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## Research Article

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# Improved mechanical strength, proton conductivity and power density in an ‘all-protonic’ ceramic fuel cell at intermediate temperature

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Protonic ceramic fuel cells (PCFCs) have become the most efficient, clean and cost-effective electrochemical energy conversion devices in recent years. While significant progress has been made in developing proton conducting electrolyte materials, mechanical strength and durability still need to be improved for efficient applications. We report that adding 5 mol% Zn to the Y-doped barium cerate-zirconate perovskite electrolyte material can significantly improve the sintering properties, mechanical strength, durability and performance. Using same proton conducting material in anodes, electrolytes and cathodes to make a strong structural backbone shows clear advantages in mechanical strength over other arrangements with different materials. Rietveld analysis of the X-ray and neutron diffraction data of  $\text{BaCe}_{0.7}\text{Zr}_{0.1}\text{Y}_{0.15}\text{Zn}_{0.05}\text{O}_{3-\delta}$  (BCZYZn05) revealed a pure orthorhombic structure belonging to the *Pbnm* space group. Structural and electrochemical analyses indicate highly dense and high proton

1 **conductivity at intermediate temperature (400-700 °C). The anode-supported single cell,**  
2 **NiO-BCZYZn05 | BCZYZn05 | BSCF-BCZYZn05, demonstrates a peak power density**  
3 **of 872 mW cm<sup>-2</sup> at 700 °C which is one of the highest power density in an all-protonic**  
4 **solid oxide fuel cell. This observation represents an important step towards**  
5 **commercially viable SOFC technology.**

6

7 As the standard technologies based on fossil fuels cannot satisfy the growing demand for  
8 energy, the future lies in the implementation of efficient and environmentally friendly  
9 technologies to produce electricity, such as hydrogen energy and fuel cells<sup>1-3</sup>. During the past  
10 few decades, fuel cells, especially solid oxide fuel cells (SOFCs), have attracted significant  
11 attention due to their high efficiency, low pollution and low environmental impact at high  
12 working temperatures (700 – 1000°C)<sup>4</sup>. YSZ is a state-of-the-art electrolyte because it  
13 possesses adequate oxide-ion conductivity (~0.13 Scm<sup>-1</sup> at 1000°C) and shows desirable  
14 phase stability in both oxidizing and reducing atmospheres<sup>5</sup>. However, its high operating  
15 temperature leads to high system costs, cell degradation, low material compatibility and  
16 dissatisfactory durability<sup>6,7</sup>. To reduce and overcome these problems, protonic ceramic fuel  
17 cells (PCFCs) have been introduced. PCFCs operate in an intermediate temperature (IT)  
18 range (400 – 700°C) due to the higher mobility of proton ions than oxygen ions<sup>8-12</sup>. Duan et  
19 al. recently proved that PCFCs can be efficiently used as reversible protonic ceramic  
20 electrochemical cells (RePCECs)<sup>13</sup>. Fop et al. observed both oxide ion and proton  
21 conductivity in disordered hexagonal perovskites<sup>14</sup>. Over the last few decades, numerous  
22 materials, especially electrolyte materials, have been explored to obtain better performance  
23 with lower activation energies in IT range fuel cell applications<sup>15-22</sup>. Recently, Sossina et al.  
24 proved that pulsed laser-deposited PrBa<sub>0.5</sub>Sr<sub>0.5</sub>Co<sub>1.5</sub>Fe<sub>0.5</sub>O<sub>5+δ</sub> cathodes show very good  
25 performance and long-term stability with a PCFC electrolyte<sup>23</sup>.

1 Due to the highly resistive nature of its grain boundaries, BaZrO<sub>3</sub> has a lower conductivity  
2 but higher chemical and thermal stability under both H<sub>2</sub>O and CO<sub>2</sub> than BaCeO<sub>3</sub>. However,  
3 BaCeO<sub>3</sub>-BaZrO<sub>3</sub> doped with yttrium along with different Ce and Zr contents exhibits high  
4 conductivity with good chemical stability and high cell performance<sup>24-27</sup>. Using ZnO as a  
5 sintering additive allows a reduction in the high sintering temperature and remarkable  
6 improvement in the density, conductivity and stability<sup>28-31</sup>.

7 A recent review from Irvine et al. discussed the processes occurring at the interface and ways  
8 to control the structure at the nanoscale for high performance and durability in solid oxide  
9 cells (SOCs)<sup>32</sup>. The high operating temperature of SOCs gives significant constraints for  
10 material selection of electrodes, electrolytes and interconnects. All materials should be  
11 nonreactive and have a matching thermal expansion coefficient. Electrodes must be redox  
12 stable and porous and have mixed ionic and electronic conductors; electrolytes and  
13 interconnects must be gas impermeable and redox stable. An ideal microstructure is crucial to  
14 optimise contacts between the electrolyte and the electrodes to be mechanically, chemically,  
15 dimensionally and thermally stable during operation. Durability depends on the ability to  
16 withstand pressure or damage, which is also highly dependent on the hardness or elastic  
17 modulus of the fuel cell. Duan et al.<sup>33</sup> showed the long-term durability and fuel flexibility of  
18 protonic ceramic fuel cells. This highlights the potential of the technology for commercial  
19 applications but without observing the mechanical properties of the fuel cells themselves.  
20 Another very interesting and important property of PCFCs is that they do not suffer fuel  
21 dilution in the way oxide ions conducting SOFCs do since water forms on the cathode side.  
22 Since the fuel dilution on the anode side does not decrease the Nernst potential, the PCFC can  
23 maintain a higher operation voltage, particularly for high fuel utilization.

24 The mechanical properties are one of the most important and critical characteristics to be  
25 considered due to the different thermal expansion coefficients of the constituting materials

1 and specific work environments. Nanoindentation/indentation methods are an attractive  
2 approach to determine the hardness and Young's modulus, which has a direct relation with  
3 durability. To determine the hardness and elastic modulus, Oliver Pharr analysis<sup>34</sup> is  
4 commonly used when  $h_f/h_m$  (final indentation depth/peak load indentation depth) is less than  
5 0.7. When the pile-up effect is observed, the relationship between the hardness and work of  
6 indentation can be written as  $H = \frac{kP_m^3}{9W^2}$ , where P is the maximum load, k is a constant that  
7 depends on the geometry of the indenter, and W is the total work or plastic work.

8 Atomic structural matching is also an important property to consider for ceramic  
9 electrode/electrolyte interface durability and performance. The interface of atoms is dynamic  
10 and evolving in SOC subsystems, which has been proven theoretically and experimentally.  
11 Recent reports demonstrate that this dynamic nature may enhance durability and  
12 performance<sup>32</sup>. To understand and control the independence between interface structure,  
13 functionality, electrochemistry, performance and durability, different approaches were tried.  
14 Octahedral distortions have very close links to functional properties and durability in  
15 perovskite oxides,  $ABO_3$ , which consists of three-dimensional corner-sharing  $BO_6$  octahedra  
16 in the perovskite lattice (Figure 1b). Atomic structural matching improves the mechanical as  
17 well as electrochemical properties for intermediate- and high-temperature applications but  
18 has been omitted in most of the experimental, theoretical and review work carried out  
19 previously. Aso et al.<sup>35</sup> discussed the effect of octahedral distortions in the heterointerface of  
20 perovskite oxides on the atomic level. The oxygen arrangements around the heterointerface,  
21 due to the octahedral mismatch, play a critical role in epitaxial strain accommodation in  
22 perovskite heterostructures. The matching thermal expansion coefficient among the  
23 anode/electrolyte/cathode is also extremely important for fuel cell durability. It can maximize  
24 the use of the same material due to their structural, thermal and behavioural similarity.

