

Optimization of parameters applied to degradation and mineralization of p-nitrophenol using advanced oxidative processes

Vanessa Santolin

UFFS: Universidade Federal da Fronteira Sul

Gabriel André Tochetto (✉ tochettogabriel@gmail.com)

UFFS: Universidade Federal da Fronteira Sul <https://orcid.org/0000-0003-1656-505X>

Adriana Dervanoski

UFFS: Universidade Federal da Fronteira Sul

Gean Delise Leal Pasquali

UFFS: Universidade Federal da Fronteira Sul

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1 **Optimization of parameters applied to degradation and mineralization of p-nitrophenol**
2 **using advanced oxidative processes**

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5 *Vanessa Santolin¹, Gabriel André Tochetto^{1,2*}, Adriana Dervanoski¹, Gean Delise Leal Pasquali^{1,3}*

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7
8 ¹Laboratory of Effluent and Waste (LAER), Department of Environmental and Sanitary Engineering (EAS),
9 Federal University of Fronteira Sul (UFFS), 997000-970, Erechim, Rio Grande do Sul, Brazil

10
11 ²Laboratory of Numerical Simulation of Chemical Systems and Mass Transfer (LabSIN-LabMASSA),
12 Department of Chemical and Food Engineering (EQA), Federal University of Santa Catarina (UFSC), 88040-
13 900, Florianópolis, Santa Catarina, Brazil

14
15 ³Post-Graduation Program in Science and Environmental Technology (PPGCTA), Federal University of
16 Fronteira Sul (UFFS), 997000-970, Erechim, Rio Grande do Sul, Brazil

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18 * Corresponding author: Gabriel André Tochetto, e-mail: tochettogabriel@gmail.com, phone: + 55 (54) 99664-
19 0195

20
21 E-mail addresses: Vanessa Santolin (vane.santolin22@gmail.com), Gabriel André Tochetto
22 (tochettogabriel@gmail.com), Adriana Dervanoski (adriana.dervanoski@uffs.edu.br), Gean Delise Leal Pasquali
23 (geandelise@uffs.edu.br)
24

25 Abstract

26

27 Advanced oxidative processes are widely used in the degradation of organic compounds. The degradation and
28 mineralization of the PNF was evaluated by means of an experimental factorial design, using photolysis (UV) and
29 photo-peroxidation (UV/H₂O₂). With the results optimized, degradation kinetics was performed and the
30 experimental data adjusted to mathematical models. In the UV system, it was possible to degrade just over 65%
31 and mineralize 15% over 7 h of reaction; however, with the addition of the oxidizing agent H₂O₂, it was possible
32 to obtain 100% removal of the contaminant, suggesting that there was no formation of intermediate compounds.
33 Kinetics results fitting the first order model and the velocity constants revealed that degradation is extremely faster
34 in the UV/H₂O₂ system ($k_{1,UV/H_2O_2} = 0.0580 \text{ min}^{-1} > k_{1,UV} = 0.0018 \text{ min}^{-1}$).

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36 **Keywords:** Photocatalysis; Photolysis; Photo-peroxidation; Phenolic compounds.

37

38 1. Introduction

39

40 Degradation of the quality of aquatic systems due to the disposal of toxic liquid waste is a significant
41 issue today (Khairy et al. 2020). Organic pollutants in the class of phenolic compounds are found in wastewater
42 because of their extensive use in industry (Liu et al. 2020; Wang et al. 2020). Even in low concentrations, these
43 pollutants present a great risks to health (Xiong et al. 2019; Liang et al. 2020) and ecosystems (Li et al. 2020).
44 Nitrophenols (NFs) are composed of benzene rings with bonds of nitro (-NO) and hydroxyl (-OH) groups, are
45 widely used in the synthesis of dyes, paints, pesticides, herbicides, solvents, in the plastic, leather and
46 pharmaceutical industry (Zhang et al. 2017; Chen et al. 2017; Xiong et al. 2019). NFs and their derivates have
47 high toxicity, carcinogenicity and bioaccumulation (Ibrahim et al. 2019; Wang et al. 2021a), with *p*-nitrophenol
48 (PNF) being listed as a priority pollutant by the United States Environmental Protection Agency (USEPA) (Tugba
49 Saka and Tekintas 2020). In Brazil, the maximum level of phenols allowed is only 0.5 mg L⁻¹ (Brasil 2011).
50 Therefore, it becomes necessary to develop effective methods to degrade NFs and their derivates.

