Modal Gain Characteristics of A Two-section InGaAs/GaAs Double Quantum Well Passively Mode-locked Laser with Asymmetric Waveguide

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Abstract

Monolithic two-section InGaAs/GaAs double quantum well (DQW) passively mode-locked lasers (MLLs) with asymmetric waveguide, concluding the layers of P-doped AlGaAs waveguide and no-doped InGaAsP waveguide, emitting at $\sim 1.06\mu\text{m}$, with a fundamental repetition rate at $\sim 19.56\text{GHz}$ have been demonstrated. Modal gain characteristics, such as a gain bandwidth and a gain peak wavelength of the MLL, as a function of the saturable absorber (SA) bias voltage (V_a) as well as the injection current of gain section (I_g), were investigated by the Hakki-Paoli method. With the increase of V_a , the lasing wavelength and net modal gain peak of the MLL both exhibited red-shifts to longer wavelength significantly, while the modal gain bandwidth was compressed. Both the net modal gain bandwidth and gain peak of the MLL followed a polynomial distribution versus the reverse bias at the absorber section. In addition, for the first time, it was found that V_a had an obvious effect on the differential gain of the MLL.

Introduction

Monolithic semiconductor passively mode-locked lasers (MLLs) are ideal light sources for short optical pulses, and particularly attractive for their low cost, small size and ease of pumping. In recent years, light sources emitting at $1.06\mu\text{m}$, with an ultra-short pulse, have attracted great research interests, which are promising for many applications such as biometric imaging [1, 2], frequency comb[3], two-photon microscopy (TPM) [4], lidar remote sensing [5, 6], and so on. In addition, they are also used as pump sources [7, 8]. These are of particular interest given their substantial impact on the applications in photonics and system integration.

Multi-section waveguide structure is generally adopted in a semiconductor mode-locked laser [9–12], where the gain section is forward biased and saturable absorber (SA) section is reversely biased. The gain properties of single-section InGaAs/GaAs QW/QD lasers also have been intensively studied [9–14]. DQW MLLs have higher output power and Electro-optic conversion efficiency than QD MLLs, and multi-section DQW MLLs also can generate shorter pulse [15]. However, the modal gain characteristics, i.e., modal gain bandwidth, peak, of multi-section InGaAs/GaAs DQW MLLs remains unexplored. All these have an important impact on the application of MLLs. Furthermore, as we all know that the thermal stability of InGaAsP semiconductor laser is better than that of AlGaAs[16], P-doped AlGaAs is easier to achieve high-quality growth than p-doped InGaAsP materials, and the ultrafast carrier dynamics in InGaAsP is better than that in AlGaAs, these characteristics of which is more suitable for generating shorter light pulses in an electrically pumped edge emitting semiconductor MLL.

So we report and demonstrate a monolithic two-section passive DQW MLL with asymmetric waveguide emitting at $1.06\mu\text{m}$ getting shorter pulse width and high output power, and the modal gain characteristics is investigated by the Hakki-Paoli method[17–21] to get better understanding on its bias-dependent output. The layers of P-doped AlGaAs waveguide and no-doped InGaAsP waveguide are included in the asymmetric waveguide. For the first time to our knowledge, picosecond pulse generation was achieved by a two-section InGaAs/GaAs DQW MLL with asymmetric waveguide emitting at $\sim 1.06\mu\text{m}$ without

external pulse compression, and the radio frequency (RF) spectrum, dynamic spectrum, net modal gain, and photocurrent performances on the absorber are systematically analyzed for two-section InGaAs/GaAs DQW MLLs. The pulse width and the peak power are also measured for the prepared monolithic two-section MLL.

Device Overview And Experimental Setup

A. Material Structure

In this work, 1.06-μm InGaAs/GaAs DQW laser structures, with asymmetric waveguide, were grown on n-GaAs(100) substrates by metalorganic chemical vapor deposition (MOCVD). The detailed epitaxial structure is shown in the Table I , similar to our previous study [22].

TABLE I.1.06-μm InGaAs DQW laser with asymmetric heterostructure layers

Material	Thickness (nm)	Doping (cm ⁻³)
GaAs	250	p, 2e19
Al _{0.55} Ga _{0.45} As	300	p, 6e18
Al _{0.35} Ga _{0.65} As	300	p, 8e17
Al _{0.3} Ga _{0.7} As	300	p, 8e17
Al _{0.05} Ga _{0.95} As	200	p, 8e16
GaAs	8	barrier
In _{0.2} Ga _{0.8} As	7	quantum well
GaAs	8	barrier
In _{0.2} Ga _{0.8} As	7	quantum well
GaAs	8	barrier
In _{0.03} Ga _{0.97} As _{0.95} P _{0.05}	200	non-doped
In _{0.32} Ga _{0.68} As _{0.4} P _{0.6}	300	n, 8e16
In _{1-x} Ga _x As _{0.5} P _{0.5}	100	n, 8e17
In _{1-x} Ga _x As _{0.7} P _{0.3}	100	n, 8e17
In _{1-x} Ga _x As _{0.9} P _{0.1}	800	n, 8e17
GaAs	200	n, 2e18