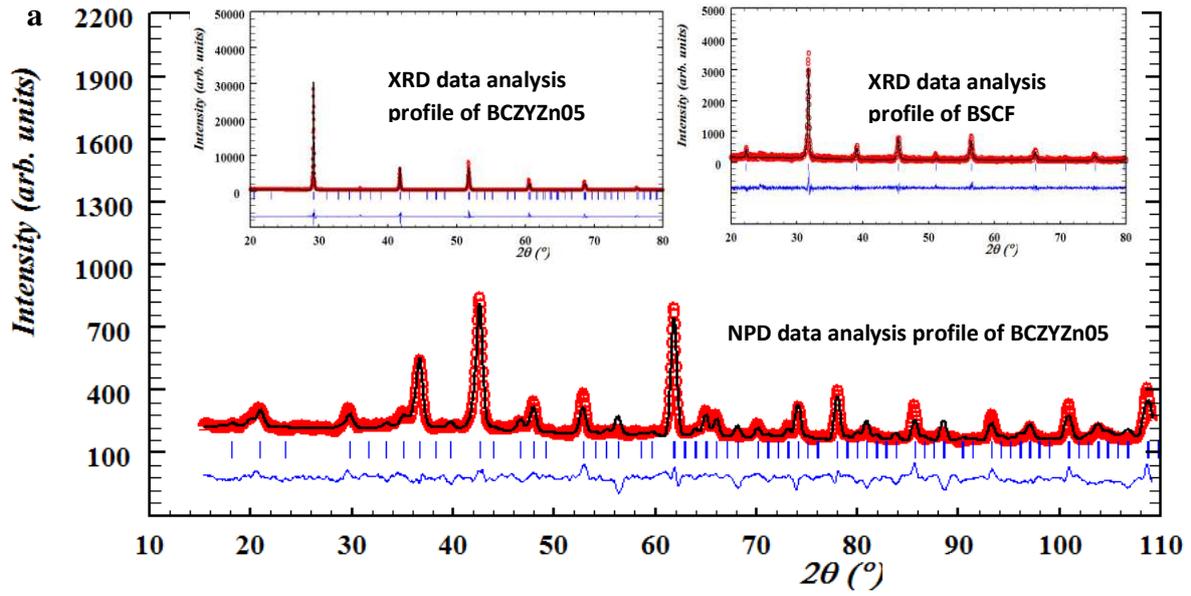
1 We explored the orthorhombic perovskite  $\text{BaCe}_{0.7}\text{Zr}_{0.1}\text{Y}_{0.15}\text{Zn}_{0.05}\text{O}_{3-\delta}$  (BCZYZn05) electrolyte,  
2 which exhibits a high power density with high conductivity and better mechanical properties  
3 when BCZYZn05 was used in all parts of the ceramic cell (anode|electrolyte|cathode).  
4  $\text{Ba}_{0.5}\text{Sr}_{0.5}\text{Co}_{0.8}\text{Fe}_{0.2}\text{O}_3$  (BSCF) cathode material<sup>6</sup> was mixed with BCZYZn05 in a 3:2 weight  
5 percent to obtain high performance and durability. A single-cell NiO-BCZYZn05 |  
6 BCZYZn05 | BSCF-BCZYZn05 displays a power density of  $872 \text{ mW cm}^{-2}$  at  $700^\circ\text{C}$  with the  
7 addition of an anode functional layer (AFL) using the drop-coating electrolyte deposition  
8 method. The performance may be further improved by controlling the preparation process  
9 and microstructure of the electrodes. Our results prove that using a single structured material  
10 in the anode, electrolyte and cathode to create a strong backbone of the cell is beneficial to  
11 improve the mechanical strength as well as performance and durability.

12

## 13 **Results and Discussion**

14 A single-phase material with nominal composition  $\text{BaCe}_{0.7}\text{Zr}_{0.1}\text{Y}_{0.15}\text{Zn}_{0.05}\text{O}_{3-\delta}$  was obtained  
15 by solid-state reaction at  $1400^\circ\text{C}$  for 10 h (supplementary information 2.1). The  
16 electrochemical impedance of a dense (~98% of the theoretical neutron diffraction density)  
17  $\text{BaCe}_{0.7}\text{Zr}_{0.1}\text{Y}_{0.15}\text{Zn}_{0.05}\text{O}_{3-\delta}$  pellet was measured at room temperature in air.  
18 Rietveld refinement of the neutron diffraction data of the perovskite-type ceramic powder  
19 BCZYZn05 shows a well-formed orthorhombic structure in the *Pbnm* space group. The unit  
20 cell parameters were found to be  $a = 6.099(2) \text{ \AA}$ ,  $b = 6.091(2) \text{ \AA}$  and  $c = 8.611(2) \text{ \AA}$ . Neutron  
21 powder diffraction (NPD) is a powerful technique that is used for its ability to detect light  
22 molecular weight elements such as hydrogen and oxygen, which shows additional peaks  
23 and, consequently, changes to the crystalline system. Determination of accurate oxygen  
24 position is crucial to find the octahedral tilting in the perovskite structure.  $\text{BO}_6$  octahedral

1 tilting is common and is important not only for structural stability but also for its relation  
 2 with physical properties ranging from ionic conductivity, electronic and magnetic  
 3 properties, and metal-insulator transitions to improper ferroelectricity. Static and/or  
 4 dynamic Jahn-Teller distortion of BO<sub>6</sub> octahedra arises when two axial atomic bonds are  
 5 shorter or longer than those of the equatorial bonds. The distortion affects the electrical,  
 6 physical and mechanical properties. The difference in the neutron powder diffraction  
 7 (NPD) pattern and X-ray powder diffraction (XRPD) pattern can be realized from Fig. 1a.  
 8 NPD shows more Bragg reflections with good intensity due to the sensitivity for oxygen  
 9 positions. As shown in Fig. 1b, BCZYZn05 crystallizes in an orthorhombic crystal  
 10 structure with a *Pbnm* space group ( $\sqrt{2}a_p \times \sqrt{2}a_p \times 2a_p$ ) that shows in-phase octahedral  
 11 rotation around the [001]<sub>po</sub> axis and out-of-phase rotation around the [1-10]<sub>po</sub> axis, which  
 12 can be described as  $a^-a^-c^+$  in the Glazer notation<sup>36</sup>. Therefore, the 3D images projected  
 13 along the [001]<sub>po</sub> direction are suitable to investigate octahedral distortions in the  
 14 BSCF/BCZYZn05 (cubic/orthorhombic) heterostructure. In cubic *Pm-3m*, the rotations in  
 15 all three directions are the same and can be described as  $a^0a^0c^0$  in Glazer notation (as  
 16 shown in Fig. 1c). The rotations in *po* (perovskite orthorhombic) and *pc* (perovskite cubic)  
 17 are related as [001]<sub>pc</sub> → [001]<sub>po</sub>, [010]<sub>pc</sub> → [110]<sub>po</sub> and [100]<sub>pc</sub> → [1-10]<sub>po</sub>. This is because  
 18 of the large difference in the lattice parameters (BSCF;  $a_{pc} = 3.99 \text{ \AA}$ , BCZYZn05;  $a_{po} =$   
 19  $6.12 \text{ \AA}$ ) as well as oxygen octahedral tilt angle  $\theta$ , where  $\theta_{BSCF} = 180^\circ$ ,  $\theta_{BCZYZn05} =$   
 20  $175.130(9)^\circ$  for B-O1-B and  $160.24(9)^\circ$  for B-O2-B. The atomic interface heterostructure  
 21 explains how the structural distortions arise from structural mismatch, which is not only  
 22 the effect of lattice parameters but also octahedral tilting. A small percentage of electrolyte  
 23 material mixed with the cathode/anode can increase the strength of the structural backbone  
 24 of the cell and thus increase the durability (Fig. 1d). A schematic diagram of a proton  
 25 conducting SOFC is given in Fig. 1e to show the proton and electron migration path.