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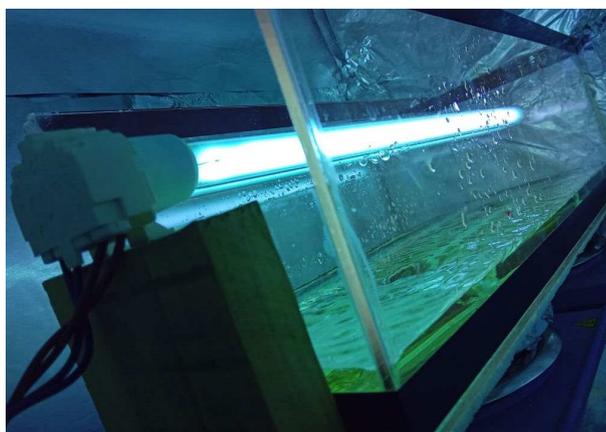
52 Conventional treatments used in industries aren't completely effective in removing NFs (Hu et al. 2020).
53 These technologies are unable to degrade or mineralize complex organic components (Mukherjee et al. 2020) with
54 high mobility and low biodegradability in high concentrations (Hu et al. 2020). In addition, phenol removal
55 processes, which involve sorption and biodegradation, are slow and, in some cases, inefficient (Ren et al. 2017;
56 Zhang et al. 2017; Jiang et al. 2018). Advanced oxidation processes (AOPs) are widely used and promising
57 technologies, as they provide highly active oxidants to remove persistent organic pollutants (Mukherjee et al.
58 2020), such as NFs in aqueous solution (Dewil et al. 2017; Abazari et al. 2019; Wang et al. 2021b). Photocatalytic
59 oxidation is seen as an effective, viable and low-cost treatment to remove pollutants from aqueous solutions (Xiong
60 et al. 2019). Hazardous pollutants can be mineralized under environmental conditions using this technique (García
61 and Hodaifa 2017; Rodrigues et al. 2018; Athanasekou et al. 2018; Fernandes et al. 2019). In the photo-
62 peroxidation process (UV/H₂O₂), two hydroxyl radicals (*OH) are formed when the hydrogen peroxide is exposed
63 to UV light (200-280 nm), by breaking the O₂ bond (Ledakowicz et al. 2019). UV/H₂O₂ has advantages over
64 conventional and biological chemical treatments, mainly due to the easy availability of commercial peroxide, the
thermal stability, and the non-formation of sludge (Yassumoto et al. 2009).

65 The purpose of this study was to evaluate the influence of the main parameters used in the UV and
66 UV/H₂O₂ systems through an experimental planning design to optimize the degradation and mineralization of
67 PNF, while evaluating the kinetics parameters of degradation of the two AOPs.

69 2. Material and methods

71 2.1 Batch photochemical reactor

73 The experimental design tests and kinetics degradation were performed in a rectangular reactor, with
74 dimensions 15 x 45 cm. The reactor was equipped with a UV lamp (36 W, $\lambda = 254$ nm) as a radiation source,
75 positioned in the center of the reactor, 10 cm from the surface of the liquid (Fig. 1). The operation was carried out
76 under ambient conditions of temperature ($25 \pm 3^\circ\text{C}$) and pressure, constant agitation of 150 rpm, and isolated in
77 order to avoid dissipation and irradiation to the external environment.



79
80 **Fig. 1** Photochemical reactor containing UV lamp and PNF solution during the advanced oxidative process.

82 2.2 Experimental design and procedure

84 The experiments were designed with a central composite design (CCD) 2² with 8 tries and 3 repetitions
85 at the central point (Table 1). In the UV-only experiments, the PNF concentration (10-100 mg L⁻¹) and height of
86 the water depth (1.5-3.5) were the variables evaluated, while in UV/H₂O₂, the PNF (10-150 mg L⁻¹) and H₂O₂ (10-
87 100 mg L⁻¹) concentrations were evaluated. For photo-peroxidation, the liquid blade was fixed at 2.5 cm (best UV
88 result). The PNF (C₆H₅NO₃) (99%, Sigma-Aldrich) and hydrogen peroxide (H₂O₂) (30%, Êxodo Científica)
89 solutions used were prepared in deionized water.

91 **Table 1** CCD experimental planning matrix for direct photolysis and UV/H₂O₂ with coded and actual values.

Assay	UV		UV/H ₂ O ₂	
	PNF (mg L ⁻¹)	Water dept (cm)	PNF (mg L ⁻¹)	H ₂ O ₂ (mg L ⁻¹)
1	(-1) 15	(-1) 2	(-1) 15	(-1) 30
2	(-1) 15	(+1) 3	(+1) 50	(-1) 30

3	(+1) 50	(-1) 2	(-1) 15	(+1) 100
4	(+1) 50	(+1) 3	(+1) 50	(+1) 100
5	(0) 30	(-1.41) 1.5	(-1.41) 10	(0) 50
6	(-1.41) 10	(0) 2.5	(0) 30	(-1.41) 10
7	(0) 30	(+1.41) 3.5	(+1.41) 100	(0) 50
8	(+ 1.41) 100	(0) 2.5	(0) 30	(+1.41) 150
9	(0) 30	(0) 2.5	(0) 30	(0) 50
10	(0) 30	(0) 2.5	(0) 30	(0) 50
11	(0) 30	(0) 2.5	(0) 30	(0) 50

92

93

The aqueous PNF solution was added to the reactor together with H₂O₂ (only for UV/H₂O₂). The system was operating for 420 min for UV and 150 min for UV/H₂O₂. The pH, PNF concentration and TOC were determined at the beginning and end of the process. The residual H₂O₂ concentration was also analyzed in the photo-peroxidation system.

