

New engineering science insights into the electrodes pairing of electrochemical energy storage devices assisted by machine learning

Longbing Qu

The University of Melbourne

Peiyao Wang

University of Melbourne

Benyamin Motevalli

The University of Melbourne

Qinghua Liang

The University of Melbourne <https://orcid.org/0000-0001-5980-9371>

Kangyan Wang

The University of Melbourne

Wen-Jie Jiang

The University of Melbourne

Jefferson Zhe Liu

University of Melbourne <https://orcid.org/0000-0002-5282-7945>

Dan Li (✉ dan.li1@unimelb.edu.au)

The University of Melbourne <https://orcid.org/0000-0003-3461-5751>

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1 **New engineering science insights into the electrodes pairing of**
2 **electrochemical energy storage devices assisted by machine**
3 **learning**

4 Longbing Qu^{1,2}, Peiyao Wang^{1,2}, Benyamin Motevalli¹, Qinghua Liang², Kangyan Wang²,
5 Wen-Jie Jiang², Jefferson Zhe. Liu^{1*} and Dan Li^{2*}

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7 ¹Department of Mechanical Engineering, The University of Melbourne, Melbourne, Victoria,
8 Australia; ²Department of Chemical Engineering, The University of Melbourne, Melbourne,
9 Victoria, Australia.; Corresponding author Email: dan.li1@unimelb.edu.au (D.L.);
10 zhe.liu@unimelb.edu.au (J.Z.L.)

11 **Pairing the positive and negative electrodes with their individual dynamic characteristics**
12 **properly matched is essential to the optimal design of electrochemical energy storage**
13 **devices. However, the complex relationship between the performance data measured for**
14 **individual electrodes and the two-electrode cells used in practice often makes an optimal**
15 **pairing experimentally challenging. In this work, taking graphene-based supercapacitors**
16 **as an example, we combine experiments with machine learning to generate a large pool**
17 **of capacitance data for graphene-based electrode materials with varied slit pore sizes and**
18 **thicknesses, and numerically pair them into different combinations for two-electrode cells.**
19 **The as-achieved pairing results allow us to conduct a comprehensive analysis of the**
20 **correlations between the key electrode structural features of individual electrodes and**
21 **volumetric capacitance of the resultant two-electrode cells. The results show that the**
22 **optimal pairing parameters are varied considerably with the operation rate of the cells**
23 **and are even influenced by the thickness of the inactive components. The best-performing**
24 **individual electrode does not necessarily result in optimal cell-level performance. The**
25 **machine learning-assisted pairing approach presents much higher efficiency compared**
26 **with the traditional trial-and-error approach for the optimal design of supercapacitors**
27 **and provides an additional effective avenue for further improving the performance of**
28 **supercapacitors and is expected to play an enabling role in the future on-demand design**
29 **of energy storage devices. The results observed in this work also indicate the call for**
30 **comprehensive performance data reporting in the electrochemical energy storage field to**
31 **enable the adoption of artificial intelligence techniques to accelerate the translation of**
32 **academic research in this rapidly growing field.**

1 Electrochemical energy storage devices (EESDs) such as batteries and supercapacitors play a
2 critical enabling role in the realisation of a sustainable society¹. A practical EESD is a multi-
3 component system that consists of at least two active electrodes and other supporting materials
4 such as separator and current collector. Understanding and optimising the interplays of
5 individual components is essential to maximising the materials utilisation efficiency of the
6 entire cell²⁻⁴. However, it has been a great challenge to quantitatively investigate the complex
7 relationships between the individual components and the cell- or system-level performance^{2,5}.
8 Matching of different components such as the pairing of positive and negative electrodes in
9 EESDs to achieve an optimal cell-level performance has so far largely relied on the
10 conventional trial-and-error approach. The community, particularly from the industry side,
11 calls for an engineering science approach that focuses on scientific method as a rigorous basis
12 to develop optimised solutions for this challenging task through enhanced understanding and
13 integrated application of mathematical, scientific, statistical, and engineering principles.

14 Taking supercapacitor as an example for EESDs and as to be reiterated below, how the two
15 electrodes of supercapacitors are optimally paired plays a considerable role in the optimisation
16 of the cell-level performance. The complex relationship between the structure of individual
17 electrodes and the two-electrode cells makes it practically challenging to predict and optimise
18 the electrodes pairing based on the performance data of individual electrodes^{2,4,6}. Previous
19 reports have demonstrated that the balancing of electrode mass⁷, pore structure^{8,9}, charging
20 rate^{10,11}, and working potential windows^{12,13} can affect the performance of the as-paired
21 supercapacitor cells. However, the electrodes pairing for supercapacitor cells have been
22 generally carried out on the basis of a simplified performance relationship between individual
23 electrodes and the two-electrode cells or through a limited number of experiments
24 screening^{6,7,14,15}. The past decades have seen tremendous progress in improving the energy
25 storage capacity of supercapacitors through the discovery of new electrode materials^{6,16,17} and
26 electrolytes^{18,19} and the improved understanding of the charging dynamics in nanoporous
27 electrodes²⁰⁻²⁴. However, there have been few methods reported to quantitatively evaluate how
28 the structural parameters of individual electrodes affect the capacitance of supercapacitor cells
29 and whether a pairing reaches the optimum at various operating conditions of the
30 supercapacitor cells. The lack of an effective strategy for electrode pairing thus presents a
31 bottleneck to limit the full potential of high-performance individual electrode materials to be
32 translated into a real supercapacitor device.

