ratios (1-20)
256

257 In addition to the micron-scale hollow, there are also some nano-scale micropore in Lyocell
258 fibers, which is located between fibrils and fibrils according to the basic fiber model of cellulose
259 fiber proposed by Schurz (Schurz and Lenz 1994). It is difficult to quantitatively analyze the
260 nano-size variation by electron microscopy. Therefore, density method, SAXS technology and
261 fibrillation test were used to study the evolution of micropore of Lyocell fiber during drawing.

262 The real density and apparent density of Lyocell fiber with draw ratio increase were
263 calculated and shown in Fig. 6. It can be seen that compared to the real density, apparent density
264 was smaller and increased much slower with the draw ratio increasing, indicating the existence of
265 micropores in the fiber. The percentage of micropores volume was obtained by further calculating
266 the apparent density and real density additionally shown in Fig. 6. It can be seen that the decrease
267 trend of the percentage of micropores volume was similar to the increase trend of apparent density.
268



269
270 **Fig. 7** SAXS patterns of the Lyocell fibers with different draw ratios (1-20)
271



272

273 Fig. 8 Structural parameters from SAXS patterns of Lyocell fibers with different draw ratios (1-20):

274

(a) micropores diameters; (b) micropores length and misorientation angle

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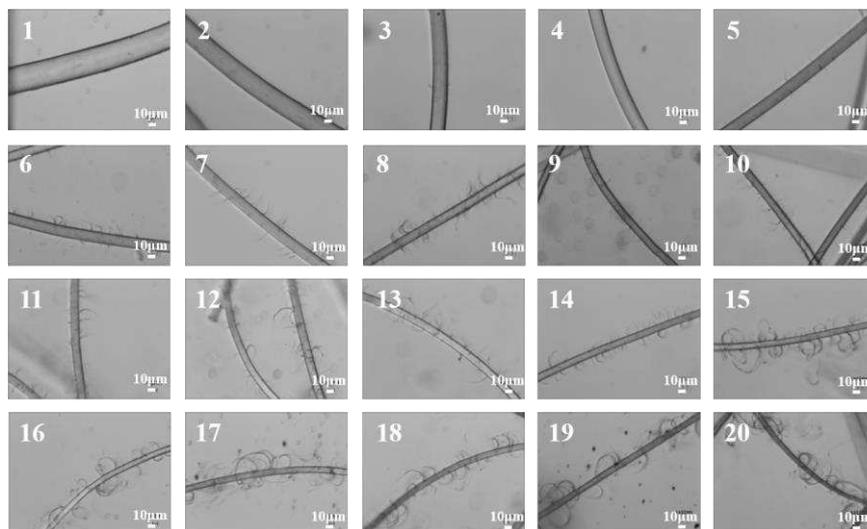
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290

The micropores of Lyocell fiber at different draw ratio were measured by SAXS as shown in Fig.7 in order to further investigated the microstructure evolution with the increase of draw ratio. The sharp and long striae on the equator in the SAXS is caused by the scattering of the micropores along the fiber axis, and additionally, the weaker and short striae on the meridian in SAXS patterns was due to the orientation and length of micropore in Lyocell fibers (Crawshaw et al. 2000). Based on the quantitative analysis of the two-dimensional SAXS scattering pattern, the micropore parameters of Lyocell fibers were calculated (The Guinier plot and Ruland plot of Lyocell fibers spun at different draw ratio were shown in supporting information (Fig. S4 and Fig. S5)), including micropore diameter, micropores length and micropore orientation deviation angle as shown in Fig. 8. It can be seen that the micropore in Lyocell fibers showed multi-level characteristics. The size of micropore decreased with draw ratio increasing, especially the larger micropore. The micropore length increased gradually while the orientation deviation angle of micropore decreased with draw ratio increasing especially at excessive drawing stage, indicating that the micropore get much longer and slenderer under drawing.