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2.3 Analytical methods

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pH assessment was performed with a digital pHmeter (Tecnopon, mPA210), using the potentiometric method (APHA et al. 1999). The PNF concentration of the samples was evaluated by the direct photometric method (Al-Asheh et al. 2004) on a spectrophotometer (Nova Instruments, NI 1600UV) at a wavelength $\lambda = 400$ nm. For evaluation of total organic carbon (TOC) removal, an automatic analyzer was used (Shimadzu, TOC-5000) (APHA et al. 1999). The residual H₂O₂ after reaction was determined by the colorimetric method with MQuant® (Merck) (0 - 100 mg L⁻¹ H₂O₂).

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The experimental data was treated using the Statistica 12.0 (StatSoft, Tulsa, USA) and the results were validated with analysis of variance (ANOVA). The response surface methodology (SRM) obtained an optimization of the advanced oxidation processes, with 95% confidence (p-value < 0.05).

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The degradation of PNF in photolysis and UV/H₂O₂ were evaluated by their fitness to the non-linear mathematical models of first order (FO), pseudo-first order (PSO) and second order (SO) (Eq. 1-3, respectively), using Statistica 12.0 (StatSoft, Tulsa, USA), with 95% confidence (p-value < 0.05).

110

$$C = C_i e^{-k_1 t} \quad (1)$$

111

$$C = C_e + (C_i - C_e) e^{-k_{p1} t} \quad (2)$$

112

113

$$C = C_i \frac{1}{1 + k_2 C_i t} \quad (3)$$

114

where C_i and C_e are the initial and equilibrium concentration of PNF (mg L⁻¹), t is the reaction time (min). The velocity constants k_1 (min⁻¹), k_{p1} (min⁻¹) e k_2 (L mg⁻¹ min⁻¹) refer to the FO, PFO and SO models.

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3. Results and discussion

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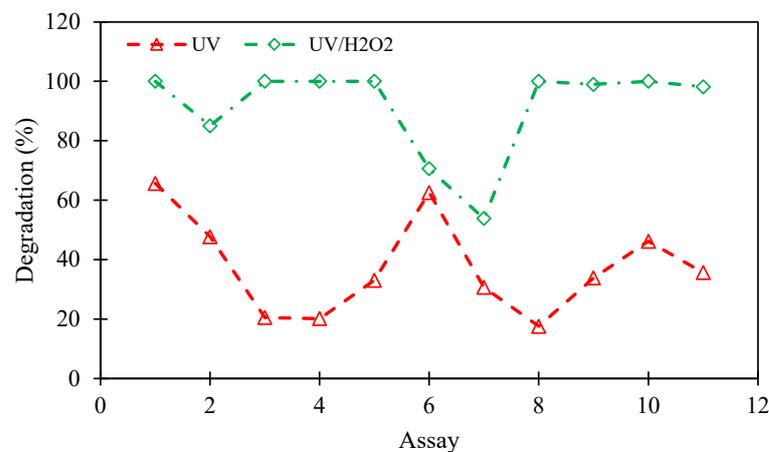
3.1 Optimization of PNF degradation

121

122 The degradation of PNF in the UV and UV/H₂O₂ systems is show in Fig. 2. It is possible to observe that
 123 the best percentage results of PNF degradation occurred in the presence of the oxidizing agent H₂O₂. For the UV
 124 system, the best result occurred in low concentrations of the contaminant (15 mg L⁻¹) and liquid slide of 2 cm,
 125 reaching a degradation of about 65% of the PNF. However, it took 7 hours of operation to achieve this result,
 126 which makes it unfeasible due to the residence time of the batch treatment, as well as the energy consumption,
 127 resulting in an increase in the system's operating cost. The treatment using only UV irradiation is not effective in
 128 the treatment of waste water containing organic compounds, as was also observed in the work of Datta et al. (2004),
 129 since it is a lengthy process and degrades the contaminant at significantly lower rates (Zhao et al. 2010). In the
 130 present study, for a concentration of 10 mg L⁻¹, it took 7 hours of experiment to obtain a degradation of about
 131 63%. This result is similar to that found by Zhao et al. (2010), who needed 12 hours to degrade 75% of the initial
 132 concentration (10 mg L⁻¹).

133 For the UV/H₂O₂ process, the degradation of the contaminant (Fig. 2) reached a value close to 100% in
 134 several tests, presenting values below 85% only in the axial points, where the combination of the conditions is
 135 more extreme (lower H₂O₂ concentration and higher PNF concentration). Ibrahim et al. (2019) studied a
 136 photocatalytic process in the presence of a titanium dioxide (TiO₂) ferrite nanotube to treat 10 mg L⁻¹ of PNF,
 137 obtaining 100% photocatalytic reduction of contaminant in a maximum time of 55 minutes. Think et al. (2020),
 138 after 50 minutes of photocatalytic treatment, reached a maximum yield of 94% when treating 20 mg L⁻¹ of PNF.
 139 These results demonstrate the importance of hydrogen peroxide as an effective, viable and ecologically efficient
 140 method to increase the hydroxyl radicals and the reaction yield, decreasing the reaction time and cost of the
 141 process. In this study, it was possible to degrade 100% of the contaminant using higher concentrations of PNF,
 142 with similar concentrated ratios of H₂O₂, in better reaction time conditions, of 10, 30, 70 and 120 minutes. Datta
 143 et al. (2004) used a UV/H₂O₂ system to degrade 15 mg L⁻¹ of PNF, degrading 100% of the contaminant in 5 hours
 144 of testing, using a 8 W mercury lamp. The experimental tests carried out in this work demonstrated the capacity
 145 for degradation under pollutant and hydrogen peroxide concentrations at much lower ratios, which makes these
 146 results interesting from an economic point of view, given the lower energy and input consumption.