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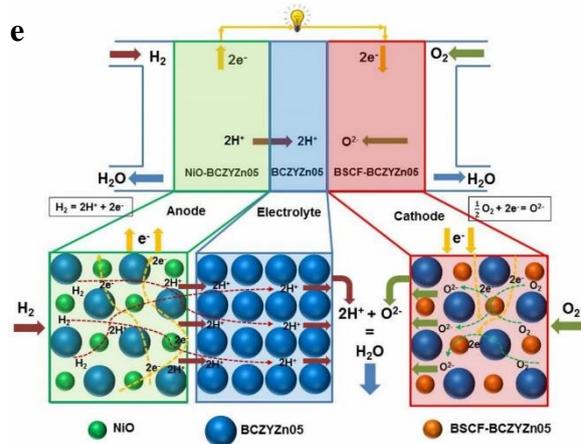
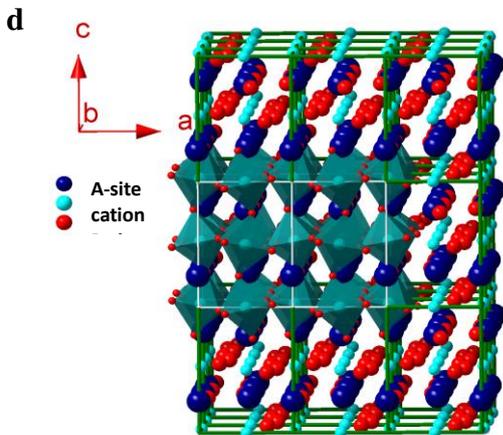
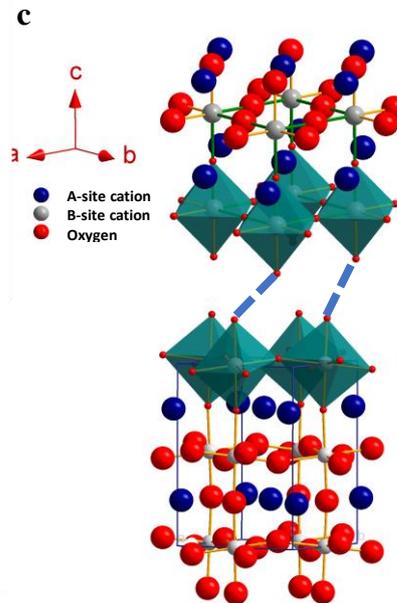
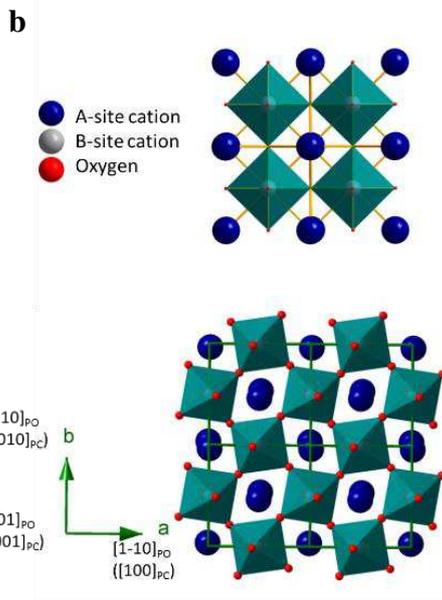
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1 **Figure 1 | Crystal structure determination and atomic arrangements.** **a**, Rietveld refinement of the  
2 neutron diffraction data of BCZYZn05 polycrystalline ceramic powder in orthorhombic symmetry in  
3 the  $Pbnm$  space group. The unit cell parameters are related to the ideal primitive cubic perovskite cell  
4 as  $a \approx \sqrt{2}a_p$ ,  $b \approx \sqrt{2}a_p$  and  $c \approx 2a_p$  ( $a_p \approx 3.96 \text{ \AA}$  is the unit cell parameter of ideal primitive perovskite).  
5 X-ray diffraction data refinement is shown in the insert for BCZYZn05 (left) and BSCF (right). **b**, c-  
6 axis view of cubic (space group  $Pm-3m$ ) BSCF cathode and orthorhombic BCZYZn05 electrolyte. In  
7 Glazer's notation, the rotation of oxygen octahedra in this cubic and orthorhombic space group can be  
8 described as  $a^0a^0a^0$  and  $a^-a^+c^+$ , respectively. In the orthorhombic case, the rotation is in-phase around  
9 the  $[001]_{po}$  axis and out-of-phase around the  $[1-10]_{po}$  axis, which indicates that the octahedral distortion  
10 in the BCZYZn05 structure will be visual along the  $[001]_{po}$  direction. **c**, The dotted line represents the  
11 mismatch between the cubic and pseudocubic (orthorhombic) structures. **d**, When the same material  
12 was used in the cathode|electrolyte|anode, no shifts of the oxygen atoms in the interface occurred, and  
13 the arrangement created a strong structural backbone for solid oxide fuel cells. **e**, Schematic diagram of  
14 the all-protonic cell, which shows the proton conducting path and formation of water at the cathode  
15 side.

16

17 High density and high ionic conductivity are two of the most important criteria for a good  
18 electrolyte. A small percentage of Zn doping at the B-site<sup>37</sup> or adding a sintering additive<sup>38</sup>  
19 increases the density and performance of the electrolyte. Zn doping has advantages over Ni  
20 for better sintering, crystal structure and density. Ni doping suffers from unexpected  
21 electronic conduction in electrolytes with low OCVs, which might be due to electronic  
22 leakage related to the low transport number, fuel efficiency and power density<sup>39</sup>. The cross-  
23 sectional SEM image of NiO-BCZYZn05 | BCZYZn05 | BSCF-BCZYZn05 (see Fig. 2a)  
24 shows the density profile of the different parts of the cell. NiO-BCZYZn05 (60:40 wt.%)  
25 anode-supported cells with the BCZYZn05 electrolyte and BSCF-BCZYZn05 cathode clearly  
26 show that the electrolyte was highly dense to stop gas crossover. The AFL was deposited  
27 between the NiO-BCZYZn05 anode support and BCZYZn05 electrolyte to reduce the  
28 difference in the shrinkage rate of both layers. The as-prepared AS shows a uniform porous  
29 structure with micro- and macropores. No delamination behaviour was found between the

1 anode and electrolyte, indicating the good wettability of the anode and electrolyte. The  
2 BSCF-BCZYZn05 composite cathode also shows uniform micropores. The interaction  
3 phenomenon between the electrolyte and cathode was excellent after sintering at 1000°C for  
4 2 h. The electrolyte thickness was 26.6  $\mu\text{m}$ . To determine the density, phase and any  
5 impurities of the electrolyte materials, SEM was performed on the BCZYZn05 pellet sintered  
6 at 1400°C for 10 h in air (supplementary document Fig. 2 a-b). A cross-sectional image of the  
7 high-density electrolyte pellet is shown in Fig. 2b. No appreciable traces of impurities were  
8 discovered on the pellet surface or the cross-sectional area, which agrees with the XRD and  
9 NPD results. The relative density of BCZYZn05 was 98% (supplementary document, Table  
10 1) and was calculated via the Archimedes method and neutron diffraction results. The  
11 average grain size of the sample was 4.7  $\mu\text{m}$ .

