

# A Novel Method for Efficient Electrochemical Treatment of Actual Dyeing Wastewater With Energy Saving

**Jiachao Yao**

Zhejiang Shuren University

**Sini Lv**

Zhejiang University of Technology

**Zeyu Wang**

Zhejiang Shuren University

**Liyong Hu**

Zhejiang University of Technology

**Jun Chen** (✉ [bec@zjut.edu.cn](mailto:bec@zjut.edu.cn))

Zhejiang Shuren University <https://orcid.org/0000-0003-2695-4673>

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## Research Article

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1     **A novel method for efficient electrochemical treatment of**  
2             **actual dyeing wastewater with energy saving**

3             Jiachao Yao<sup>1</sup>, Sini Lv<sup>2</sup>, Zeyu Wang<sup>3</sup>, Liyong Hu<sup>2</sup>, Jun Chen<sup>1\*</sup>

4     <sup>1</sup> College of Biology and Environmental Engineering, Zhejiang Shuren University,  
5     Hangzhou 310015, China

6     <sup>2</sup> College of Environment, Zhejiang University of Technology, 310014 Hangzhou,  
7     China

8     <sup>3</sup> Interdisciplinary Research Academy, Zhejiang Shuren University, Hangzhou, 310015,  
9     China

10

11     \*Corresponding author

12     E-mail address: bec@zjut.edu.cn

13 **Abstract:** Electro-oxidation is a promising technology for wastewater treatment with  
14 bio-refractory organic and nitrogen pollutants; however, the high energy-demanding  
15 hinders its wide application. In this study, a novel method by regulating the significant  
16 parameter during electro-oxidation process timely for actual dyeing wastewater  
17 treatment with energy saving was studied. Operating factors (i.e., flow rate, initial pH  
18 value, electrode distance, and current density) were investigated for chemical oxygen  
19 demand (COD) and ammonia removal, and results indicated that current density was  
20 the key factor which obviously influenced the electrochemical performance. Indirect  
21 oxidation by active chlorine was then confirmed as the main reaction pathway for  
22 pollutants oxidation, and the relationship between the current density and the generation  
23 of active chlorine was established, suggesting that a large part of the generated active  
24 chlorine was not utilized effectively. Subsequently, a novel method by variation of  
25 current density timely based on the reaction mechanism was proposed; results indicated  
26 that, with similar pollutant removal efficiency, energy consumption could be reduced  
27 from 31.6 kWh/m<sup>3</sup> to 20.5 kWh/m<sup>3</sup>. Additionally, the novel system was further  
28 optimized by Box-Behnken design: COD and ammonia removal efficiencies could  
29 reach 71.8% and 100% respectively, and energy-demanding could be reduced by 45.6%.

30 **Keywords:** Novel method; Parameter optimization; Removal efficiency; Energy saving;  
31 Box-Behnken design

## 32 **1. Introduction**

33 Textile industry is a traditional pillar industry in developing countries and has  
34 greatly contributed to the development of economy (Tang et al., 2021). However, the  
35 dyeing wastewater from textile production usually contains large amounts of residual  
36 dyestuffs, additives and inorganic salts (Aghili et al., 2021). The incompletely treated  
37 dyeing wastewater will pose a direct hazard to environmental safety and public health  
38 due to its highly toxic, mutagenic, and carcinogenic compositions (Patel et al., 2021).  
39 Biological treatment has been considered as one of the most cost-effective technologies  
40 for biodegradation of organic and nitrogen pollutants (Paz et al., 2017); but some non-  
41 biodegradable dyes impede biological activity, even causing the death of  
42 microorganism (Chen et al., 2019). Other techniques such as Fenton (Esteves et al.,  
43 2016), ozone oxidation (Xin et al., 2020), and membrane filtration (Cao et al., 2020),  
44 are also proposed for treating such wastewater; however, the potential secondary by-  
45 products hinder their wide applications (Bae et al., 2015; Yao et al., 2016a).

46 Nowadays, electro-oxidation has presented as a favorable approach for  
47 environmental remediation, especially for the treatment of bio-refractory wastewater  
48 (Meng et al., 2020; Chung et al., 2020). Ma et al. (2018) summarized that, compared  
49 with traditional physico-chemical methods, electro-oxidation is much suitable for the  
50 degradation of persistent color and pollutants from dyeing wastewater. Nippatla and  
51 Philip (2020) investigated the electrochemical performance for dyeing wastewater  
52 treatment; results indicated that 98.3% chemical oxygen demand (COD) removal

53 efficiency along with complete decolourization could be achieved under optimal  
54 conditions.