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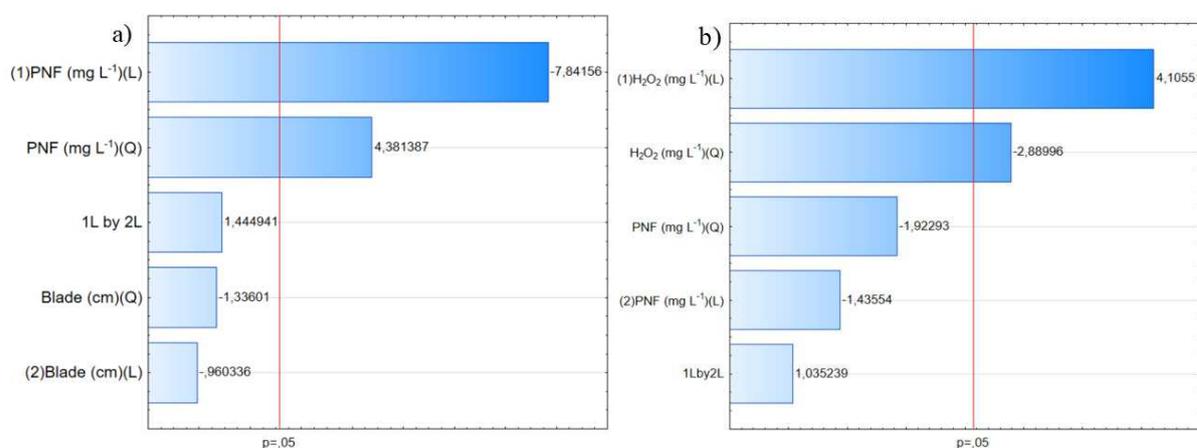
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149 **Fig. 2** Percentages of PNF degradation obtained from the experimental design for the UV and UV/H₂O₂ system.

150

151 In the Pareto diagram (Fig. 3), it is possible to visualize the influence of the studied variables in the applied
 152 treatments. As a planning response, for the degradation in the UV-only system (Fig. 3a), the linear and quadratic

153 term of the contaminant concentration were statistically significant in the oxidation reaction of the PNF. As the
 154 linear term had a negative effect (-7.84156), it can also be concluded that the greatest efficiency of degradation
 155 occurs in lower concentrations of PNF. For the effects of contaminant degradation by the UV/H₂O₂ process (Fig.
 156 3b), it is possible to observe the direct influence of the primary oxidizing agent H₂O₂ in the linear and quadratic
 157 term. The linear term (+4.10551) indicates that PNF degradation is enhanced in higher concentrations of peroxide.
 158 This effect was also observed by Wang et al. (2021b) when treating 10 mg L⁻¹ of PNF through the photo-fenton
 159 process in continuous flow for approximately 4 hours, in which he observed that the reaction rate increases as
 160 H₂O₂ is added in the system. The author increased the efficiency from 35% to 84% of PNF degradation by
 161 increasing the peroxide concentration from 68 mg L⁻¹ to 170 mg L⁻¹. The increase in catalysis performance by
 162 increasing H₂O₂ concentrations was also observed by Khairy et al. (2020).
 163



164
 165 **Fig. 3** Pareto chart of effects for PNF degradation in the UV (a) and UV/H₂O₂ (b) system.
 166

167 From the calculation of the effects of the studied factors, as well as the possible interactions, an optimized
 168 parameterized model was obtained to describe the PNF degradation for the UV-only (Eq. 4) and UV/H₂O₂ (Eq. 5)
 169 processes. The percentage of explained variation (R²) obtained by the models was 94.33% for the UV-only process
 170 and 92.55% for the UV/H₂O₂ system, showing good adjustment to the experimental data.

171
 172
$$UV \text{ Degradation } (mg \text{ L}^{-1}) = 84.155 - 2.840x + 0.010x^2 + 14.663y - 6.487y^2 + 0.451xy \quad (4)$$

173
$$UV/H_2O_2 \text{ Degradation } (mg \text{ L}^{-1}) = 82.588 - 0.528x + 0.003x^2 + 0.174y - 0.005y^2 + 0.004xy \quad (5)$$