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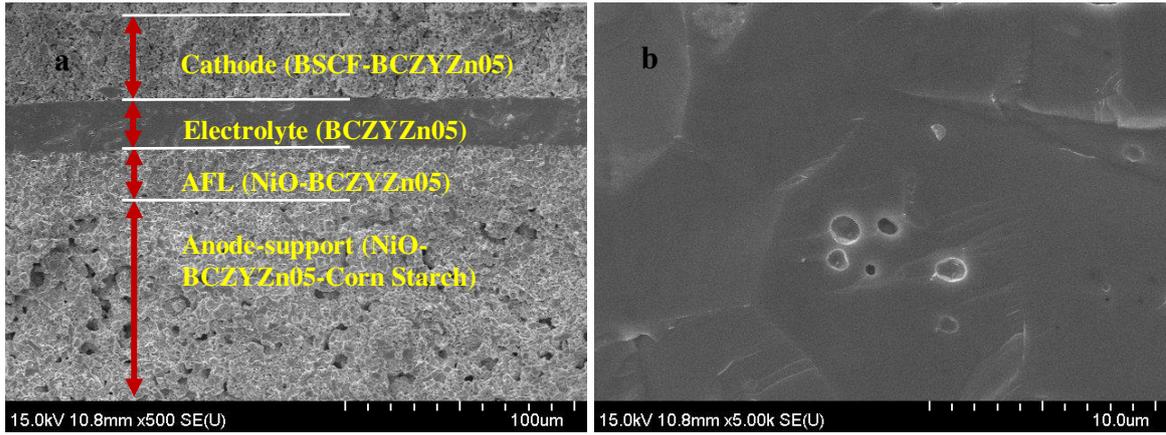
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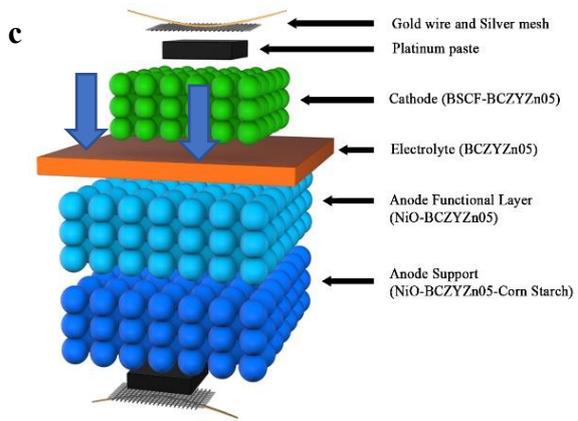
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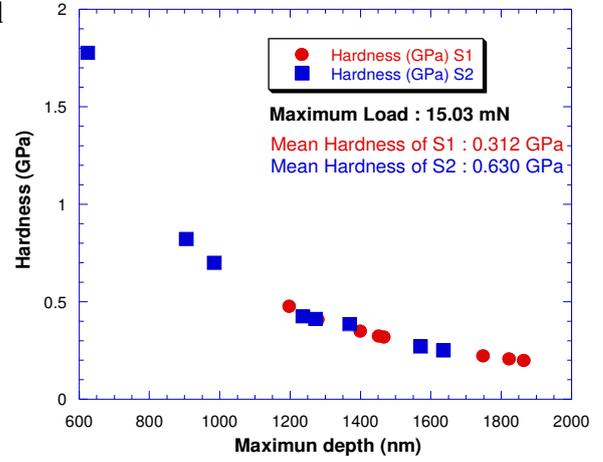
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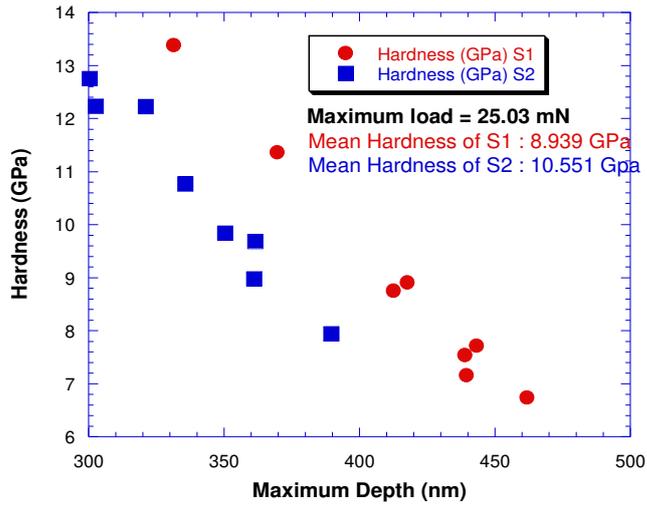
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1 **Figure 2 | SEM analysis and hardness test.** **a**, Cross-sectional image of the single cell  
 2 indicating the porosity difference in the anode and cathode and electrolyte. The electrolyte is  
 3 the densest part of the cell and is approximately 26  $\mu\text{m}$  thick. **b**, Cross-section of the electrolyte  
 4 to observe the grain size and boundaries. **c**, Schematic diagram of nanoindentation on the cathode  
 5 and electrolyte surface. Due to the higher density, the electrolyte is the hardest part of the cell. **d**,  
 6 Comparison of the hardness of the cathode between two cells without mixing electrolyte  
 7 (BSCF) and with mixing electrolyte (BSCF (60%) + BCZYZn05 (40%)). **e**, Comparison of  
 8 hardness between two electrolytes:  $\text{Ba}_{0.9}\text{Sr}_{0.1}\text{Ce}_{0.5}\text{Zr}_{0.35}\text{Y}_{0.1}\text{Sm}_{0.05}\text{O}_{3.8}$ <sup>40</sup> and BCZYZn05.  
 9

10 The hardness of the cell can be calculated using the Oliver Pharr method<sup>34</sup>, which has the  
 11 formula  $H = \frac{P_m}{24.56 h_c^2}$ , where  $P_m$  is the maximum load and  $h_c$  is the contact depth for a  
 12 triangular pyramidal indenter with an identical depth-to-area relationship. Taking into  
 13 account the fact that elastic displacement occurs in both specimen  $E$  and Poisson's ratio  $\nu$  and  
 14 the indenter with elastic constants  $E_i$  and  $\nu_i$ , the reduced modulus  $E_r$  can be calculated by the  
 15 following equation:

$$16 \quad \frac{1}{E_r} = \frac{(1-\nu^2)}{E} + \frac{(1-\nu_i^2)}{E_i} \quad (1)$$

17 Figure 2c shows the schematic atomic diagram of the cell and indentation points. The nanoindentation  
 18 using a 15.03 mN load on 8 different points in the cathode surface shows that the mean hardness of  
 19 the electrolyte mixed cathode (BSCF + BCZYZn05) was 101.92% higher than that without the  
 20 electrolyte mixed cathode (BSCF). The mean hardness of the BSCF + BCZYZn05 and BSCF  
 21 cathodes was 0.63 GPa and 0.312 GPa, respectively (supplementary document Tables 3 and 5). The  
 22 maximum indentation depths were found to be 1635.2 nm and 1865.4 nm in the BSCF + BCZYZn05  
 23 and BSCF cathodes, respectively. Since the thickness of the cathode layers was more than 50,000 nm,  
 24 the measured hardness effect was solely from the cathode and not from the cathode/electrode  
 25 interface. The maximum indentation depth versus hardness of the two cathodes is compared in Fig.  
 26 2d. For the electrolytes, the hardness of BCZYZn05 was compared with a similarly dense electrolyte,  
 27  $\text{Ba}_{0.9}\text{Sr}_{0.1}\text{Ce}_{0.5}\text{Zr}_{0.35}\text{Y}_{0.1}\text{Sm}_{0.05}\text{O}_{3.8}$  (BSCZYSm)<sup>40</sup>. The mean hardness of BCZYZn05 was  
 28 approximately 18.033% higher than that of BSCZYSm (Fig. 2e). The maximum indentation depths

1 using a 25.03 mN load on the electrolyte were 389.6 nm and 443.3 nm for BCZYZn05 and  
 2 BSCZYSm, respectively (the thickness of the electrolytes was more than 25,000 nm). These results  
 3 also prove that the electrolytes are much harder than the cathodes. Due to the different distances  
 4 between test points and the interface, the energetic quantities have no linear relationships among the 8  
 5 test points.