55 Although electro-oxidation has received great attention due to its advantages of  
56 environmental compatibility, easy handling, and no sludge production, it is a highly  
57 energy-demanding method which hinders its extensive application (Adeogun et al.,  
58 2021; Ozturk and Yilmaz, 2019). In recent decades, intensive attentions have focused  
59 on the electrode preparation (Xia et al., 2020), reactor design (Dória et al., 2020), multi-  
60 technology combination (Bustos-Terrones et al., 2021), and parameter operation  
61 (Aquino et al., 2014). Hamous et al. (2021) developed a carbon textiles electrode  
62 modified with Pt nanoparticles for electrochemical treatment of Orange G (OG) azo  
63 dyeing wastewater; results indicated that the removal efficiency of OG reached 91.8%,  
64 and energy saving could be up to 37.2%. Wang et al. (2020a) investigated the effects of  
65 frequency, pulse duty cycle, and current density on the electrochemical treatment of  
66 indigo carmine wastewater using a pulse power supply; after parameters operated,  
67 energy consumption of 35.5% was saved. In our previous work (Yao et al., 2021), a  
68 process control, namely stepping control of key parameter, was developed for the  
69 treatment of simulated wastewater with known contaminants by direct oxidation. Firstly,  
70 the degradation pathway of target pollutant was measured, i.e., intermediate products  
71 were detected. Then, the oxidation potentials of the target pollutant and its intermediate  
72 products were determined by the linear sweep voltammetry. Finally, stepping control of  
73 oxidation potential was performed timely to oxidize the contaminants selectively based

74 on the degradation pathway of the target pollutant. The results indicated that pollutants  
75 could be efficiently removed, and energy saving could be up to 33.8%, i.e., it proved  
76 that operating key parameter regularly could achieve high contaminants removal and  
77 low energy consumption. However, the composition of actual wastewater is usually  
78 complex so that it is difficult to determine the type of pollutants (Ye et al., 2021; Liu et  
79 al., 2021). Thus, it is necessary to find a way to achieve non-selective oxidation of  
80 pollutants. Generally, in-situ electrochemical generation of excessive active radical is  
81 proposed as a promising method (Yang et al., 2019; Wang et al., 2020b). As reported  
82 by Díaz et al. (2011) and Wang et al. (2021), compared with the traditional method,  
83 pollutants elimination by the in-situ produced oxidants via parameter regulation seemed  
84 to be one of the most convenient methods to achieve the purpose. Though this method  
85 can promote the pollutant removal so as to save energy, a part of energy is still wasted  
86 on maintaining the active radical excess (da Costa et al., 2021). Herein, it's time to  
87 propose an applicable way to regulate the formation of oxidants regularly for efficient  
88 electrochemical wastewater treatment and reduce its energy-demanding.

89 In this study, a novel method, i.e., regulating key parameter timely, was developed  
90 for the treatment of actual dyeing wastewater. Firstly, the effects of flow rate, initial pH  
91 value, electrode distance, and current density on COD and ammonia removal were  
92 investigated, and a significant parameter was determined. Secondly, the reaction  
93 mechanism of the electro-oxidation process was studied to confirm the types of the  
94 active radicals which provided contributions to the pollutant removal, and the

95 relationship between the significant parameter and the generation of the dominated  
96 active radical was established. Then, the novel method by regulating the selected  
97 significant parameter was operated and validated to evaluate its efficiency and energy  
98 consumption. Finally, Box-Behnken design was applied to optimize the novel system  
99 for maximizing pollutant removal and minimizing energy consumption.

## 100 **2. Materials and methods**

### 101 **2.1 Wastewater characteristics**

102 The actual dyeing wastewater was provided by a dyeing factory located in  
103 Shaoxing (Zhejiang, China). The main characteristics of the actual wastewater were as  
104 follows: the COD concentration was  $285\pm 20$  mg/L; the ammonia concentration was  
105  $35\pm 2$  mg-N/L; the pH value was  $8.0\pm 0.1$ ; and the concentration of chloride ion was  
106  $1530\pm 26$  mg/L.

### 107 **2.2 Electro-oxidation experiments**

108 Electro-oxidation experiments were carried out in a self-made electrochemical cell  
109 equipped with a Ti/PbO<sub>2</sub> anode and two Ti cathodes. The anode was placed in the  
110 middle of the two cathodes, and each electrode has an effective area of 9 cm<sup>2</sup>. A  
111 reservoir was connected with the electrochemical cell. During the experiments, the  
112 actual dyeing wastewater (250 mL) could be recirculated in the electrochemical system  
113 with a set flow rate by a peristaltic pump. An electrolysis time of 180 min was selected  
114 for each electro-oxidation experiment.

### 115 **2.3 Analysis and calculation methods**

116 COD and ammonia were measured by the dichromate method and Nessler reagent  
117 spectrophotometry, respectively. Active chlorine and chloramines were measured using  
118 the DPD standard method (Yao et al., 2021).