174

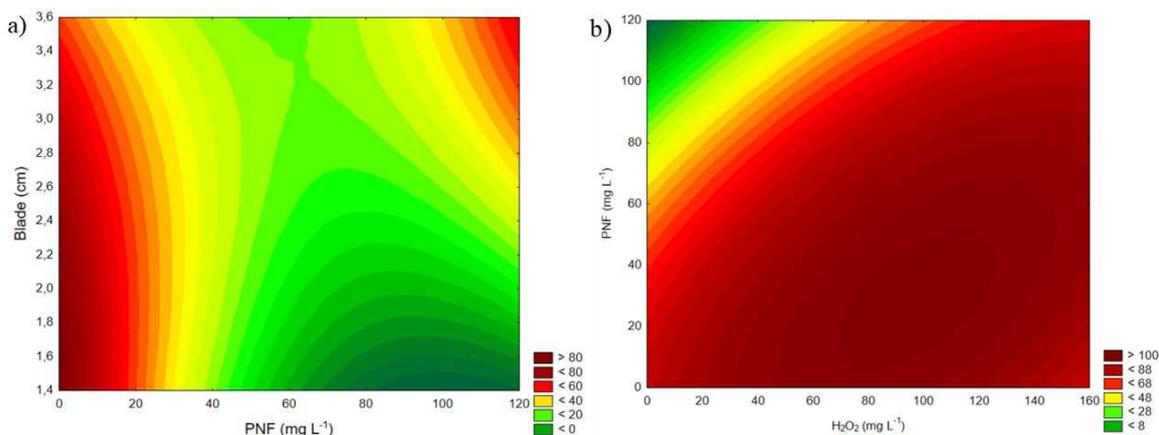


Fig. 4 Response surface for PNF degradation in the UV-only (a) and UV/H₂O₂ (b) system.

Optimized conditions of PNF concentration, water depth and H₂O₂ concentration are obtained (Fig. 4) from the contour surfaces generated by the model. It is possible to verify, from the contour curve (Fig. 4a), that the optimal degradation conditions in the presence of UV light only occurs for concentrations of up to 10 mg L⁻¹ of contaminant (C₆H₅NO₃) and at a water depth of effluent to be treated between 1.4 cm and 2.5 cm, obtaining in these conditions up to 80% of degradation in the maximization of the process. ANOVA (Table SM1) confirms that these results are statistically significant ($F_{calc} > F_{tab}$) and reliably represent the results (Fig. SM1).

The optimal range for degradation in the UV/H₂O₂ process (Fig. 4b) indicates that the PNF concentration, under the conditions evaluated, can reach up to 60 mg L⁻¹, and the H₂O₂ concentration between 50 and 130 mg L⁻¹. In addition to increasing the degradation efficiency at concentrations above 50 mg L⁻¹ of H₂O₂, the experimental tests showed that the increase in the initial concentration of peroxide contributed to the decrease in reaction time, since the primary oxidant is responsible for the formation of hydroxyl radicals. When the ratio between the concentrations of the oxidizing agent and the contaminant was 5:1 and 6:1, the kinetics were favored; that is, when the H₂O₂ concentration was 5 and 6 times the stoichiometric dose of C₆H₅NO₃, the kinetics obtained the equilibrium of reaction faster, in less than 20 minutes, and managed to degrade 100% of PNF. The same did not occur in the tests where the peroxide content corresponded to 2 and 1.7, 0.6, and 0.5 of H₂O₂ of the stoichiometric dose of the PNF. In these tests, the reaction times were longer, varying between 70 and 150 minutes, and degradations of 85%, 70% and 53% were obtained in the longest reaction time. Using ANOVA (Table SM2), it is possible to confirm that these results are statistically significant ($F_{calc} > F_{tab}$) and reliably represent the results (Fig. SM1).

3.2 Optimization of PNF mineralization

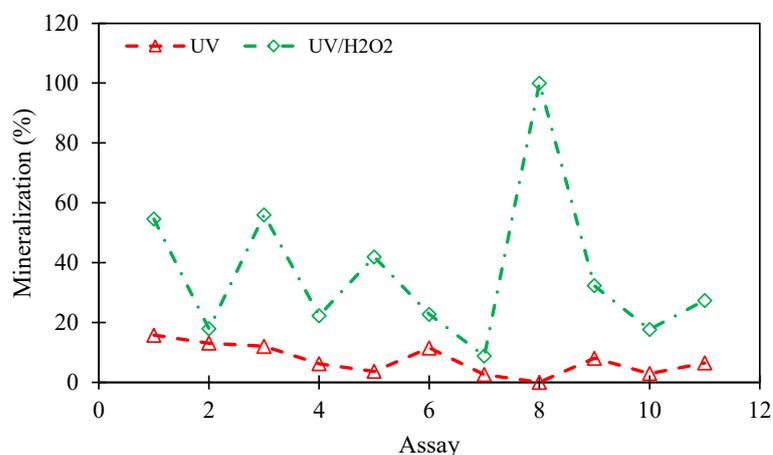
The contaminant mineralization was evaluated by removing TOC, that is, the amount of total organic concentration oxidized to CO₂ and H₂O, which was an important indicator of process effectiveness. Regarding mineralization in the direct photolysis process (Fig. 5), no significant values of TOC removal were found, reaching a maximum of 15.76% for the lowest concentrations of the contaminant (15 mg L⁻¹) associated with lower water depth (2 cm).