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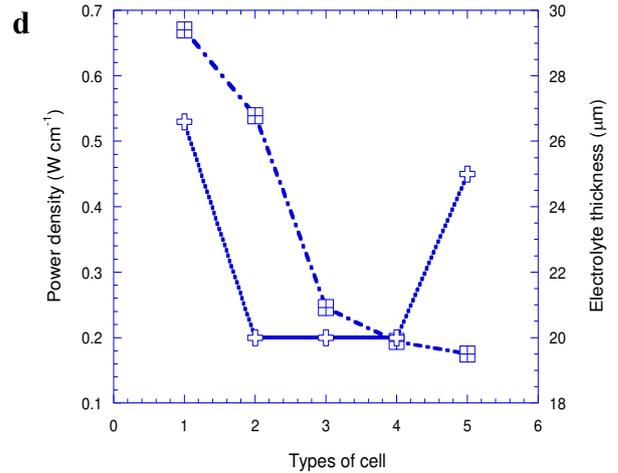
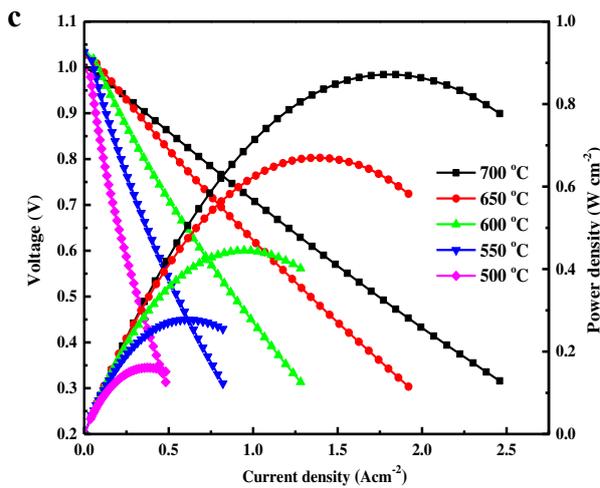
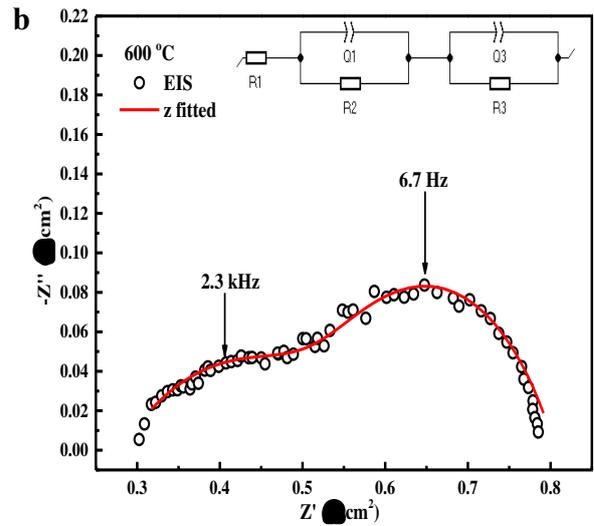
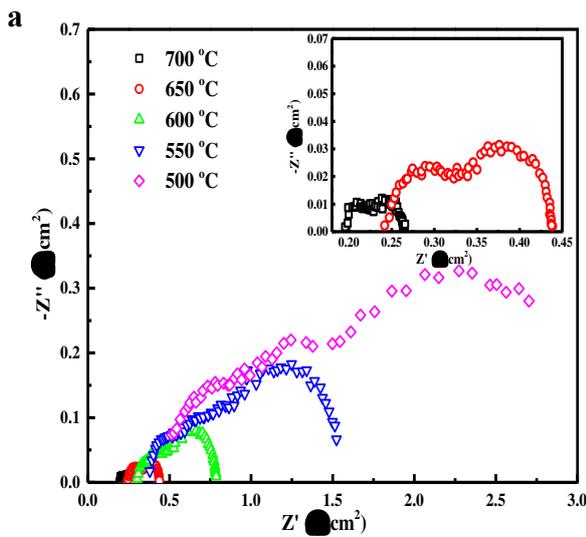
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1 **Figure 3 | Electrochemical properties of NiO-BCZYZn05 | BCZYZn05 | BSCF-**  
2 **BCZYZn05 single cells. a,** Electrochemical impedance spectra collected at 500 ~ 700 °C in  
3 50 °C intervals. **b,** Fitted Nyquist impedance plot at 600°C, which shows two semicircles; the  
4 equivalent circuit is shown in the insert. **c,** *I-V* and power-density curves of the BCZYZn05-  
5 based fuel cell using humidified H<sub>2</sub> (3% H<sub>2</sub>O) as the fuel and ambient air as the oxidant for the  
6 cathode at 500 ~ 700°C. **d,** Comparison of power density and thickness of 4 similar proton  
7 conducting cells with the cell under study. The cells, electrolyte fabrication process and  
8 measured temperatures were as follows: 1. NiO-BCZYZn05 | BCZYZn05 | BSCF-BCZYZn05,  
9 drop coating, 650 °C (present study), 2. NiO-BCZY712 | BCZY712 | LSF-BCZY712, co-  
10 pressing, 650 °C<sup>41</sup>, 3. NiO-BZCYZn04 | BZCYZn04 | SSC-BZCYZn04, co-pressing, 600 °C<sup>42</sup>,  
11 4. NiO-BZCYZn04 | BZCYZn04 | PBC-BZCYZn04, co-pressing, 600 °C<sup>43</sup>, 5. NiO-  
12 BZCYZn04 | BZCYZn04 | LSCF-BZCYZn04, tape casting, 600 °C<sup>44</sup>.

13

14 High electrocatalytic activity and ionic and electronic conduction are three essential  
15 functionalities for the electrochemically active region of fuel cell electrodes. These  
16 functionalities are extremely important aside from durability, cell stability, cell integration  
17 and mass transport. To illustrate the good performance of the single cell, electrochemical  
18 impedance spectra of the cell were obtained at various working temperatures. Typical  
19 Nyquist plots at different temperatures are shown in Figure 3a. The high-frequency intercept  
20 on the real axis represents the ohmic resistance ( $R_{ohm}$ ) of the cell, which mainly originates  
21 from the resistance of the electrolyte. The difference between the low-frequency and high-  
22 frequency intercepts with the real axis designates the interfacial polarization resistance ( $R_p$ ),  
23 which is mainly dominated by the electrode materials and microstructures<sup>45</sup>. The area-  
24 specific resistance (ASR) of a single cell was calculated (fitted) from the impedance spectra  
25 using EC lab software with an equivalent circuit model, where  $R_1$  is  $R_{ohm}$  and the sum of  $R_2$   
26 and  $R_3$  is  $R_p$ . Figure 3b presents the fitting profile of the obtained spectra with an equivalent  
27 circuit at 600°C. The obtained frequencies for the first semicircle and second semicircle were  
28 2.3 kHz and 6.7 Hz, respectively. The conductivity values of the single cell were  $2.3 \times 10^{-2}$ ,  
29  $5.17 \times 10^{-2}$ , 0.13, 0.34 and 0.97 Scm<sup>-1</sup> at 500, 550, 600, 650 and 700°C, respectively. The  
30 bulk and total conductivities of the electrolyte material reached  $9.23 \times 10^{-3}$  and  $7.61 \times 10^{-3}$   
31 under wet Ar conditions, where the activation energies were below 0.6 eV. Proton migration