119 The current efficiency  $CE$  (%) was estimated as:

$$120 \quad CE = \frac{[COD]_0 - [COD]_t}{8It} FV + \frac{3([NH_4^+]_0 - [NH_4^+]_t)}{14It} FV \quad (1)$$

121 where  $[COD]_0/[NH_4^+]_0$  and  $[COD]_t/[NH_4^+]_t$  are the COD/ammonia concentrations at  
122 time  $0$  and  $t$ , respectively;  $I$  is the applied current;  $F$  is the Faraday constant (96 485  
123 C/mol);  $8$  is the oxygen equivalent mass (g/eq);  $14$  is the atomic mass of N;  $3$  is the  
124 electron transfer number from ammonia to  $N_2$ ;  $V$  is the solution volume;  $t$  is the reaction  
125 time.

126 The energy consumption  $E$  (kWh/m<sup>3</sup>) was calculated as follows:

$$127 \quad E = \frac{Ut}{V} \quad (2)$$

128 where  $U$  is the voltage.

129 Response surface methodology based on Box-Behnken design (BBD) was selected  
130 as an experimental design to investigate the effect of significant parameter on pollutant  
131 removal and energy consumption. The three current densities were set as explanatory  
132 variables in BBD, and the pollutant removal and energy consumption were set as  
133 responses.

### 134 **3. Results and discussion**

#### 135 **3.1 Effect of the main parameters**

136 The effect of flow rate, initial pH value, electrode distance, and current density on

137 electrochemical performance were investigated individually to determine the optimal  
138 conditions. **Fig. 1a** shows that, with the increase of flow rate, pollutant removal  
139 increased gradually at the beginning of the experiment, and then reached a maximum  
140 value with a flow rate of 150 mL/min. This finding implies that mass transfer limitation  
141 of pollutants existed at flow rate lower than 150 mL/min, and then reaction limitation  
142 hindered increasing pollutants degradation with further increase of flow rate (Huang et  
143 al., 2016). The effect of initial pH value is illustrated in **Fig. 1b**. The increase of initial  
144 pH value had a negative effect on COD removal. Such results might be related to the  
145 existence form of active chlorine, that is, HClO ( $E^0=1.49$  V vs. SHE) mainly exists in  
146 the pH range from 3 to 8, and  $\text{ClO}^-$  ( $E^0=0.89$  V vs. SHE) at  $\text{pH} > 8$  (Zou et al., 2017).  
147 Although excellent ammonia removal efficiency was also obtained in acidic condition,  
148 initial pH value of 9 was also favorable for ammonia removal; the explanation was  
149 connected with the direct electron transfer which had been reported in our previous  
150 work (Yao et al., 2016b). **Fig. 1c** displays that an apex existed for the COD and  
151 ammonia removal efficiencies at electrode distance of 1 cm. Shortening the electrode  
152 distance can not only increase the potential between the solution phase and the electrode,  
153 but also reduce the mass transfer resistance; however, too small distance may cause  
154 electrode breakdown or short circuit, resulting in reduction of electro-oxidation  
155 performance (Kahraman and Şimşek, 2020). Additionally, **Fig. 1d** indicates that there  
156 was always an upward trend for COD removal with the increase of current density. The  
157 same phenomenon was observed on ammonia oxidation: it was completely removed as

158 current density of 20 mA/cm<sup>2</sup> was applied. These results were consistent with other  
159 studies: high current density could accelerate the generation of active radicals and thus  
160 promote the pollutant removal (Li et al., 2020).

161 According to the results shown in **Fig. 1**, an inflection point always existed for the  
162 pollutant removal with flow rate, initial pH value, and electrode distance, that is, these  
163 parameters could be easily optimized. However, the optimization of current density  
164 would be further investigated combining reaction mechanism, current efficiency,  
165 energy consumption, etc.

### 166 **3.2 Reaction mechanism**

167 Base on the results of optimization process, current density was selected as the key  
168 factor to illustrate the oxidation mechanism during the electrochemical wastewater  
169 treatment. As reported by many scholars (Ken and Sinha, 2021; Iskurt et al., 2020),  
170 COD and ammonia are usually oxidized by direct (i.e., electron transfer) and indirect  
171 (mainly by hydroxyl radical and active chlorine) oxidation. In order to reveal the  
172 electrochemical performance of different oxidation pathways, several comparative  
173 experiments were carried out. In the first group, *p*-chlorobenzoic acid (*p*CBA), which  
174 could react with hydroxyl radicals ( $\bullet$ OH) extremely fast but slowly by other oxidants  
175 and direct electro-oxidation, was selected as the scavenger to measure the function of  
176  $\bullet$ OH radicals (Yao et al., 2016b; Rosal et al., 2008). In the second group, Cl<sup>-</sup> was  
177 removed in advance by the chemical precipitation to avoid the disturbance of active  
178 chlorine during the experiments. The third group combined the above mentioned

179 methods by utilizing the *p*CBA and silver ion to measure the electrochemical  
180 performance by electron transfer. In sight of this, a comparison of the oxidation  
181 pathways of COD/ammonia during the electro-oxidation process were investigated and  
182 the results are shown in **Fig. 2**.