B. Device structure and manufacturing process

The MLL fabrication process is similar to those reported in Refs [23, 24]. First, a 6 μm -wide and 1.3 μm -deep ridge waveguide was formed by standard lithography and wet etching. A 300-nm-thick SiO_2 film was deposited as an electrical isolation layer, and a 3 μm -wide p-type electrode window was opened on the etched ridge less than 6 μm -wide (due to the ridge etch). Then, a 10 μm -wide electrical isolation region was patterned by another lithography step. Ti/Au layers were evaporated to form the p-side ohmic contact. After that, lift-off process was carried out to expose the electrical isolation region, and a consequent wet etching process was used to improve the electrical isolation effect. An isolation resistance of $\sim 1\text{k}\Omega$ was achieved between the two sections. Finally, the substrate was thinned, Ni/Ge/Au/Ni/Au layers were evaporated on the n-side, and then an ohmic contact layer was formed after 410 $^\circ\text{C}$ annealing. The processed wafer was cleaved into laser chips for device characterization. During the characterization, a thermo-electrical cooler (TEC) was used to control the operation temperature for the non-soldered MLL. In this study, the MLL was tested p-side up on the TEC, the length of the gain section (L_g) and the saturable absorber (SA) section (L_a) are 1576 μm and 404 μm , respectively. The gain section is forward driven by current (I_g) while the absorber section is reversely biased with V_a . The side view of the two-section MLL with gain section and SA section is shown in Fig. 1. No coating on the cavity facet of MLLs was prepared.

C. Measurement setup

The reverse bias voltage is directly applied to the saturation absorption section by Keithley 2520 power supply, and the photocurrent value is automatically read.

The output light from the gain section facet was first coupled into a single mode fiber, then was split by a 10:90 fiber coupler, the 10 percent was guided into an optical spectrum analyzer (OSA, AQ6370C), and the 90 percent was further split into two equal parts: one was fed into a high-speed photodiode (PD) detector monitored by a 30-GHz real-time oscilloscope (DSO93004L); another was fed as the signal source for an electrical spectrum analyzer (ESA, N9030A). The details are shown in the Fig.2.

D. Experimental results and analysis

The measurement sensitivity is set constant for all measurements. For the tested laser in this study, the wet etched ridge width provides single spatial mode operation condition while operating in the mode locking regime. Figure 3 shows the light output power characteristics under different reverse bias voltages of the absorber section for the tested device in the continuous wave (CW) operation at room temperature (RT). The bias voltage (V_a) applied to the absorber section varied from +1V to -3 V, with a 1V

step, and I_g increased from 0 to 200 mA under each V_a . The use of long absorber sections (up to 20.4 % of total length) resulted in increased absorption and was beneficial to mode locking and obtain ultrashort pulse. As the negative bias on the absorption region increases, the threshold current changes obviously differently in two intervals, one is the interval from +1 to -1V, where the threshold current increases slowly; the other is the interval from -1 to -3V, the threshold current increases rapidly with increased negative bias. This phenomenon should be caused by the strong absorption of the absorption section under a strong negative bias V_a . The L-I and V-I curves show the good operating characteristics of the MLL.

Stable mode locking was achieved over a wide range of V_a (from 0 to -3V). The RF spectra were measured at $I_g=180$ mA and $V_a=-0.9$ V as shown in Fig. 4(a) using a resolution bandwidth (RBW) of 10 kHz.. The fundamental repetition rate with more than 42 dB signal to noise ratio (SNR) at room temperature is ~ 19.56 GHz, corresponding to the photon round-trip time in the 1.99 mm-long laser cavity. The second harmonic frequency at ~ 39.12 GHz is also marked in the figure with ~ 15 dB SNR, which indicate an efficient mode locking. The RF signal from the photodetector was also fed into a 30 GHz real-time oscilloscope (DSO93004L). Fig. 4(b) shows the pulse train observed on the oscilloscope. The time interval between two pulses is ~ 50.78 ps, corresponding well to a repetition rate at ~ 19.69 GHz, which is very close to the fundamental repetition rate ~ 19.56 GHz. The response resolution of the real-time oscilloscope in picosecond and femtosecond level is not enough. Therefore, the measured time pulse train is actually an envelope of ultra-narrow pulses. It can also be seen from Fig. 4(b) that the distribution of the time-domain pulse train presents a more uniform and regular time distribution and the cycle time change is very small and barely noticeable, which shows that the time-domain pulse envelope is much closer to no chirp. It also proves that it is weakly affected by the chirp effect during the test. This provides a basis for calculating its ultra-narrow pulse width using the ideal sech^2 shaped of the time-bandwidth product (TBP) later.