1 In the past few years, data science techniques, particularly machine learning (ML), have been
2 introduced into the energy storage field to solve some challenging research questions of
3 EESDs²⁵⁻²⁹. In battery research, ML has been applied for electrode material design,
4 synthesis/manufacturing, and characterisation^{30,31,32,33,34,35} as well as battery cell diagnosis and
5 prognosis^{36,37}. For supercapacitors, ML has been introduced for active material performance
6 prediction and electrode optimal design³⁸⁻⁴¹. These results clearly demonstrate the merit (high
7 efficiency and cost effective) of combining experiment and data driven approach to address the
8 complex energy material processing-structure-property relationship or device managements. It
9 is promising to combine experiments and ML to investigate the complicated component-device
10 relation to gain much-needed engineering science insights to accelerate the translation of
11 breakthrough energy materials to cell-level performance under various working conditions.

12 In this work, we use graphene-based supercapacitors as a model system to analyse the
13 complexity and necessity of a rational approach for electrodes pairing to optimise the
14 performance of EESDs and demonstrate how the emerging ML and data science techniques
15 can provide an effective solution to this long-standing problem. Briefly, we will first revisit the
16 basic principles and key considerations of electrodes pairing for supercapacitors and discuss
17 the need of a large performance data pool of individual electrodes under varied conditions for
18 an optimal pairing. We then present a combined approach of experiments and ML to address
19 this need. On the basis of a comprehensive analysis of the relationships between the electrode
20 structures and the volumetric performance of the paired combinations, we highlight some new
21 engineering science insights that are often overlooked yet important in the existing electrodes
22 pairing practice. We conclude this article with a perspective on the enabling role of ML in the
23 future on-demand design of EESDs.

24 **Revisit the principles of electrodes pairing engineering for supercapacitors**

25 As with other electrochemical devices, a supercapacitor cell in practical use must contain at
26 least two electrodes connected in series, which are respectively charged positively and
27 negatively during the charging process⁷. Assuming that no other side reactions or energy loss
28 occur during the operation, the charges stored in the cell and both electrodes will be equal
29 ($\Delta Q_{cell} = |\Delta Q_+| = |\Delta Q_-|$) at any time to ensure the charge balance between the two
30 electrodes⁴². Because the positive and negative electrodes are connected in series in the cell,
31 the working voltage of the cell will be a sum of the absolute values of working potential
32 windows for the two electrodes ($\Delta U_{cell} = |\Delta U_+| + |\Delta U_-|$). Thus, the following relationships
33 should be satisfied in the design of a supercapacitor⁴³:

$$1 \quad C_+ \times |\Delta U_+| = C_- \times |\Delta U_-| = C_{v+} \times V_+ \times |\Delta U_+| = C_{v-} \times V_- \times |\Delta U_-| \quad (1)$$

$$2 \quad C_{cell} = (C_+ \times C_-)/(C_+ + C_-) \quad (2)$$

3 where C_+ and C_- (V_+ and V_-) are the total capacitance (the corresponding electrode volume)
 4 for the individual positive and negative electrodes, respectively. C_{v+} and C_{v-} are volumetric
 5 capacitance of the corresponding electrodes against their volume. ΔU_+ and ΔU_- are the
 6 working potential windows of positive and negative electrodes, respectively. C_{cell} is the total
 7 capacitance of the supercapacitor cell.

8 It is worth pointing out that other engineering issues, often overlooked in the scientific literature,
 9 need to be considered in the design of EESDs. Apart from the electrodes that actively store
 10 energy, other supporting components such as the current collector, separator, and packaging
 11 materials are needed. These components are inactive for energy storage, but they take up a
 12 considerable amount of mass/volume of the cell, affecting the overall energy density of the
 13 whole cell^{2,4}. To allow a reliable evaluation of the performance of a supercapacitor cell that is
 14 aligned with the requirement by the energy storage industry, the mass or volume of the entire
 15 device, including inactive components, needs to be considered^{2,4}. The volumetric capacitance
 16 and energy density of the supercapacitor cells can thus be described as below^{4,15}:

$$17 \quad C_{v-cell} = C_{cell}/(V_+ + V_- + V_{inactive}) \quad (3)$$

$$18 \quad E_{v-cell} = \frac{1}{2} C_{v-cell} \times \Delta U_{cell}^2 = \frac{1}{2} C_{v-cell} \times (|\Delta U_+| + |\Delta U_-|)^2 \quad (4)$$

19 where C_{v-cell} , E_{v-cell} , and ΔU_{cell} are the volumetric capacitance, energy density, and working
 20 voltage of a supercapacitor cell, respectively. $V_{inactive}$ refers to the volume of the inactive
 21 components. These equations indicate that the performance of a supercapacitor cell follows a
 22 nonlinear relationship with the capacitance of individual electrodes and the volume of inactive
 23 components.

24 More complicating for the supercapacitor design is that the two electrodes can involve different
 25 charging kinetics, particularly for asymmetric supercapacitors. Even for the same electrode
 26 materials, C_{v+} and C_{v-} can be different or exhibit different variation profiles against the
 27 operation rate^{13,44,45}. The discrepancy between C_{v+} and C_{v-} is particularly remarkable when
 28 the ΔU_+ and ΔU_- are adjusted to maximise the cell voltage (ΔU_{cell}) to achieve the maximal
 29 E_{v-cell} (Eq. 4)^{13,14}. According to Eq. 1, a change in the ratio of C_{v+} to C_{v-} need to be
 30 compensated by the ratio of the electrode volume or the working voltage distribution of positive
 31 and negative electrodes in the cell. The variations of either ΔU_+ (ΔU_-) or C_{v+} (C_{v-}) would then

1 affect the cell-level energy density (Eq. 4). Thus, it is a challenge to achieve the optimal
2 electrode pairing parameters of the supercapacitors under various operating conditions using
3 the experimental trial-and-error approach. Until now, the electrodes pairing for supercapacitors
4 in the literature is generally carried out with simplified assumptions, for example, neglecting
5 the divergence of charging kinetics in two pairing electrodes, the effect of inactive components,
6 or the operation rate. As a result, the capacity of individual electrode materials in a
7 supercapacitor cell is often underutilized.