183 **Fig. 2a** presents that the COD removal was contributed by electron transfer, •OH,  
184 and active chlorine. The order of dominance of these three pathways was active  
185 chlorine > •OH > electron transfer. Moreover, with the increase of current density, the  
186 function of active chlorine became more and more obvious, while the role of electron  
187 transfer decreased gradually. This phenomenon might be in connection with the  
188 chlorine evolution reaction (**Eq. (3)**): more electron was consumed to generate active  
189 chlorine. Additionally, similar results were observed for ammonia removal, as shown  
190 in **Fig. 2b**. All the results indicated that the COD and ammonia were mainly removed  
191 by active chlorine in this case.



193 Because of the importance of active chlorine, the variations of its concentration  
194 with different current densities are measured and displayed in **Fig. 3**. The results  
195 indicated that the generation of active chlorine increased with electrolysis time, and it  
196 was positively correlated with current density. As the current density ranging from 10  
197 mA/cm<sup>2</sup> to 25 mA/cm<sup>2</sup>, the production of active chlorine increased exponentially.  
198 However, compared with the phenomenon in **Fig. 2**, the COD/ammonia removal rate  
199 contributed by active chlorine increased slowly with respect to the current density. Such

200 results suggested that the produced active chlorine was excessive, and a large part was  
201 not utilized effectively in the electro-oxidation process. Thus, it seems that a feasible  
202 way to enhance the electrochemical performance and reduce the energy consumption is  
203 to conduct the chlorine evolution reaction and improve the utilization ratio of active  
204 chlorine.

### 205 **3.3 A novel method for wastewater treatment**

206       Based on the above investigation, current density was undoubtedly determined as  
207 the key factor to achieve the aims of high efficiency and low energy consumption for  
208 wastewater treatment. A novel method by variation of current density (VCD) timely  
209 was conducted, that is, the current density was controlled and decreased from 20 to 15,  
210 and 10 mA/cm<sup>2</sup> gradually for each electrolysis time of 60 min. As shown in **Fig. 4a**, the  
211 removal efficiencies of 73.0% and 100% were achieved in the VCD system for COD  
212 and ammonia, respectively, which were higher than the efficiencies obtained by current  
213 density of 15 mA/cm<sup>2</sup> (66.3% COD; 97.4% ammonia) and close to 20 mA/cm<sup>2</sup> (75.1%  
214 COD; 100% ammonia). Besides, the current efficiency of VCD was compared with the  
215 traditional electrochemical system as displayed in **Fig. 4b**. It indicated that the current  
216 efficiencies decreased from 34.6% to 25.6%, and 21.2% with the increase of current  
217 density from 10 mA/cm<sup>2</sup> to 20 mA/cm<sup>2</sup>, respectively. Fortunately, 27.7% current  
218 efficiency was obtained by VCD. More significantly, the VCD system also had an  
219 advantage in energy saving: the energy consumption was calculated as 20.5 kWh/m<sup>3</sup>  
220 which was approximately equal to the required energy with current density of 15

221 mA/cm<sup>2</sup> (20.2 kWh/m<sup>3</sup>) and much lower than that of 20 mA/cm<sup>2</sup> (31.6 kWh/m<sup>3</sup>).

222 The variation of active chlorine generation in electrolysis is shown in **Fig. 5a**. A  
223 linear relationship between the concentration of active chlorine and electrolysis time  
224 could be observed during the VCD, which was different with the situation in traditional  
225 electrochemical process (**Fig. 3**). It indicated that the stable growth of active chlorine  
226 concentration could ensure the efficient oxidation of pollutants, rather than to oxidize  
227 pollutants by generating excessive active chlorine, suggesting that the energy utilization  
228 efficiency could be greatly improved. **Fig. 5b** displays the concentration profiles of  
229 chloramines with different current densities in electrolysis. Fortunately, after 180 min  
230 electrolysis, the generated chloramine concentration in all cases was negligible,  
231 especially for current density of 20 mA/cm<sup>2</sup> and VCD. **Fig. 5c** shows that the pH value  
232 decreased obviously in electrolysis as the current density increased, which was in  
233 accordance with the above results of chlorine evolution reaction (**Eqs. (4) and (5)**). For  
234 the VCD system, the pH variation was relatively stable compared with the traditional  
235 electrolysis.