1 in this system was supposed to be the result of the incorporation of water into oxygen  
2 vacancies generated by acceptor doping of the host ceramic material. Protons are introduced  
3 as point defects that become mobile as the temperature increases via the transport  
4 phenomenon known as the Grotthuss mechanism<sup>46</sup>. This low activation energy makes fuel  
5 cells more proton conductive, affordable and practical. The  $R_{ohm}$  values were 0.196, 0.238,  
6 0.269, 0.266 and 0.306  $\Omega\text{cm}^2$  and the  $R_p$  values were 0.07, 0.207, 0.543, 1.405 and 3.427  
7  $\Omega\text{cm}^2$  at 700, 650, 600, 550 and 500°C, respectively. Compared with previous results, both  
8  $R_{ohm}$  and  $R_p$  values are lower than those of many BCZY-based cells<sup>47</sup>. The excellent  
9 performance of the present cell is due to the low cell resistances. The low  $R_{ohm}$  values should  
10 be attributed to the highly dense and thin electrolyte film. Current – voltage – power (IVP)  
11 with area-specific resistance curves of the as-fabricated NiO-BCZYZn05|BCZYZn05|BSCF-  
12 BCZYZn05 single cells with added AFL using 3% humidified  $\text{H}_2$  as the fuel and ambient air  
13 as the oxidant in the temperature range of 500 – 700°C are presented in Figure 3c. The  
14 observed peak power densities were 161, 278, 445, 670 and 872  $\text{mWcm}^{-2}$  at 500, 550, 600,  
15 650 and 700°C, respectively. The cell performance was highly promising in comparison to  
16 similar cell performances, as shown in Fig. 3d (a detailed list of closely related proton  
17 conducting SOFCs is presented in the supplementary file, Table 6). The total performance of  
18 the fuel cell depends not only on the materials but also on many other factors, such as  
19 processing, thickness, gas flow, and current collector. Therefore, it is difficult to understand  
20 from the comparison of different cell arrangements. The coking resistance and sulfur  
21 tolerance and thermal cycling stability are crucially important for fuel cell commercialization,  
22 particularly for applications requiring start/stop capability or for transient or variable loads.  
23 Duan et al. demonstrated and achieved excellent performance, robust and exceptional  
24 durability with direct operation on 11 different fuel streams without any modifications in the  
25 cell composition or architecture, many of which have not previously been studied in a

1 PCFC<sup>33</sup>. Fuel cell performance can vary greatly depending on the processing of the materials  
2 for electrodes and electrolytes and their thickness. Figure 3d also compares the electrolyte  
3 thickness with the performance of 5 similar cells. There is no linear relationship between  
4 electrolyte thickness and performance. Even with a high thickness (26.6  $\mu\text{m}$ ), the BCZYZn05  
5 electrolyte shows better performance than the others. The open circuit voltage (OCV) values  
6 of the cell were 0.998, 1.034, 1.037, 1.027 and 1.0 V at 500, 550, 600, 650 and 700°C,  
7 respectively. This confirms the high density of the electrolyte.

8 In summary, the strategy of adding Zn to Y-doped barium cerate-zirconate was successful in  
9 decreasing the sintering temperature and creating a high-density electrolyte with high proton  
10 conductivity. The BCZYZn05 electrolyte material was investigated for IT-SOFCs in terms of  
11 conductivity, density and performance. XRD and neutron patterns of the electrolyte were measured  
12 and showed a pure phase with an orthorhombic structure. Moreover, an anode-supported single  
13 cell with the configuration NiO-BCZYZn05 | BCZYZn05 | BSCF-BCZYZn05 was fabricated  
14 and obtained a maximum power density of 872  $\text{mWcm}^{-2}$  at 700°C. Although the results  
15 demonstrate that BCZYZn05 is a promising proton-conducting electrolyte for intermediate-  
16 temperature solid oxide fuel cells due to its high output performance, further improvement  
17 can be achieved. This can be done by lowering the  $R_p$  values using better cathode materials  
18 and reducing the electrolyte thickness. Moreover, the high performance combined with good  
19 conductivity demonstrates that the  $\text{BaCe}_{0.7}\text{Zr}_{0.1}\text{Y}_{0.15}\text{Zn}_{0.05}\text{O}_{3-\delta}$ -based cell is a promising IT-  
20 SOFC with good mechanical strength, durability and performance.

21

## 22 **Methods**

23 **Fabrication of the electrolyte.**  $\text{BaCe}_{0.7}\text{Zr}_{0.1}\text{Y}_{0.15}\text{Zn}_{0.05}\text{O}_{3-\delta}$  powders were synthesized via a  
24 solid-state sintering process from  $\text{BaCO}_3$  (99% purity, Merck, Germany),  $\text{CeO}_2$  (99% purity,

1 Aldrich, China), ZrO<sub>2</sub> (99% purity, Sigma-Aldrich, UK), Y<sub>2</sub>O<sub>3</sub> (99.9% purity, Aldrich,  
2 China) and ZnO (99% purity, Merck, Germany). Stoichiometric amounts of selected  
3 materials were ball-milled in ethanol using zirconia balls for 24 h. The ball-milled materials  
4 were dried in an oven and calcined at 650°C for 10 h, cooled down to room temperature (RT)  
5 and subsequently ground and palletized using a 15 mm diameter die under 20 MPa pressure.  
6 The palletized sample was sintered at 1000°C for 10 h and cooled to RT. The pellet was  
7 again ground, repalletized and sintered at 1200°C for 10 h and finally at 1400°C for 10 h. X-  
8 ray powder diffraction showed a pure orthorhombic phase, which was used for cell  
9 performance and other characterization. All heat treatments were carried out in air with a  
10 heating and cooling rate of 5°/min.

11 **Fabrication of the thin anode support and single cell.** Anode support (AS) materials, NiO  
12 (K ceracell, Korea) and BCZYZn05 powders, were mixed (65:35 wt%), ball-milled with 10  
13 wt% corn starch (as a pore-former) in ethanol for 24 h, and then dried in an oven. These  
14 powders were pressed at 20 MPa for 1 min and then sintered at 900°C for 2 h. For the anode  
15 functional layer (AFL) of the cells, NiO- BCZYZn05 powders were ball-milled with  
16 Solsperse (Lubrizol), polyvinylbutyral (PVB, Butvar, B-98), and di-n-butyl phthalate (DBP,  
17 Daejung Chemicals & Metals, 99%). The as-prepared AFL slurries were drop-coated onto the  
18 sintered anode pellet and then fired at 400°C for 2 h. The BCZYZn05 powders were ball-  
19 milled with Solsperse, PVB, and DBP for 48 h. The resultant slurries were drop-coated onto  
20 the presintered anode substrate and then sintered at 1450°C for 4 h. For the cathode materials,  
21 composite cathode inks were fabricated by mixing BSCF and BCZYZn05 in a weight ratio of  
22 3:2 with terpineol using a mortar and pestle. The composite cathode ink was screen printed  
23 onto the composite electrolyte side (i.e., NiO-BCZYZn05 anode substrate | NiO-BCZYZn05  
24 AFL | BCZYZn05 electrolyte | BSCF-BCZYZn05 composite cathode) and then fired at  
25 1000°C for 2 h. For the electrical measurements, platinum (Pt) paste (Heraeus, USA) was

1 coated on both sides of the pellets and dried at 120°C for 30 min in an oven. Au wires were  
2 used as the current collector and attached to the electrode using Pt paste.