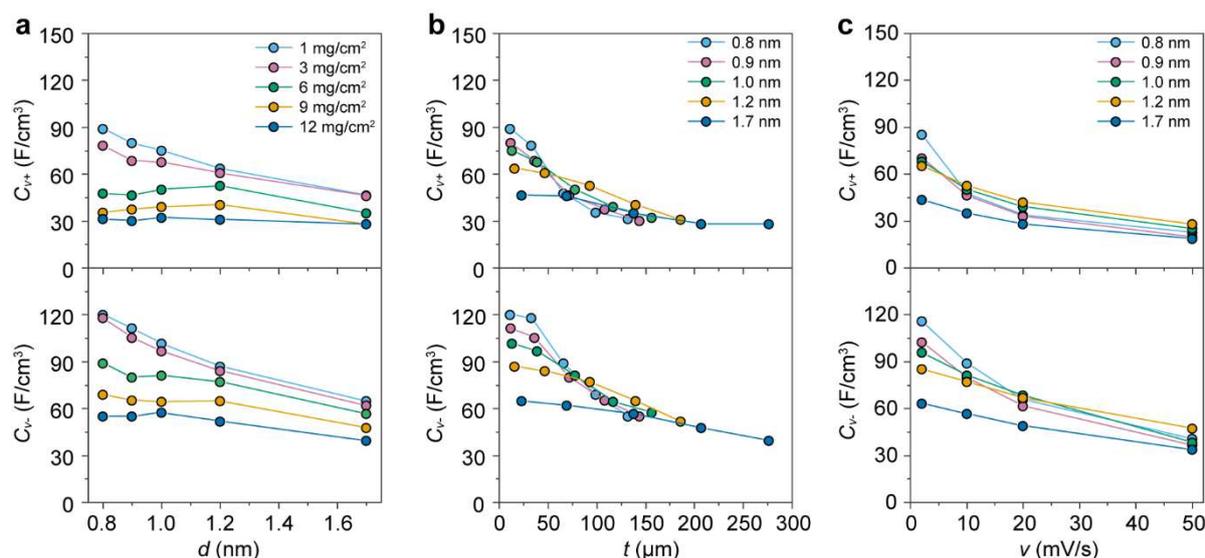
8 As the volumetric capacitance of an individual electrode is dependent on several structural
9 parameters such as the electrode thickness (t), pore size (d), and operating conditions such as
10 working potential window and operation rate (ν)^{6,46,47}, optimally pairing two electrodes at
11 various operation conditions according to Eq. 1 will require a large number of electrochemical
12 data of individual electrodes under various conditions. If all the data were to be obtained by
13 experiments, it would be practically infeasible. Here, we will combine experiments with ML
14 to build a predictive ML model to correlate the electrochemical performance of individual
15 electrodes with the corresponding electrode structural features and operation rates. We will use
16 the as-obtained model to generate the performance data of positive and negative electrodes for
17 any given conditions and then numerically pair them into supercapacitor cells that meet Eq. 1
18 and calculate the volumetric capacitance of the cells based on Eqs. 2 and 3. To test the validity
19 of the numerical paired results, we fabricated supercapacitor cells with the predictive paired
20 structural parameters to evaluate the numerically paired results. The results have allowed us to
21 analyse how the electrodes pairing affects the cell-level performance and establish the
22 quantitative relationship of each structural/operation parameter for each electrode with the
23 performance of the resultant two-electrode cell.

24 **Acquiring experimental capacitance database for individual electrodes**

25 Acquisition of a sufficient number of data is essential for training a reliable ML model. It has
26 been widely documented in the literature that the pore size⁴⁸⁻⁵⁰, thickness^{2,4,15}, and operation
27 rates^{6,10,11} are the primary parameters affecting the electrochemical performance of
28 supercapacitors. ML has been recently used to predict the specific capacitance of activated
29 porous carbon from the data collected from the literature³⁸⁻⁴⁰. However, given that the literature
30 data were acquired from varied conditions and material sources and thus are unsuited for this
31 work, we decided to obtain the experimental data from our own experiments by taking
32 advantage of the broad-range structural tuneability of the multilayered reduced graphene oxide
33 membranes (MGMs) we previously developed⁶. To achieve this, we first fabricated these

1 graphene-based electrodes with various slit pore sizes and thicknesses (see the details in
2 **Supplementary Note 1** and **Supplementary Table 1**). We followed the previous
3 practice^{12,14,51} to maximise the cell voltage (ΔU_{cell}) by respectively adjusting the working
4 potential window of the positive and negative electrodes to be 0.55 and 1.05 V in an aqueous
5 electrolyte of 1.0 M KCl (see the details in **Supplementary Note 2** and **Supplementary Fig.**
6 **1-3**). Then, we obtained the volumetric capacitance of positive and negative electrodes under
7 the intended working potential windows using the three-electrode electrochemical setup. The
8 as-obtained experimental data were then used for ML to understand how the electrode
9 polarization, pore size, and thickness collectively affect the electrochemical performance under
10 various charging conditions at both individual electrodes and cell levels. The size of
11 experimental data for fitting the ML models for either positive or negative electrodes is 100.