### 238 **3.4 Optimization of the novel method using BBD**

239 Box-Behnken design was selected to provide an advisable way to regulate the  
240 interactions between pollutant removal efficiency and energy consumption (Sharma  
241 and Simsek, 2020; Tak et al., 2015). Herein, three current densities (A, B, C) were  
242 chosen as the explanatory variables of BBD. The detailed levels of the current densities

243 are listed in **Table S1**, where the range for current density A is 15–20 mA/cm<sup>2</sup>, for  
244 current density B is 12.5–17.5 mA/cm<sup>2</sup>, and for current density C is 10–15 mA/cm<sup>2</sup>.  
245 An electrolysis time of 60 min was arranged for each stage. And the current density was  
246 set to decrease gradually from A to C. Besides, the above results indicated that ammonia  
247 could be efficiently removed in this electrochemical system; thus, COD removal  
248 efficiency was selected as the evaluation indicator of pollutant degradation.  
249 Subsequently, seventeen runs of individual experiments with different current densities  
250 were required to fit the three-factor BBD (**Table S2**). Moreover, normality of data was  
251 estimated by means of normal probability plot (**Fig. S1**) which showed that residuals  
252 generally fell near the straight line. Such results supported normal distribution and  
253 confirmed the applicability of the model for well-fitting of the data. The response  
254 contour diagrams for the interactive effect of three current densities on the  
255 corresponding experimental results are shown in **Fig. 6**, and their related 3D surface  
256 diagrams are shown in **Fig. S2**. For the effect of the current densities on the COD  
257 removal, the A-B plot indicated that the contour values increased obviously when the  
258 B increased, and it was also highly linked with A; the A-C plot showed that A is the  
259 significant factor for the COD removal over C; besides, the B-C plot also depicted that  
260 the increase of current density B was beneficial to the COD removal. When it came to  
261 the impact on energy consumptions, similar results could be observed. Such results  
262 obtained from the BBD were consistent with the phenomena as mentioned in **Figs 1**  
263 and **4**.

264 By regulating the effect of each explanatory variable in a reasonable operating  
265 range, the optimal operating parameters of A, B and C were predicted as 18.1, 14.7, and  
266 11.6 mA/cm<sup>2</sup>, respectively. After optimization, the model values of the pollutant  
267 removal efficiencies and the energy consumptions were experimentally verified. **Table**  
268 **1** shows that the experimental results were in good agreement with the model results.  
269 As shown, actual removal efficiencies of 71.8% and 100% were obtained for COD and  
270 ammonia respectively, and energy consumption of 17.2 kWh/m<sup>3</sup> was calculated.  
271 Compared with the traditional electrolysis (20 mA/cm<sup>2</sup>), though the COD removal  
272 efficiency decreased slightly from 75.1% to 71.8%, the energy consumption was saved  
273 by 45.6%.

#### 274 **4. Conclusion**

275 A novel method for efficient treatment of dyeing wastewater by electro-oxidation  
276 was investigated. Main factors, such as flow rate, initial pH value, electrode distance,  
277 and current density, were studied to reveal their impacts on the pollutant removal, and  
278 the results of electrochemical performance indicated that the current density was the  
279 dominant factor. The reaction mechanism was then explored, suggesting that COD and  
280 ammonia were mainly oxidized by active chlorine. Simultaneously, the relationship  
281 between the current density and active chlorine generation was established; results  
282 indicated that improving the utilization ratio of active chlorine was favorable for  
283 pollutant degradation and energy reducing. A novel method by variation of current  
284 density timely to conduct the chlorine evolution reaction was thus presented, suggesting

285 that energy-demanding could decrease from 31.6 kWh/m<sup>3</sup> to 20.5 kWh/m<sup>3</sup>. Further  
286 investigation of the interactive effect of current densities on energy saving was  
287 predicted by BBD; results indicated that the energy efficiency could be enhanced: with  
288 a high level of pollutant removal efficiency, the energy saving could be up to 45.6%.

289

290 **Ethical Approval** Not applicable

291 **Consent to Participate** Not applicable

292 **Consent to Publish** Not applicable

293 **Authors Contributions**

294 Jiachao Yao: formal analysis, investigation & writing;

295 Sini Lv: formal analysis & investigation;

296 Zeyu Wang: validation & data curation;

297 Liyong Hu: review & methodology;

298 Jun Chen: resources, writing & review

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304 **Competing Interests**

305 The authors declare that they have no competing interests.

306 **Availability of data and materials**

307 All data generated or analyzed during this study are included in this published  
308 article [and its supplementary information files].