205 The removal of TOC for the UV/H₂O₂ assays (Fig. 5) obtained better results compared to the treatment
206 using only UV radiation. About 100% of the PNF was mineralized in the test conducted with the lowest
207 concentration of pollutant studied (10 mg L⁻¹) in the presence of 50 mg L⁻¹ of H₂O₂. In the other tests, some TOC
208 level persisted, depending on the concentration of the contaminant; that is, with the increase in PNF concentration,
209 the concentration of carbon present in the sample after treatment is higher, with lower removal rates being
210 observed. Ledakowicz et al. (2019) states that the persistence of high carbon concentration is characteristic of
211 UV/H₂O₂, compared to other advanced oxidative processes.

212 The permanence of some TOC, even in the tests that obtained degradation of 100% of p-nitrophenol,
213 indicates the formation of intermediate compounds that are resistant to degradation by the UV/H₂O₂ process. That
214 is because, as Xiong et al. (2019) points out, compounds with lower toxicity may be formed (Wang et al. 2021a).
215 P-nitrophenol may have been broken down into low-toxicity p-aminophenol, as well as its byproducts:
216 benzoquinone, hydroquinone and molecular carboxylic acids (Li et al. 2017). Xiong et al. (2018) states that the
217 PNF can be directly oxidized to hydroquinone and benzoquinone, and later to carboxylic acids. When PNF in an
218 aqueous solution is subjected to an advanced oxidation process, intermediate compounds occur in the solution,
219 such as phenol, catechol and p-nitrocatechol, 2,4-DNP, p-benzoquinone, oxalic acid, and acetic acid (Rodrigues
220 et al. 2018; Wang et al. 2021a).

221 The acidic compounds formed during the oxidative process explain the acidity of the solution after
222 treatment. Before the treatment, the initial pH of the solution coincided with the natural pH of the PNF in aqueous
223 solution, being in the range of 5.5 to 6.6 (Li et al. 2019). At the end of the reaction time, the measured pH remained
224 in the range of 3.2 and 4.1, in all tests. The reduction in pH is associated with the production of anions of organic
225 and inorganic acids during the photochemical process, as mentioned by Shu and Chang (2005). The formation of
226 intermediate compounds increases as the initial concentration of PNF is increased, and because these intermediates
227 are highly reactive to hydroxyl radicals, they can reduce the removal efficiency (Daneshvar et al. 2007). The final
228 pH of the treatments using only UV radiation remained slightly acidic, between 5.2 and 6.1. The behavior of the
229 pH close to the natural PNF pH and the low TOC removal shows that, in the direct photolysis system, even in tests
230 that reached values above 60% of degradation, the presence of the contaminant persists at the end of the treatment,
231 as well as that of possible intermediate compounds resulting from the molecular changes undergone by it during
232 photolysis.

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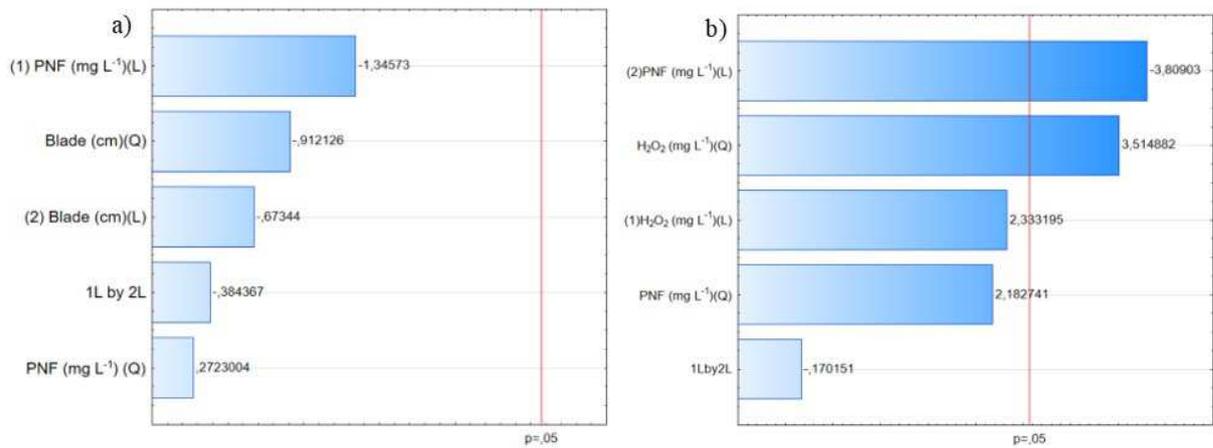
234

235 **Fig. 5** Percentages of PNF mineralization obtained from the experimental design for the UV-only and UV/H₂O₂
 236 system.

237

238 In the Pareto diagram (Fig. 6), it can be seen that, in the mineralization process using the UV-only system
 239 (Fig. 6a), there was no significance for the studied variables, PNF concentration and water depth, within the
 240 conditions evaluated. For the UV/H₂O₂ tests (Fig. 6b), however, the diagram points to the direct influence of the
 241 linear term of PNF concentration (-3.80903) and the quadratic term referring to hydrogen peroxide for
 242 mineralization, with the negative value of variable PNF (linear) suggesting that, at lower concentrations of the
 243 contaminant, the mineralization would be higher.

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245

246 **Fig. 6** Pareto chart of effects for PNF mineralization in the UV-only (a) and UV/H₂O₂ (b) system.