12 **Figure 1** presents the representative volumetric capacitance of the graphene-based electrodes
13 with various pore sizes and thicknesses obtained from the three-electrode setup under a range
14 of operation rates. The results show that the volumetric capacitance (C_{v+} and C_{v-}) of the same
15 graphene-based electrodes measured at the positive and negative potential windows give rise
16 to rather different values. For example, at the tested operation rates, the value of C_{v+} is always
17 lower than that of C_{v-} . Such a variation has also been observed in activated porous carbon⁵².
18 Both C_{v+} and C_{v-} show a nonlinear dependence on the slit pore size, thickness, and operation
19 rates of electrodes (**Fig. 1**). For example, with the increase of the operation rate, there is an
20 increase in the nonlinear relationship between volumetric capacitance and structural parameters
21 of electrodes (**Supplementary Fig. 4**). Increasing the slit pore size of the electrode (**Fig. 1a**),
22 the electrode thickness (**Fig. 1b**), or the charging rate (**Fig. 1c**) leads to reduced volumetric
23 capacitance. These trends are consistent with the literature^{6,15,46,49}. Although the trends can be
24 qualitatively explained by the ion transport theories for porous electrodes, no theoretical
25 models are available to explain and predict the results in a quantifiable manner due to the
26 complex charging dynamics in nanopores^{21,53,54}. The complex interplay of these parameters
27 makes it even more challenging to quantify and predict the relationship between these
28 parameters and the volumetric capacitance.

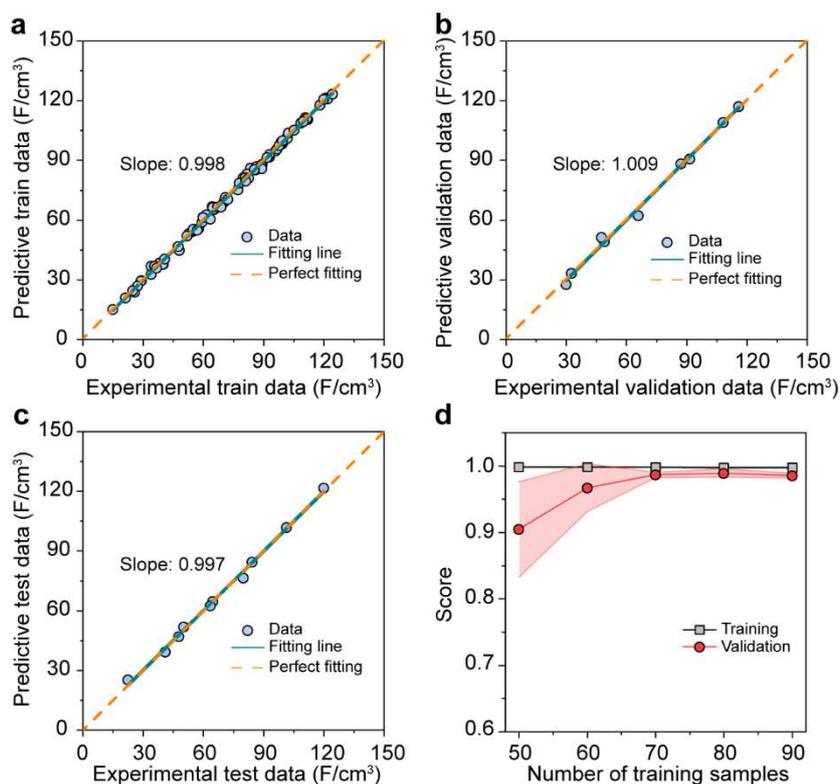


1
2 **Fig. 1 | Representative volumetric capacitance of the individual electrodes of graphene-based**
3 **supercapacitors experimentally obtained under various conditions. a, C_{v+} (top) and C_{v-} (bottom)**
4 **vs. the average slit pore size (d) of the graphene-based electrodes with varying areal mass loading. Only**
5 **the data obtained at $v = 10$ mV/s are presented in the plots. b, C_{v+} (top) and C_{v-} (bottom) vs. the**
6 **thickness (t) of the graphene-based electrodes with varying average slit pore size. Only the data obtained**
7 **at $v = 10$ mV/s are presented in the plots. c, C_{v+} (top) and C_{v-} (bottom) vs. the charging rate (v) of the**
8 **graphene-based electrodes. The data obtained with the electrode mass loading of 6 mg/cm^2 are plotted**
9 **in this figure.**

10 **Machine learning-assisted prediction of the volumetric capacitance of individual**

11 **electrodes**

12 After obtaining the experimental datasets of volumetric capacitance and corresponding
13 structural parameters at different operating rates, we tested several kinds of ML algorithms
14 including ridge regression, polynomial regression, random forest regression and artificial
15 neural network (ANN). After analysing the results of these tested ML algorithms
16 (**Supplementary Table 2**), we decided to use the ANN model to establish quantifiable
17 relationships regarding how the key structural parameters of individual electrodes and the
18 operation rate affect the volumetric performance of individual electrodes. The input descriptors
19 of our ANN models include the electrode thickness and interlayer distance (or slit pore size) of
20 electrode and operation (or charging) rate. The output is the volumetric capacitance of positive
21 or negative electrodes. The middle part of the ANN structure is the hidden layers. The layers
22 among the input layer, hidden layers, and output layer are connected by the weights (see the
23 details in **Supplementary Note 3** and **Supplementary Fig. 5a**).