309

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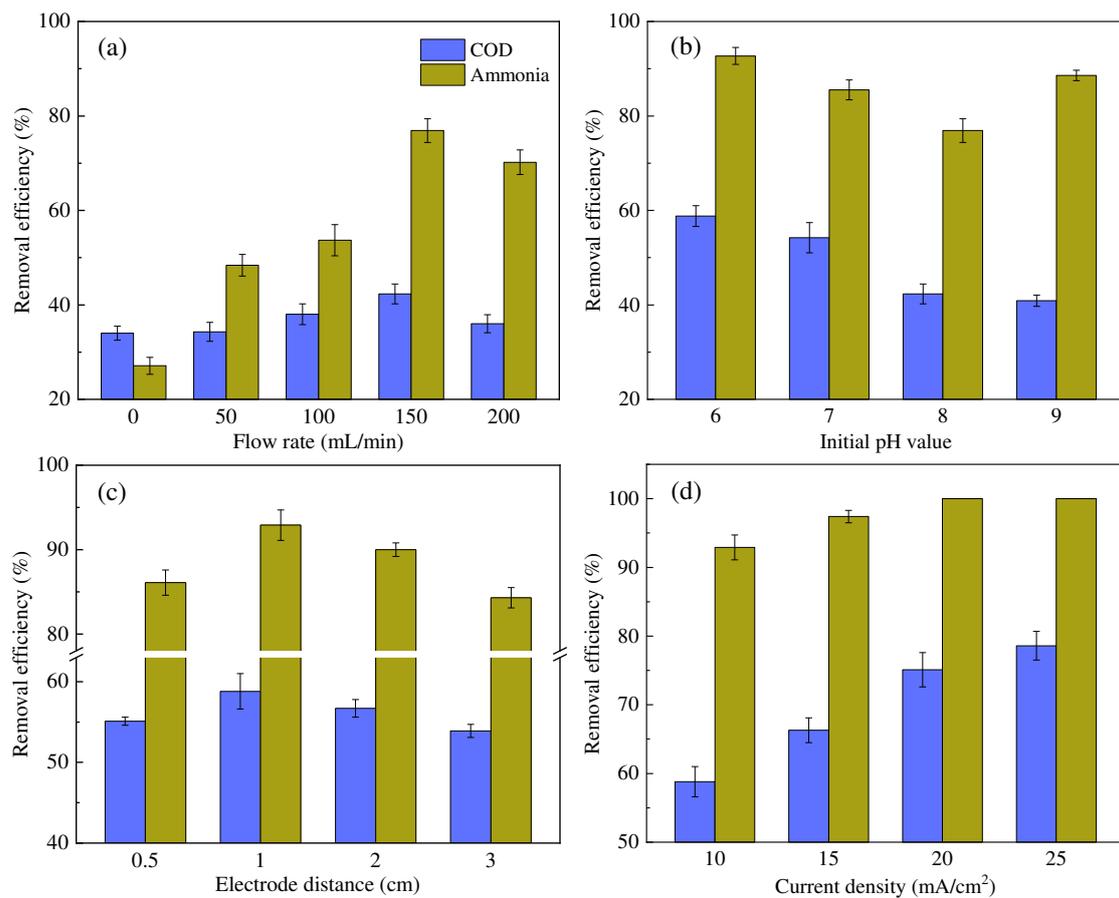
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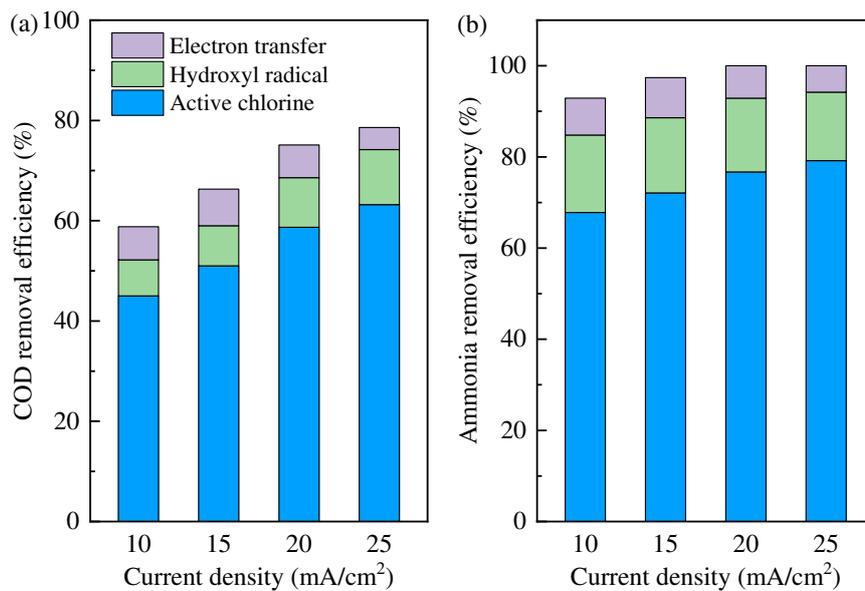


444

445 **Fig. 1.** The effect of (a) flow rate, (b) initial pH value, (c) electrode distance, and (d)

446 current density on COD/ammonia removal.