291

292

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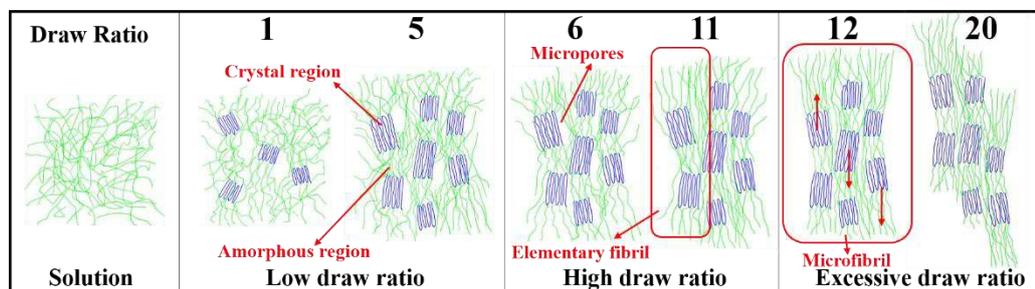
Fig. 9 The effect of draw ratios on fibrillation of Lyocell fibers

Table. 1 The effect of draw ratios on the average fibril length of Lyocell fiber

Low draw ratios	Draw ratios	1	2	3	4	5
	Average fibril length/µm		0	0	0	3.9

High draw ratios	Draw ratios	6	7	8	9	10	11			
	Average fibril length/ μm	7.8	9.1	10.1	10.6	11.3	11.5			
Excessive draw ratios	Draw ratios	12	13	14	15	16	17	18	19	20
	Average fibril length/ μm	12.4	12.8	12.9	20.0	22.5	22.8	24.6	31.3	34.3

295



296

297 Fig.10 Schematic diagram to depict the evolution of Lyocell fiber microstructure with different
298 draw ratios
299

300 The fibrillation of Lyocell fiber samples at different draw ratios was measured by radiated
301 strong sonic wave on the fiber surface for 30min, the fibrillation and the average fibril length of
302 Lyocell fiber was shown in Fig. 9 and Tab.1 respectively. In order to intuitively describe the
303 differences in structure as well as the structural evolution of Lyocell fiber at different draw ratio,
304 an appropriate structural model based on all the above tests was proposed, as shown in Fig. 10.

305 It can be seen that there was no obvious fibril on the fiber surface at low drawing stage due to
306 the amorphous region with low degree of orientation increase the binding force of the elementary
307 fibril. The increase of crystallinity and orientation lead to the increase of the breaking strength,
308 modulus and yield strength of the fiber with the drawing ratio at low drawing stage.

309 At high drawing stage, the fibers form a highly crystalline and oriented structure, leading to
310 the formation of microfibrils. Meanwhile, the length of the microfibrils increase is due to the raise
311 of the amorphous orientation, which leads to the lengthening of the elementary fibrils as shown in
312 Fig. 10, it can also be reflected by the variation of micropore structure. And the increase of the
313 breaking strength, modulus and yield strength of the fiber with the drawing ratio at high drawing
314 stage is mainly owing to the increase of amorphous orientation.

315 Moreover, it can be seen from Tab. 1 that the fibril length also increased with draw ratio
316 especially when the draw ratio was above 15. Both of crystallinity and orientation of the fiber
317 remained unchanged with draw ratio increase at excessive drawing stage while the length of
318 micropores and microfibrils increase. This seems to be a contradictory problem, but the fact is the
319 elementary fibrils slip due to weak interaction forces, which leads to the increase of the length of
320 micropores and microfibrils as shown in Fig. 10. The structure of highly crystallized and oriented
321 elementary fibrils keeps the breaking strength constant, but the slip of elementary fibrils leads to
322 the decrease of modulus and yield strength.

323 Conclusions

324 Summarizing the changes of mechanical properties and structure of Lyocell fiber with
325 different draw ratio, it can be concluded that, at low drawing stage, the increase of the breaking

326 strength, modulus and yield strength attributed to the raise of crystallinity and orientation, and the
327 raise of crystallinity is mainly due to the increase of crystal region and crystal size perpendicular to
328 the (002) crystal plane; at high drawing stage, the mainly reason for the breaking strength,
329 modulus and yield strength increasing was the improvement of amorphous orientation; and at
330 excessive drawing stage, the highly crystallized and oriented structure kept the breaking strength
331 constant, while the decrease of modulus and yield strength was due to the elementary fibrils
332 slipping caused by weak interaction. Therefore, the above structural defects limited the increase of
333 fiber strength with the increase of draw ratio, in other words, there is a limitation to improve the
334 mechanical properties by increasing the draw ratio in the current production process of
335 Lyocell fiber, this suggests that further improvements must be made in the processing of
336 Lyocell fibers.

337 **Declaration**

338 **Conflict of interest**

339 The author states that there are no competing economic interests.

340 **Ethical approval**

341 This paper does not cover studies of human participants or animals by all the authors.

342 **Acknowledgements**

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344 help of Shanghai Synchrotron Radiation Facility (SSRF).

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