The full width at half maximum (FWHM) of the emission spectrum (D/I) is ~ 1.08 nm, and the optical spectrum of the laser is centered at 1065.35nm. The tested peak and fitted peak curves are showed in Fig. 5. The ideal Lorentz-shaped TBP of ~ 0.22 is a smaller value than the ideal sech^2 shaped pulses TBP of ~ 0.315 . Here, taking into account that it is not significantly affected by the chirp, and assuming an ideal Fourier transform-limited pulse, a pulse width (PW) of ~ 1.1 ps can be expected by the sech^2 shaped. Under this condition, the average power from the MLL is ~ 71 mW, corresponding to a peak power ~ 3.3 W. To our knowledge, this is the narrowest pulse width and the highest peak output power obtained from an electrically pumped edge emitting GaAs-based two-section semiconductor DQW-MLL. It can be seen that pulses get broadened with increasing I_g , and narrowed with increasing V_a .

Figure 6 shows the electroluminescence spectrum measured at different V_a (a: $V_a=+1$ V ; b: $V_a=0$ V ; c: $V_a=-1$ V ; d: $V_a=-2$ V ; e: $V_a=-3$ V). It can be found that the redshift of the lasing peak occurred is moved further away from the center of the spontaneous emission spectrum with an increasing reverse bias. As the reverse bias V_a increases, the band-gap of the absorption region shrinks significantly due to the

quantum confined Stark effect (QCSE). In the gain spectrum of the MLL, lasing tends to happen at long wavelength while mode gain reaches the threshold current [24].

The peak is shifted from 1063 to 1074 nm near the threshold current under different V_a . The peaks redshift, and become narrower and higher with I_g under increasing bias V_a in Fig6.(a-e) . Especially, it is also found that lasing peak will be getting obviously narrower as reverse bias changes from +1 to -3V. This should be caused by the more bandgap shrinkage under big reverse bias.

Gain can be determined by amplified spontaneous emission (ASE) spectrum measurement. The net modal gain (G_{net}) of the two-section MLL was computed using the Hakki-Paoli method. Fig.7 shows the net modal gain spectra at different I_g when V_a was set at +1, 0, -1, -2 and -3V, respectively. The net modal gain is extracted from the peak to valley ratio of sub-threshold Fabry-Perot oscillations, which was computed using the following relation [25].

$$G_{net}(\lambda) = \Gamma g_m(\lambda) - \alpha_i = \frac{1}{L} \ln \frac{\sqrt{S(\lambda)} - 1}{\sqrt{S(\lambda)} + 1} + \frac{1}{2L} \ln \left(\frac{1}{R_1 R_2} \right) \quad (1)$$

where Γ is the confinement factor, g_m is the material gain, α_i is the internal loss related to defects and dopants in the waveguide and QW. S is the peak-to-valley ratio of the FP resonances which can be directly obtained from the ASE spectra, L is the whole cavity length (~ 1.99 mm), and R_1, R_2 are facet reflectivity (A value of 0.346 is used for both cleaved facets). The ASE spectra were recorded with a wavelength step size of 0.02 nm. From Fig. 7, it can be seen that, the net modal gain increases with increasing current, and reaches a value close to the mirror loss ($a_m = (1/2L) \ln(1/R_1 R_2) = \sim 5.33 \text{ cm}^{-1}$), which is the threshold loss.

In the following, a comparison of ASE and gain spectra for InGaAs/GaAs DQW MLLs is implemented. Fig.7 plots the modal gain spectrum as a function of gain section currents, which is derived from the ASE spectra as shown in Fig.6, and it also shows the lasing spectrum near threshold. The laser lases exactly at wavelength of the net modal gain peak, and same results are observed at other V_a , including an internal loss, $a_i \sim (1.56 \pm 0.34) \text{ cm}^{-1}$. An obvious redshift in the gain peak is also observed with increasing V_a , which is attributed to carrier thermalisation within the DQW active layer. It can be seen that the distribution of net modal gain curve tends to be closer near the threshold current at a larger negative V_a value. From formula (1), a larger negative V_a causes the first item on the right side of the formula to become closer to zero, which means the value of S approaching to $+\infty$. When S value is getting larger, the modes of the MLL becomes more stable, also exhibiting a higher power output.