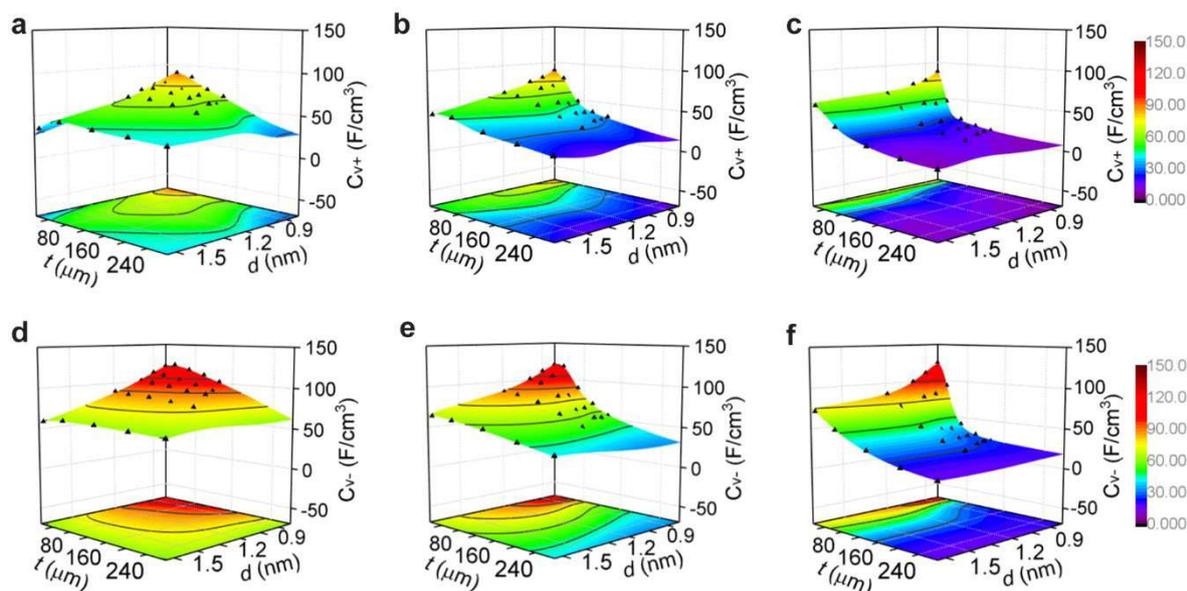


1
2 **Fig. 2 | Representative results of ANN model for the negative electrode. a, b, and c, Model training**
3 **results vs. experimental data, model validation results vs. experimental data, and model test results vs.**
4 **experimental data of ANN model for the negative electrode, respectively. d, The cross-validation**
5 **learning curve of the built ANN model for the negative electrode.**

6 We allocated 80%, 10%, and 10% experimental datasets for training, validation, and test,
7 respectively (**Supplementary Fig. 6**). We did the hyperparameters optimisation to select the
8 suitable ANN network structure and learning rate (see the details in **supplementary file of**
9 **hyperparameter, Supplementary Note 3 and Supplementary Fig. 7**). After that, we
10 conducted the ANN training (**Fig. 2a** and **Supplementary Fig. 5b**). To evaluate the trained
11 ANN models, we compared the validation results and experimental data after the validation
12 procedure. The validation analysis shows that the prediction results from the trained ANN
13 models are in good agreement with the experimental data of positive and negative electrodes
14 (both with the fitting slopes of 1.009) and with mean squared error (MSE) of 0.063% and
15 0.017%, respectively (**Supplementary Fig. 5c** and **Fig. 2b**). The reliability testing with the
16 unseen data that was not used for the ML model training and validation process gives a fitting
17 slope of 1.040 (positive electrode ANN model) and 0.997 (negative electrode ANN model) for
18 experiment and prediction data (**Supplementary Fig. 5d** and **Fig. 2c**). The corresponding MSE
19 for positive and negative models are 0.058% and 0.023%, respectively.

1 We also undertook the stratified shuffle split cross-validation approach to examine the
 2 reliability and sufficiency of the collected experimental data for the ANN models
 3 (**Supplementary Fig. 5e** and **Fig. 2d**). Generally, increasing the number of training examples
 4 results in a higher validation score and lower score variation. For example, when the number
 5 of the training sample reaches 80, the cross-validation score approaches 99%, with a score
 6 variation of 0.6%, suggesting the number of training samples used in our work is rather
 7 sufficient for the ANN model training to achieve a reasonably reliable ANN model, which is
 8 likely due to the high quality of the experimental data obtained from our well-controlled
 9 experiments and the appropriate choice of the key feature descriptors guided by the domain
 10 knowledge⁵⁵.

11 We then simulated 50,000 volumetric capacitance values predicted from the trained ANN
 12 models and plotted the results in the predictive 3D graphs shown in **Fig. 3**. All experimental
 13 data are located on the surface of the 3D graphs, further demonstrating the reliability of the as-
 14 obtained ANN models and the high accuracy of the predicted results. The nonlinear
 15 relationships indicated from these graphs also suggest the intertwined influence of the slit pore
 16 size, thickness, and operating rate of electrodes, indicating the challenge of obtaining a
 17 universal mathematical equation to predict the volumetric capacitance of the electrode
 18 materials using the traditional methods.



19
 20 **Fig. 3 | Volumetric capacitance prediction of the graphene-based individual electrodes from the**
 21 **resulting ANN models. a-c,** The 3D surface and corresponding 2D projection figures (volumetric
 22 capacitance vs. slit pore size and thickness) under the scan rates of 2, 10, and 50 mV/s for the positive
 23 electrodes, respectively. **d-f,** The 3D surface figures and corresponding 2D projection figures

1 (volumetric capacitance vs. slit pore size and thickness) under the scan rates of 2, 10, and 50 mV/s for
2 the negative electrodes, respectively; The triangles in black located at the surface of the 3D figures are
3 the corresponding experimental data.

4 **Numerical pairing of electrodes and experimental testing**

5 To pair the positive and negative electrodes for a completed supercapacitor cell, we first
6 generated an extensive dataset of the values for C_{v+} and C_{v-} under a given condition of
7 electrode structural parameters (slit pore size (d) and electrode thickness (t)) and operation rate
8 (v), with d varied from 0.8 to 1.7 nm at an interval of 0.009 nm, t varied from 11 to 276 μm at
9 an interval of 0.53 μm , and v varied from 2 to 50 mV/s, respectively. We thus obtained 50,000
10 volumetric capacitances of positive and negative electrodes for each under different operating
11 rates. As a demonstration, we numerically paired the electrodes by satisfying Eq. 1 and
12 calculated the volumetric capacitance based on Eqs. 2 and 3 for the cells working at 6, 30, and
13 75 mV/s, respectively, which resulted in 8,533,144, 5,320,777, and 3,576,000 paired
14 combinations, respectively (see the details in **Supplementary Note 4** and **Supplementary Fig.**
15 **8**).