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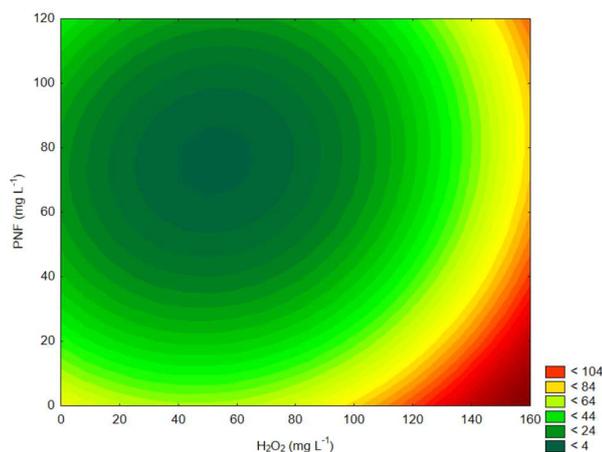
248 In ANOVA (Table SM3), it appears that, in the UV-only system, the mineralization was not significant
 249 ($F_{calc} < F_{tab}$) and did not present a good correlation of the data (Fig. SM3), thus it was not possible to obtain an
 250 equation capable of predicting the removal of TOC. However, in the UV/H₂O₂ system, ANOVA (Table SM4)
 251 confirms the reliability of the results (Fig. SM4), making it possible to obtain a parameterized model (Eq 6) that
 252 manages to represent about 92.44% of the data.

253

254 $UV/H_2O_2 \text{ Mineralization (mg L}^{-1}\text{)} = 75.552 - 0.630x + 0.006x^2 - 1.481y + 0.010y^2 - 0.001xy$ (6)

255

256 Fig. 7 shows the contour curves for TOC mineralization in UV/H₂O₂ tests. The maximum removal of PNF
 257 occurred in low concentrations of contaminant (< 10 mg L⁻¹) and H₂O₂ concentrations above 150 mg L⁻¹.



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259 **Fig. 7** Response surface for PNF mineralization in the UV/H₂O₂ system.

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In a photocatalytic process with the presence of H₂O₂, it is important to optimize the dose of the oxidizer, since the excess increases the cost of the process and can eliminate the hydroxyl radicals formed (Rodrigues et al. 2018). Thus, the residual peroxide concentration was evaluated at the end of the degradation time in the experimental tests. The higher the concentration of the contaminant, the greater the consumption of H₂O₂ in the system. For example, in PNF concentrations higher than 30 mg L⁻¹, consumption of the oxidant was greater than 60% in all tests, reaching 80%. The tests with a contaminant concentration of 50 and 100 mg L⁻¹ obtained consumption of 70% H₂O₂, consequently, a residual content of 30%. The residual content of the oxidizing agent quantified at the end of the treatment does not interfere in the oxidative capacity, since, in tests 3 and 8, there was a residual content of 90 and 140 mg L⁻¹, respectively, and these conditions allowed for 100% degradation of the nitrophenolic compound. Thus, excess peroxide present in the experimental tests of this study did not lead to the elimination of hydroxyl radicals. Rodrigues et al. (2018) points out the disadvantage of overdosing the oxidative agent. The disadvantage of overdosing applies to the oxidant waste, since there was an excellent degradation of 50 and 30 mg L⁻¹ of the contaminant with less residual content, 30 and 20 mg L⁻¹, respectively, in test 4 and in the central point triplicate (tests 9, 10 and 11).

3.3 Modeling kinetics

Fig. 8 shows the experimental results of the kinetic tests and the adjustment through the models, where the best performance was obtained for each of the studied systems. For the UV-only system, an initial concentration of 15 mg L⁻¹ was used, while for the UV/H₂O₂ system the concentration was 30 mg L⁻¹. In the UV-only system (Fig. 8a), it is noticed that the degradation of the contaminant does occur; however, very long times (400 min) are required, making the process unfeasible. For the UV/H₂O₂ system, the degradation of the PNF was effective and faster (70 min) when compared to the system with the presence of UV light only.

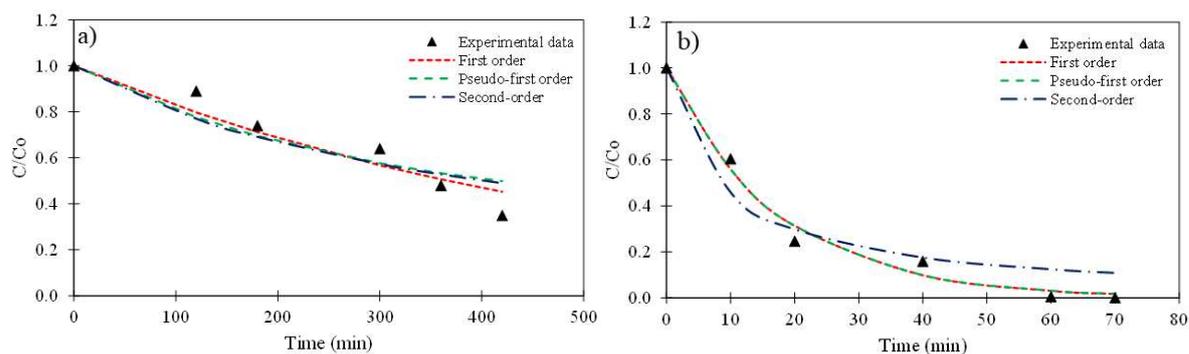


Fig. 8 Experimental results and fitness to mathematical models of first order (FO), pseudo-first order (PFO) and second order (SO) for PNF degradation of the UV-only and UV/H₂O₂ systems.