3 **X-ray diffraction, neutron diffraction, SEM, EIS, TGA and nanoindentation.** The phase  
4 purity of the material was investigated by X-ray diffraction analysis (XRD, D/MAX 2500,  
5 Rigaku, USA) using Cu-K $\alpha_1$  ( $\lambda = 1.5406 \text{ \AA}$ ) radiation in the  $2\theta$  range from 20 to 80°. Neutron  
6 diffraction data were collected using position-sensitive detectors in a neutron diffractometer  
7 at the Bangladesh Atomic Energy Commission. The neutron diffraction scan covered  $2\theta$   
8 angles between 10° and 110°. The microstructure was measured by field emission scanning  
9 electron microscopy (FE-SEM, S-4700, Hitachi High tech, Japan). The anode and cathode  
10 sides of the single cell were fed H<sub>2</sub> (3 vol% humidification) and dry air, respectively, at a  
11 flow rate of 200 sccm in the temperature range of 500 – 700°C. Gas humidification was  
12 performed by bubbling air through a bottle with deionized water. Current-voltage-power  
13 (IVP) curves were measured using an SOFC test station (NARA Cell Tech Corp., Korea)  
14 using a potentiostat/galvanostat EIS instrument (SP-240, Biologic, Claix, France). The  
15 conductivity was determined by electrochemical impedance spectroscopy (EIS) using a  
16 potentiostat/galvanostat from 6 MHz to 0.1 Hz in the temperature range of 500 – 700°C. An  
17 equivalent circuit model was fitted to the impedance spectra using EC-Lab software  
18 (provided from Biologic) to estimate the conductivity of the components. The weight change  
19 of the proton conductor was examined using the thermogravimetry (TG) technique by  
20 NETZSCH (STA 449F3, Germany). The sample was heated from room temperature to 900°C  
21 at a heating rate of 10°C min<sup>-1</sup> under a N<sub>2</sub> atmosphere.

22 A diamond Berkovich indenter tip was used to determine the hardness and elastic modulus of  
23 the anode-supported SOFC. It has a three-sided pyramidal shape. The Berkovich tip has a  
24 half angle of 65.27 degrees measured from the axis to one of the pyramid sides. Since it has a  
25 sharp and well-defined tip geometry, it is good for measuring the modulus and hardness

1 value. However, the elastic-plastic transition may not be truly clear. The rate of force was  
2 fixed at 1 mN/s for both loading and unloading of the tip. Eight random locations were  
3 selected inside the center part for both samples, and eight random locations were selected in  
4 the outer part for both samples. The indentation points were perpendicular to the cell  
5 interface of the SOFC.

6

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10

11

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## 19 **Author contributions**

20 A.K.A. and A.A. developed the intellectual concept, designed the fuel cell experiments,  
21 analysed the data and led the manuscript writing. N.R., A.M.A., M.S.R. analysed the data,  
22 helped in writing manuscript. S.H. performed neutron diffraction, analysed diffraction data.  
23 A.C.I. performed nanoindentation experiments and analyzed the data. J.Y.P. and A.H.  
24 provided supervisory guidance on the fuel cell experiments and data interpretation. J.Z. and  
25 J.I. provided supervisory guidance and manuscript refinement. All authors reviewed the  
26 manuscript.