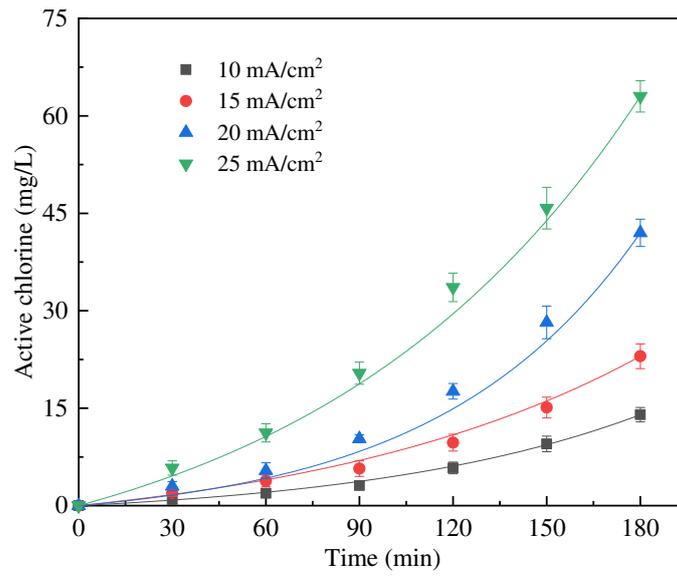
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449 **Fig. 2.** Reaction mechanism for (a) COD and (b) ammonia oxidation with different  
 450 current densities. (Flow rate of 150 mL/min, initial pH value of 6, electrode distance of  
 451 1 cm)

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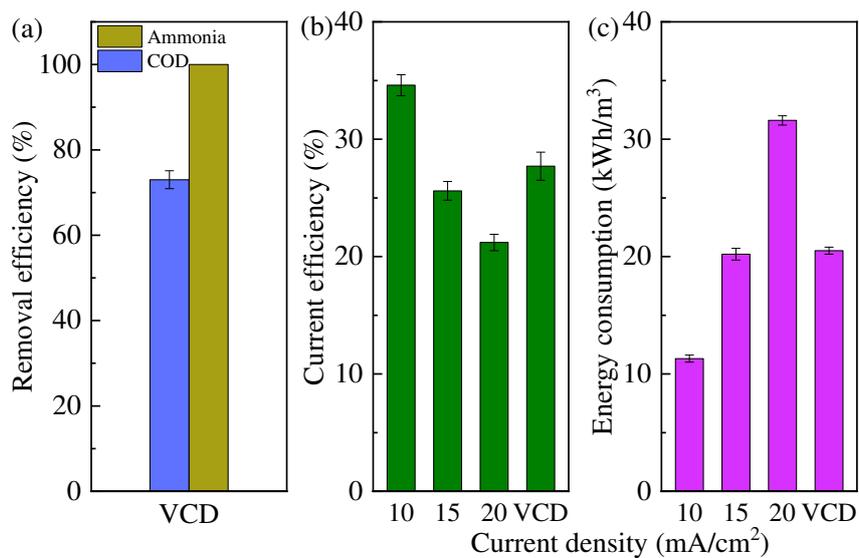


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454 **Fig. 3.** The effect of current density on active chlorine generation. (Flow rate of 150

455 mL/min, initial pH value of 6, electrode distance of 1 cm)

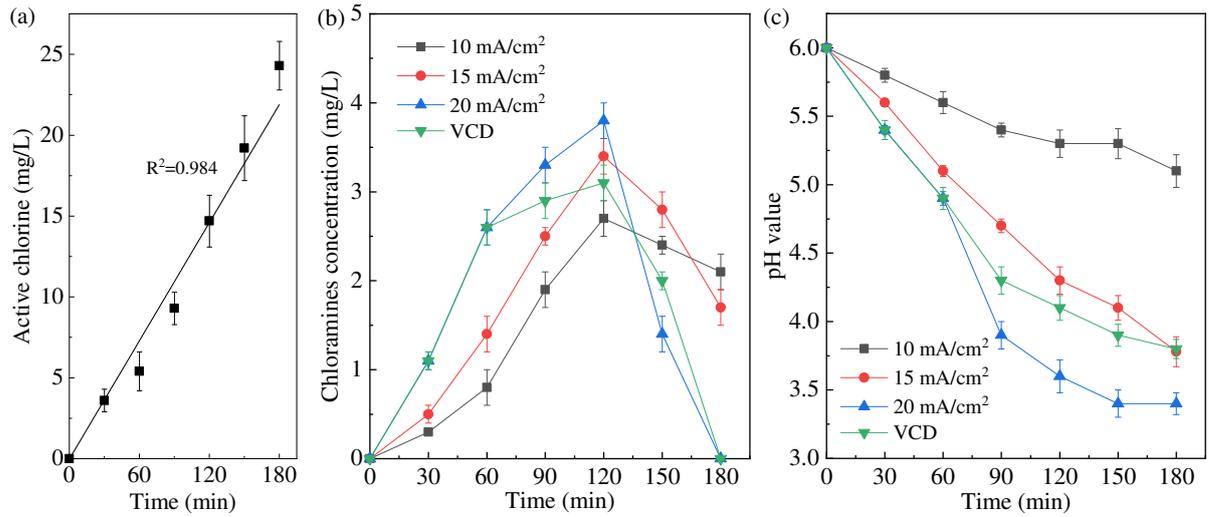
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457