16 To further test the validity of our model and the numerical paired results, we conducted
17 experiments to test whether the numerically paired results based on the predictive datasets can
18 be reproduced by experiments. As a demonstration, we fabricated supercapacitor cells with the
19 paired structural parameters (slit pore size and thickness) that were predicted to generate
20 optimal volumetric capacitance values of 12.4 F/cm³ at 6 mV/s, 9.1 F/cm³ at 30 mV/s, and 7.8
21 F/cm³ at 75 mV/s (see the details in **Supplementary Note 5**). The experimental values we
22 obtained at the corresponding operation rate are 12.1 F/cm³ at 6 mV/s, 8.7 F/cm³ at 30 mV/s,
23 and 7.4 F/cm³ at 75 mV/s (**Supplementary Fig. 9**). All these achieved experimental values are
24 very close to the predicted pairing results. Meanwhile, we also monitored the actual potential
25 window at varied operation rates and found they are also very close to the values intended. For
26 example, when the working voltage of the as-fabricated supercapacitor cell is 1.6 V, the actual
27 potential window recorded at the positive electrode is 0.560 V at 6 mV/s, 0.545 V at 30 mV/s,
28 and 0.552 V at 75 mV/s. All are in good agreement with the intended working potential window
29 of the positive electrode (0.55 V).

30 **Examining the key design parameters for cell-level optimisation**

31 As our pairings were conducted across the entire ranges of all the key targeted design
32 parameters, the comprehensive data obtained allows us to systematically evaluate what design
33 parameters could lead to the optimal cell performance and review how the traditional design

1 practice can be improved. Such an analysis also helps us to unveil the new engineering science
 2 insights for the EESD community that is difficult to gain through the conventional electrodes
 3 pairing practice. To achieve this, we calculated the volumetric capacitance of all the cells that
 4 can be numerically paired according to Eqs. 1-3 and presented the detailed results in the
 5 **Supplementary files of electrodes pairing** and some representative results in **Table 1**.

6 **Table 1.** A list of optimal volumetric capacitance values of supercapacitor cells (C_{v-cell_t}) and the
 7 corresponding structural parameters of positive and negative electrodes in the examined range of
 8 structural parameters at selected operation rates of the cell (v_{cell}) and the thickness (t) of inactive
 9 components. The slit pore size and electrode thickness for the paired positive and negative electrodes
 10 that led to the optimal values are given as $[d_+; t_+]$ and $[d_-; t_-]$. The results are from the cell with the
 11 inactive component of three thicknesses (0, 65, and 130 μm).

v_{cell} (mV/s)	$C_{v-cell_0} [d_+; t_+ d_-; t_-]$ F/cm ³ [nm; μm nm; μm]	$C_{v-cell_65} [d_+; t_+ d_-; t_-]$ F/cm ³ [nm; μm nm; μm]	$C_{v-cell_130} [d_+; t_+ d_-; t_-]$ F/cm ³ [nm; μm nm; μm]
6	22.0 [0.80;35 0.81;14]	12.4 [0.80;96.5 0.80;31]	9.8 [1.15;171 0.80;43]
30	19.7 [0.81;31 0.88;11]	9.1 [1.25;103 0.80;22]	6.9 [1.25;118 0.80;24]
75	17.0 [0.81;24 1.37;11]	7.8 [1.35;73 0.80;15]	5.5 [1.35;83 0.80;16]

12 Our results provide the opportunity to study the optimal design of supercapacitors under
 13 various operating conditions and quantitatively analyse the effect of the operation rates on the
 14 optimal design of supercapacitors. When the inactive component is not considered, which is
 15 often practiced in the laboratory-based research study, at a relatively low operation rate (6 mV/s)
 16 of the supercapacitor, the slit pore sizes of the two electrodes required to realize the maximal
 17 C_{v-cell} are very close (0.80 nm and 0.81 nm, respectively). This is in agreement with the
 18 traditional design practice where the porous electrode materials with the same pore size are
 19 routinely used for both electrodes. However, at the higher charging rates, as generally required
 20 for the real-world use of supercapacitors², our data show that the slit pore sizes of the two
 21 electrodes required for the realisation of optimised C_{v-cell} are rather different, a direct reflection
 22 of the asymmetry in the charging kinetics of the electrode materials under different polarization.
 23 In practice, this means that different porous carbon materials should be used for the paired

1 electrodes in the design of high-rate supercapacitors in contrast to what is traditionally
2 practiced for electrical double layer-type supercapacitors.

3 When the inactive components of supercapacitors are taken into account, which is required for
4 industrial applications, the structural parameters of electrodes to realize the highest C_{v-cell}
5 are also found to be varied for different operation rates. For example, if an inactive component
6 of 65 μm thickness is used, to achieve the optimal design of the supercapacitor cells at a
7 charging rate of 6 mV/s, the slit pore size of positive and negative electrodes should be 0.80
8 nm (**Table 1**). When the supercapacitor cell is intended for optimal use at a charging rate of 75
9 mV/s, the paired slit pore size of positive and negative electrodes should be 1.35 and 0.80 nm,
10 respectively. They are rather different from those of the cells optimised for optimal use at 6
11 and 30 mV/s. We also have conducted several control experiments to examine this trend. We
12 fabricated the supercapacitors with the electrode parameters to be tailored to realize the optimal
13 C_{v-cell} at one charge rate and tested its performance at other operation rates. The resultant
14 volumetric capacitance of the supercapacitor cell was indeed found to be lower than that of the
15 optimal volumetric capacitance predicted at the tested operation rates (**Supplementary Table**
16 **3**). For example, when selecting the optimal structural parameters at 6 mV/s to design the
17 supercapacitor cell working at 75 mV/s, the achieved volumetric capacitance of the
18 supercapacitor cell is 4.3 F/cm³, which is only 58.1% of the volumetric capacitance (7.4 F/cm³)
19 of the supercapacitor cell fabricated based on the optimal electrodes pairing at 75 mV/s.