The experimental results for PNF degradation obtained in the treatments with UV-only and UV/H₂O₂ were adjusted to the first order, pseudo-first order and second order models. In Fig. 8, it is possible to observe that the mathematical models evaluated showed good adjustments to the experimental data. In Table 3, it was found that the determination coefficient (R²) for the UV system, a first-order model, represented the experimental data with greater precision, obtaining a k₁ constant of 0.0018 min⁻¹ with 99% reliability (p-value <0.001). For the UV/H₂O₂ system, two models were able to reproduce the experimental results (first order and pseudo-first order), also with reliability greater than 99% (p-value <0.001) and good R² (0.9927), where the speed constants k₁ and k_{p1} found were 0.0580 min⁻¹.

The rate of degradation for the UV/H₂O₂ system was higher when compared to the UV system (0.0580 min⁻¹ > 0.0018 min⁻¹), where this result is expected, since the presence of H₂O₂ potentiates the oxidation reaction, due to greater amount of *OH produced. According to the study by Zhao et al. (2012), the velocity constant is affected by the pH of the solution, and the rate of degradation in acidic pH is higher when compared to values closer to neutrality and alkalis. In this study, it was observed that the pH at the end of the oxidation process in the presence of only UV light varied between 5.2 to 6.1, while in the UV/H₂O₂ system the pH showed more acidic characteristics, oscillating between 3.2 and 4.1. It should be noted that the initial PNF concentration has a direct influence on the degradation rate constant (Zhao et al. 2012).

Table 3 Results of the kinetics constants of PNF degradation in the UV/H₂O₂ system.

Mathematical model	UV	UV/H ₂ O ₂
First order		
k ₁ (min ⁻¹)	0.0018 ± 0.0002	0.0580 ± 0.0049
p-value	0.0002	< 0.0001
R ²	0.9559	0.9927
Pseudo-first order		
k _{p1} (min ⁻¹)	0.0035 ± 0.0006	0.0580 ± 0.0049
p-value	0.0033	< 0.0001
R ²	0.9241	0.9927
Second order		
k ₂ (L mg ⁻¹ min ⁻¹)	0.0001 ± 0.0001	0.0039 ± 0.0010
p-value	0.0027	0.0010
R ²	0.9257	0.9672

308 The PNF degradation rates found are consistent with the results observed in the literature. The work of
309 Zhao et al. (2012) investigated the removal of the same contaminant ($C_o = 100 \text{ mg L}^{-1}$) under different AOPs,
310 obtaining a constant k_{p1} of 0.012 min^{-1} for degradation in the presence of ultrasound (US) irradiation, 0.035 min^{-1}
311 using Fenton and 0.097 min^{-1} in the combination of these processes (US/Fenton). The combination of AOPs is a
312 strategy to increase the efficacy of the treatment. In the kinetic study of Li et al. (2020), it was found that the
313 pseudo-first order model also obtained the best fit; however, the velocity constant k_{p1} (0.0002 min^{-1}) for the
314 combined UV/H₂O₂ system was much lower than that observed both in the UV-only system and the UV/H₂O₂
315 combination found in this work. Another possibility to improve the efficiency of AOP is the use of catalysts that
316 aim to increase the reaction speed. The constant k_1 obtained in the work of Li et al. (2020) for the combination of
317 the UV/H₂O₂ system with iron-based catalysts reached 0.0415 min^{-1} (UV/Fe-PAN/H₂O₂) and 0.2247 min^{-1}
318 (UV/Fe-HPAN/H₂O₂).

319

320 **4. Conclusion**

321

322 In the present study, AOPs were used to evaluate the degradation and mineralization of the PNF present
323 in aqueous solutions, using a photochemical batch reactor. The UV-only system was not effective due to the high
324 residence time and the low removal of NFs. However, the use of H₂O₂ in low concentrations combined with
325 ultraviolet radiation has shown to be promising for the treatment of wastewater containing PNF in low
326 concentrations, as it obtained the complete removal of PNF. The first-order kinetics model of degradation
327 represented the results. The k_1 constants prove that combining the processes increases the rate of degradation
328 ($k_{1,UV/H_2O_2} = 0.0580 \text{ min}^{-1} > k_{1,UV} = 0.0018 \text{ min}^{-1}$). The intermediate compounds formed in the degradation process
329 are of reduced toxicity compared to the priority compound studied in this work.

330

331 **Declarations**

332

333 **Ethics approval and consent to participate**

334 Not applicable.

335

336 **Consent for publication**

337 Not applicable.

338

339 **Availability of data and materials**

340 Not applicable.

341

342 **Competing interests**

343 The authors declare that they have no competing interests. All authors certify that they have no affiliations with or
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350 **Author's contributions**

351 All authors contributed to the study conception and design. Material preparation and data collection were
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