458 **Fig. 4.** The effect of current density variation on (a) removal efficiency, (b) current  
 459 efficiency, and (c) energy consumption. (Flow rate of 150 mL/min, initial pH value of  
 460 6, electrode distance of 1 cm)

461



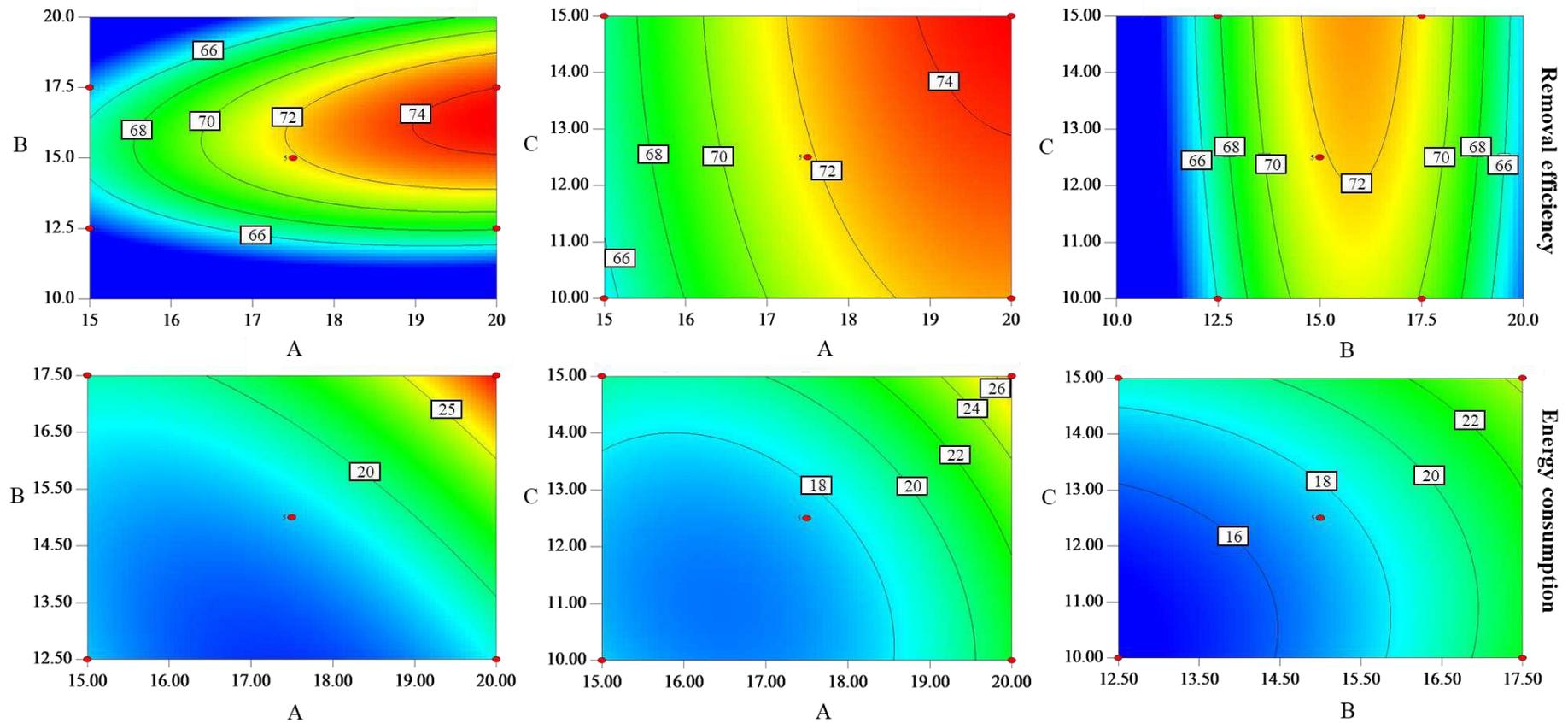
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463 **Fig. 5.** The variation of (a) active chlorine concentration, (b) chloramines concentration,

464 and (c) pH value. (Flow rate of 150 mL/min, initial pH value of 6, electrode distance of

465 1 cm)

466



467

468 **Fig. 6.** Response contour diagrams of Box-Behnken designs for the variation of current density (A, B, and C) on the COD removal and energy

469 consumption. The first and second row in the figure refer to the removal efficiency and energy consumption, respectively. The change of color

470 from blue to red represents an increase of removal efficiency/energy consumption.

471 **Table 1.** The determination and verification of BBD for maximizing removal efficiency and minimizing energy-demanding.

Condition	A (mA/cm <sup>2</sup> )	B (mA/cm <sup>2</sup> )	C (mA/cm <sup>2</sup> )	COD removal (%)	Ammonia removal (%)	Energy consumption (kWh/m <sup>3</sup> )
Predicted	18.1	14.7	11.6	72%	/	17.1
Actual	18.1	14.7	11.6	71.8%	100%	17.2
Traditional	20	20	20	75.1%	100%	31.6

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