20 Our results also offer a great opportunity to quantitatively examine how the dimension of the
21 inactive components affects the volumetric performance of EESDs and optimal electrodes
22 pairing. In the literature, the influence of inactive components on the device performance is
23 often neglected, leading to much-inflated reporting performance data on their device fabricated
24 based on the new electrode materials developed^{2,56}. It is recommended that the real
25 performance values of an EESD could be estimated by multiplying the inflated value with the
26 volume/mass ratio of the active components in the entire device². This recommendation is
27 certainly valuable to help inexperienced researchers understand the true metrics for EESDs.
28 However, our analysis reveals that the volumetric capacitance normalized by linearly scaling
29 down an optimized C_{v-cell} value may not be maximal anymore after $V_{inactive}$ is taken into
30 account. For example, at the charge rate of 6 mV/s for the supercapacitor cell, without
31 considering $V_{inactive}$, the optimal volumetric capacitance of the cell is 22.0 F/cm³. Multiplying
32 this value with the volume ratio of the active components in the entire device when the
33 thickness of the inactive component is 65 μm , the calculated volumetric capacitance of the

1 device is 9.4 F/cm^3 at this charging rate, which is 24% lower than that of the maximal
2 volumetric capacitance of the device that can be achieved with other pairing parameters at this
3 operation rate (**Supplementary Table 4**). Such a discrepancy can be qualitatively explained
4 due to the nonlinear relationship between $C_{v\text{-cell}}$ and the dimension of inactive components (Eq.
5 3). Meanwhile, at a given operation rate of the supercapacitor cell, with the thickness change
6 of the inactive component, to achieve the optimal volumetric capacitance of resultant
7 supercapacitor cells, there is also the pairing change for the structural parameters of positive
8 and negative electrodes (**Table 1**). For example, at 6 mV/s of the supercapacitor cell, if the
9 thickness of the inactive component is $65 \text{ }\mu\text{m}$, to achieve the optimal design of the
10 supercapacitor cell, the slit pore size and thickness of the positive electrode is 0.80 nm and 96.5
11 μm , the corresponding slit pore size and thickness of the negative electrode is 0.8 nm and 30
12 μm . When the thickness of the inactive component increases to $130 \text{ }\mu\text{m}$, to achieve the optimal
13 volumetric capacitance of the supercapacitor cell at this working rate, the slit pore size and
14 thickness of positive electrode changes to 1.15 nm and $171 \text{ }\mu\text{m}$, the slit pore size and thickness
15 of the negative electrode is 0.8 nm and $43 \text{ }\mu\text{m}$. These findings suggest that the role of inactive
16 components should be examined for the future cell-level optimisation of EESDs from a holistic
17 system engineering viewpoint.

18 Our results also present a tangible case to help properly understand the correlation of the
19 performance of individual electrodes and supercapacitor cells, which is often confusing to
20 inexperienced researchers in the fields of EESDs. As shown in **Fig. 1** and other reports^{6,48,50},
21 the performance of a supercapacitor electrode is dependent on its structural parameters (pore
22 size, thickness) and charge rate. However, when paired electrodes into a real device, the cell-
23 level performance is also related to the pairing of the structural parameters of positive and
24 negative electrodes, the C_{v+} and C_{v-} may not necessarily be at their maximal values when the
25 cell achieves the optimal volumetric capacitance (**Supplementary Table 5-7**). For example,
26 when the inactive component of $65 \text{ }\mu\text{m}$ thick is used, to achieve the optimal volumetric
27 capacitance of the cell at the charge rate of 6 and 75 mV/s , respectively, the paired volumetric
28 capacitance of positive and negative electrodes is 72 F/cm^3 || 119 F/cm^3 and 47 F/cm^3 || 120 F/cm^3 ,
29 respectively, which is lower than that of the maximal values of C_{v+} (89 F/cm^3) and C_{v-} (123
30 F/cm^3).

31 Discussion

32 To demonstrate the advantage of the data-driven approach over the traditional trial-and-error
33 approach for the optimal design of supercapacitor, we have compared the results of ML-

1 assisted supercapacitors design and the general applied practices for the design of
2 supercapacitors. For the most reported supercapacitor design strategy which the positive and
3 negative active materials have the same pore structure, the researchers adjust the mass loading
4 or thickness ratio of positive and negative electrodes experimentally to achieve the optimal
5 design of the supercapacitors^{7,15,25-26}. Compared to this generally used supercapacitor design
6 strategy, our achieved supercapacitors based on the ML-assisted design method present larger
7 cell capacitance and much higher optimal cell design efficiency (**Supplementary Table 8**).
8 Meanwhile, compared with the traditional symmetric supercapacitor design, our ML-assisted
9 designed supercapacitors also exhibit better performance, especially much higher working
10 voltage (**Supplementary Table 3**, and **Supplementary Fig. 10-11**). Additionally, without the
11 assistance of the ML method, we designed the supercapacitor cells following the same design
12 principles only based on the experimental data. We were only able to achieve the
13 supercapacitor design which works at the operation rate of 30 mV/s due to the requirement of
14 the charge rate ratio of positive and negative electrodes. The resultant design results show that
15 the optimal supercapacitor capacitance based on the experimental data is lower than that of the
16 ML-assisted optimal designed supercapacitors (**Supplementary Table 9**). For example, when
17 the inactive component of 130 μm thick is used, the optimal volumetric capacitance of the
18 supercapacitor cell achieved only based on experimental data is 4.8 F/cm^3 , which is 69% of the
19 volumetric capacitance (6.9 F/cm^3) of the ML-assisted optimal designed supercapacitors.