27

## 28 **Competing interests**

29 The authors declare no competing financial interests.

# Figures

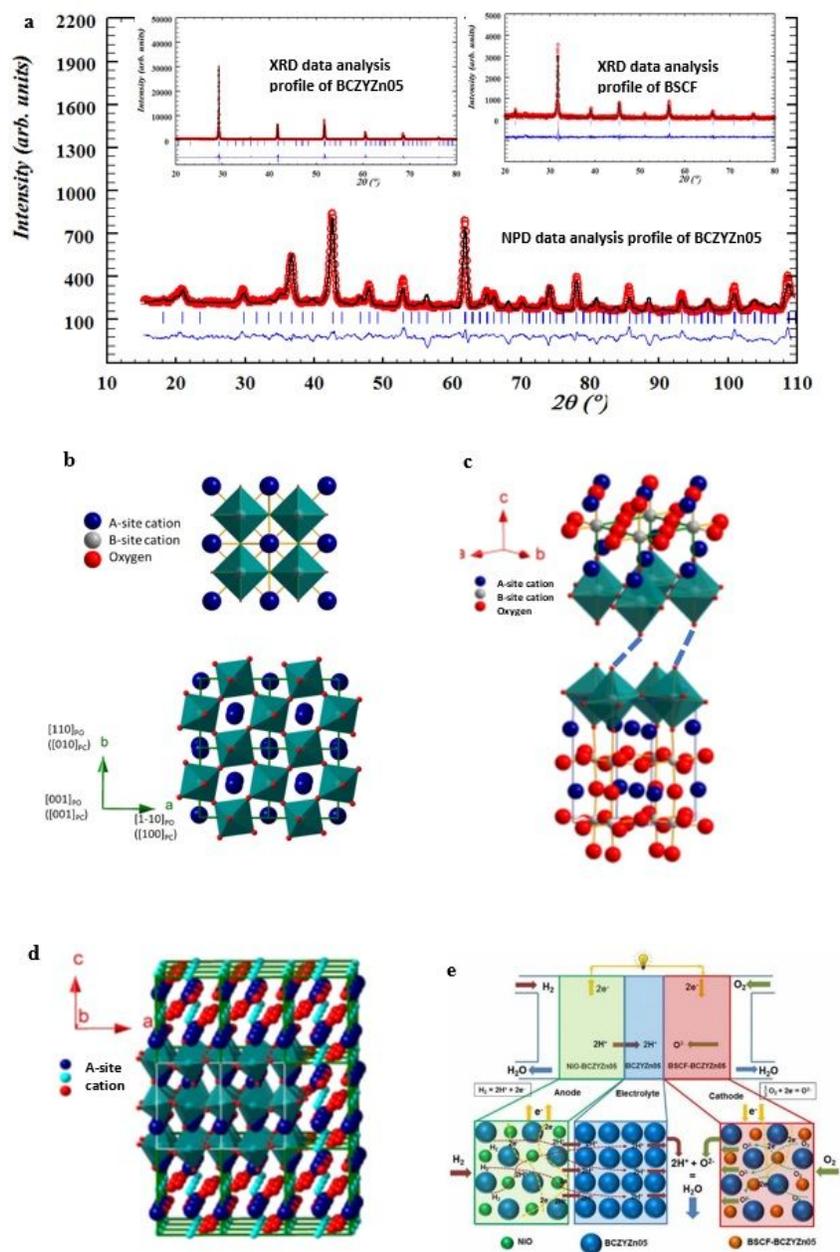


Figure 1

please see the manuscript file for the full caption

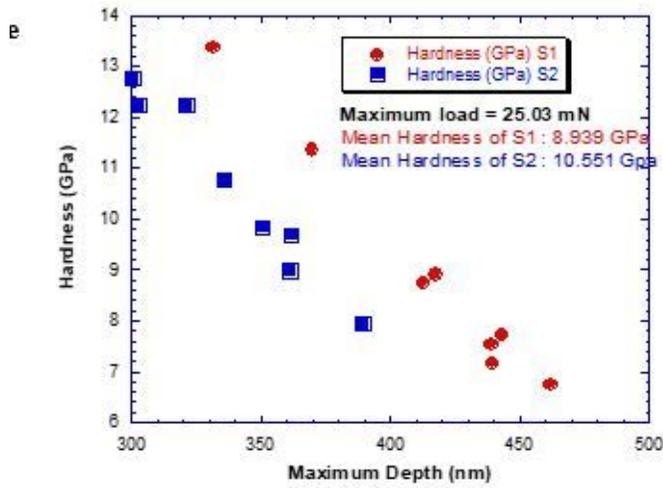
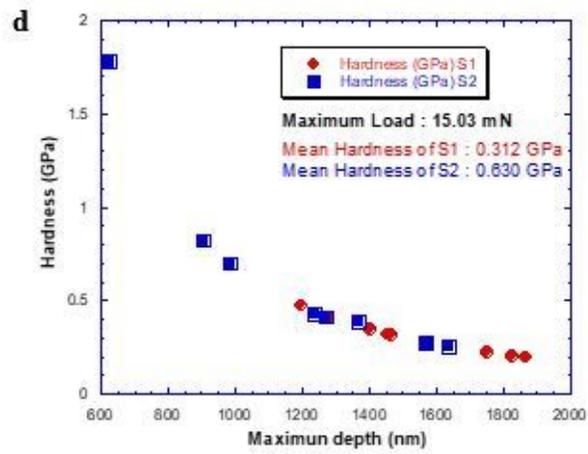
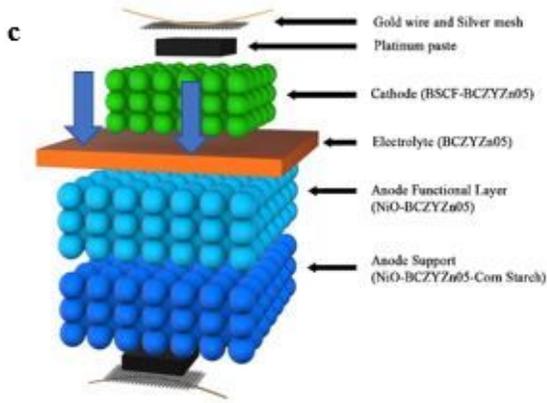
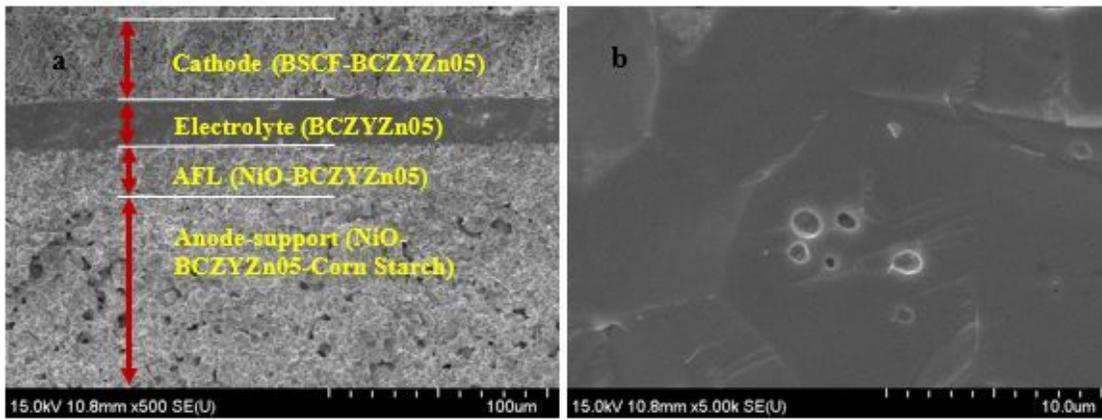
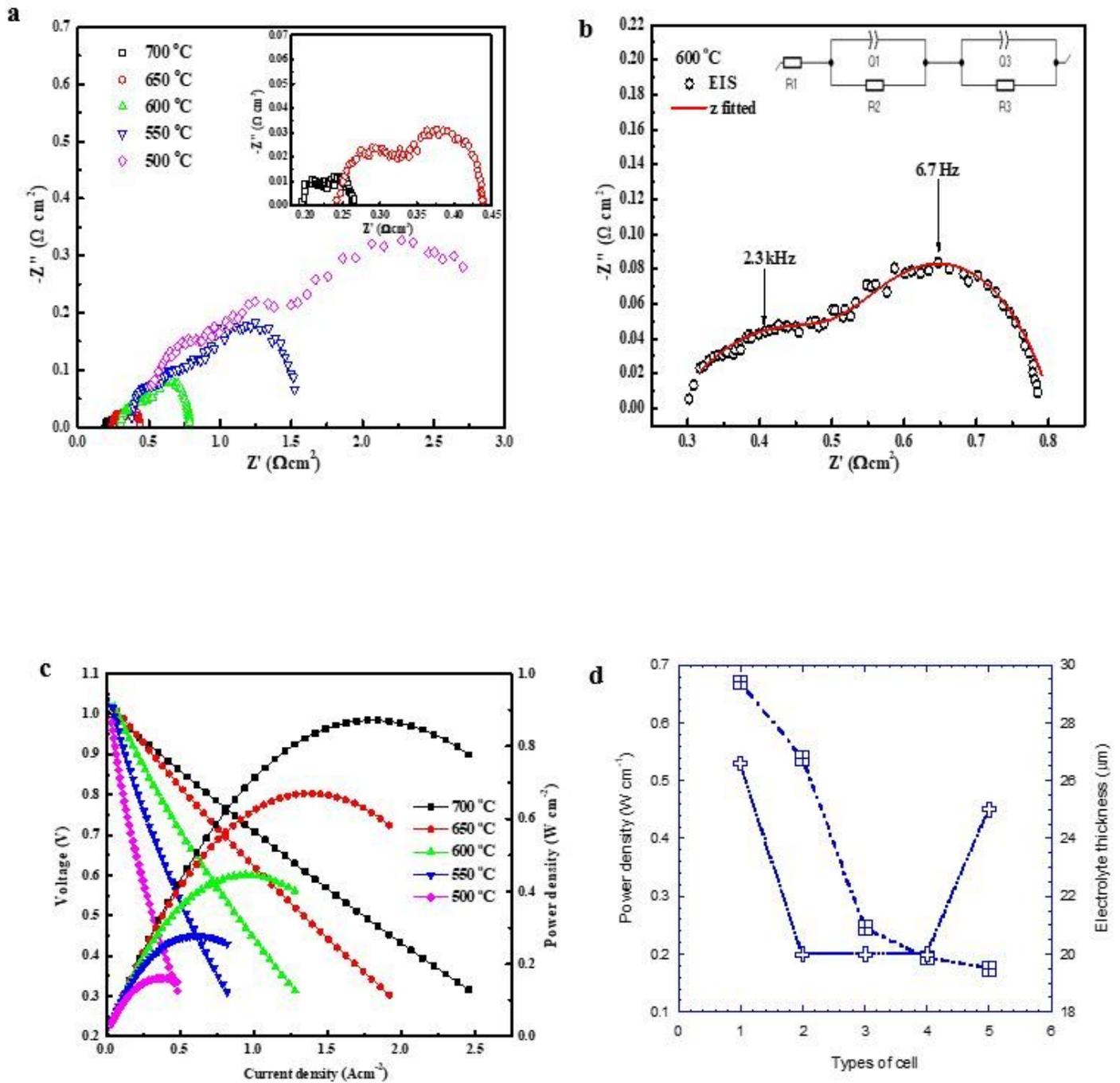


Figure 2

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**Figure 3**

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