20 We have also statistically analysed the data in the **Supplementary files of electrodes pairing**.
21 We found that the volumetric capacitance distribution of the as-achieved supercapacitor cells
22 is in a broad range and depends on the operation rate and thickness of inactive components
23 (**Supplementary Figs. 12a-12c**). The probability for achieving the top 10% volumetric
24 capacitance of the cell is less than 0.1% for all the cases we examined with the satisfaction of
25 Eqs. 1-3 (**Supplementary Fig. 12d**). Interestingly, the results also show that there is an overlap
26 of the volumetric capacitance of the resultant cells when charging the cells at different charging
27 rates (**Supplementary Figs. 12a-12c**), further demonstrating the importance and necessity of
28 the operation rate-dependent numerical pairing of positive and negative electrodes to achieve
29 the cells with optimal volumetric capacitance. These results suggest the insurmountable
30 challenge of using the traditional trial-and-error approach for the performance optimization of
31 EESD

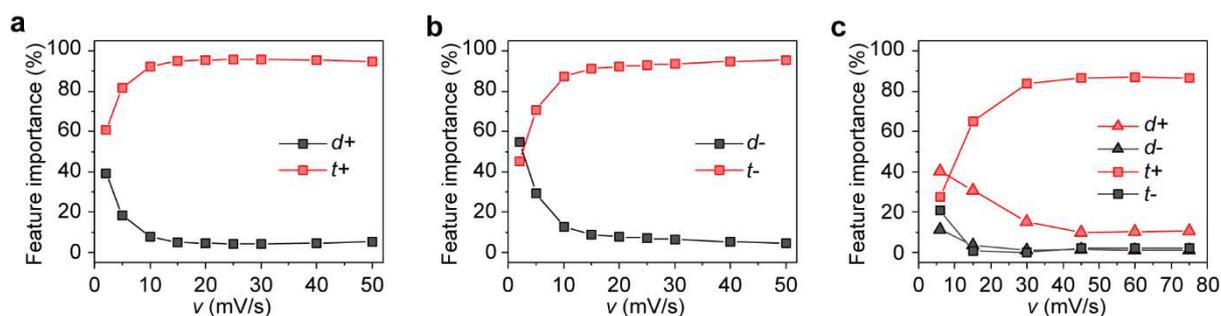


Fig. 4 | Feature importance of the electrode structure parameters on the volumetric capacitance of individual electrodes and supercapacitor cells, respectively. **a** and **b**, The feature importance score of electrode structure parameters on the volumetric capacitance of positive and negative electrodes, respectively. **c**, The feature importance score of electrode structure parameters on the volumetric capacitance of supercapacitor cell. The inactive component with a thickness of 65 μm was considered in the evaluation.

We have further applied a random forest regressor to quantitatively evaluate the weighting of each design parameter in the capacitive performance of individual electrodes and cells at a given condition. The results show that the importance level of each parameter on the volumetric capacitance of electrodes and cells, such as the slit pore size or the electrode thickness, is quite different and depends on the operation rate (**Fig. 4**). For instance, with the increase of the given operation rates, the importance weighting becomes higher for electrode thickness but lower for the slit pore size for both positive and negative electrodes (**Figs. 4a and 4b**). Interestingly, the importance score of electrode thickness for determining the volumetric capacitance of electrodes is always higher than that of the slit pore size of electrodes except for the negative electrode working at a low charge rate (2 mV/s). At a low operation rate (6 mV/s) for the supercapacitor cell, the most crucial electrode parameter in determining the volumetric capacitance of supercapacitor cell is the slit pore size of the positive electrode. When the charge rate is increased to 75 mV/s, the most influential parameter is changed to the thickness of the positive electrode (**Fig. 4c**). We also find that the structural parameters of the positive electrode always are more influential than that of the negative electrode for the volumetric capacitance of supercapacitor cells, indicating the predominant role of the positive electrode for the resultant supercapacitor cells. These results will be particularly valuable for guiding the priority level of design when the optimization of some parameters is prohibitive due to practical technical or cost restraints.

Given that many other EESDs such as batteries and hybrid capacitors are also involved with imbalanced charging kinetics between positive and negative electrodes and rate-dependent

1 performance, we hope that our findings revealed in this work could inspire researchers in other
2 EESD fields to rethink the existing design practice and explore whether the domain knowledge-
3 guided ML can be adopted to tackle these problems that are too difficult for the existing
4 methods. Providing comprehensive data to reveal the remarkable effects of the specific testing
5 conditions on the performance of an EESD at both the individual electrodes and cell levels and
6 the complex relationships between them, this work highlights the great necessity of the
7 previous call for the proper use of true performance metrics^{2,4} and the need for a systems
8 materials engineering approach for the broad field of EESDs³. We also hope that our finding
9 that the best cell performance does not necessarily result from the best individual components
10 suggests the great value of comprehensively reporting the research data including negative
11 results.

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4 **Author contributions**

5 L.B.Q. conceived, designed and carried out the experiments and analysed the experimental
6 results under the guidance of D.L. and J.Z.L. D. L. J. Z. L. and L.B.Q. formulated the concept
7 of applying machine learning models to assist the electrodes pairing. L.B.Q., P.Y.W. and B. M
8 designed and carried out the machine learning modelling and analysed the machine learning
9 model results. L.B.Q and P.Y.W. conducted the electrodes pairing and analysed the electrodes
10 pairing results. All authors participate the discussion of the manuscript writing. L.B.Q. J.Z.L
11 and D.L. wrote the manuscript with contributions from all the other authors.

12 **Competing interests**

13 The authors declare no competing interests.

14 **Data availability**

15 The data that support the findings of this study are available from the corresponding author
16 upon reasonable request.

17 **Additional information**

18 Supplementary information is available in the online version of the paper. Reprints and
19 permission information is available online at www.nature.com/reprints. Correspondence and
20 requests for materials should be addressed to D.L. and J.Z.L.

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