Figure. 8 shows the peak net modal gain as a function of gain section injection current at +1, 0, -1, -2 and -3V bias voltage, respectively, all measured just at or below the threshold. With increasing reverse bias voltage, the peak net modal gain decreases at constant gain current, which is similarly reported It revealed that the dissociation time of the exciton (the width of exciton absorption peak) in the saturable absorber determines the pulse width of mode locked laser. The exciton binding energy of is higher for InP

system and is lower for GaAs/AlGaAs than that for InGaAs/GaAs. The exciton absorption peak shift toward the longer wavelength as the reverse bias is applied (QCSE effect). On the other hand, the gain peak will shift slightly toward shorter wavelength due to band filling effect as the cavity loss increases with reverse bias to the SA section. As a result, the gain peak and absorption peak are separated (as Refs [26, 27]. also observed). Therefore, in this paper, the bandgap of SA was shifted to the shorter wavelength to match the gain and the absorption peaks. This helps to generate short pulse for mode-locked lasers.

for the QD lasers [28,29]. Peak gain saturation trend is observed under a high bias voltage at room temperature, while the temperature condition in the reference is at 80°C. The slope of peak net modal gain versus current declines obviously with reverse bias voltage increasing, which may be caused by the increased the thermal effect of photocurrent in the absorber. This will be further discussed in the following part.

In Fig. 9, the net modal gain spectra at threshold for the same sample at different V_a are plotted. The linear fitting is usually used to derive the internal loss (α_i), which relies on the assumption that the internal differential efficiency keeps constant for lasers with different cavity length. The modal internal loss (α_i) of the DQW laser is derived to be $(1.56 \pm 0.34) \text{ cm}^{-1}$, which is a higher value than the data reported previously [30]. The high internal loss should be caused by the significant shrinking of band gap of the saturated absorption region under negative V_a . The V_a -dependent net modal gain spectra from +1 to -3 V, are measured near threshold current. It can also be seen from Fig 9 that the gain peak is red-shifted and the gain bandwidth is narrowed. These factors lead to an increase in internal optical loss. This is consistent with the internal loss result of the test.

The net modal gain peak redshifts consistently about 10 nm with increasing negative V_a , which may be mainly due to the absorption spectrum shift by the quantum well band-gap shrinking effect. Since the lasing start exactly at the location of the net modal gain peak of the MLL, it also implies a potential application for wavelength tunable or multi-wavelength laser [31]. Both of the polynomial fitting curves imply a very good adjustability. As expected, at all absorber biases, the peak value of net modal gain has nearly a similar value which is mainly determined by mirror loss.

Figure 10 shows the photocurrent (I_s) at absorption region increases as I_g increases, and increases with the V_a negatively increasing. I_s comes from the saturated absorption region under reverse bias, and its current direction and magnitude are related to the applied bias. When $I_g > 140 \text{ mA}$, I_s saturates in the reverse bias voltage range of -3 to -2V. Comparing the effect of I_g on photocurrent, a higher I_g has much greater influence on the photocurrent of MLL, while V_a has important effect on photocurrent saturation. For example, when V_a is in the range of -3 to -2V, I_s increases with V_a negatively increasing, and then saturates. Especially, in Fig.10, the increment of I_s versus gain current (I_g) is uneven under -2V bias. And the efficiency that gain current converts photon into photocurrent gets to the highest value from 120 to 140mA under -2V reverse bias, which indicates the most photons are absorbed by the absorption section.

So mode-locking always happen at high photon absorption status of the absorber, such as $V_a = -0.9\text{V}$ while $I_g = 180\text{mA}$, as shown in Fig. 4(a).

Conclusion

A monolithic two-section InGaAs/GaAs DQW MLL with asymmetric waveguide emitting at $\sim 1.06\text{ }\mu\text{m}$ is demonstrated, and its mode-locking characteristics have been investigated. The mechanisms of the operating behavior are analyzed based on the gain and the saturable absorption in the device.

The fundamental repetition rate with more than 42 dB signal to noise ratio (SNR) is measured at $\sim 19.56\text{ GHz}$, and an ultra-short pulse width (PW) of 1.1 ps is achieved with a peak power of $\sim 3.3\text{ W}$. These results are generally better than the reported by most traditional electrically pumped edge emitting semiconductor MLL. The spectral width and peaks are measured, which become narrower and higher as the bias V_a is negative increased, and the MLL is redshifted while operating in the above changing. The gain peak redshift is observed with increasing V_a , which may be attributed to carrier and photocurrent thermalisation in the DQW active layer. The net modal gain spectrum of MLL with InGaAs DQW has been measured under different bias V_a and at gain region current I_g . An internal loss of $(1.56 \pm 0.34)\text{ cm}^{-1}$ is achieved. It also is found that the photocurrent tends to saturate under high reverse bias voltage. And the PW and peak power can still be further optimized by the multi-section or other structure designs of MLL.

Overall, the results show monolithic two-section InGaAs/GaAs DQW MLL with asymmetric waveguide is more suitable for generating shorter light pulses, and there are of great significance to the research of ultrafast semiconductor mode-locked lasers.

Declarations

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Author Contributions Statement

Qiao Zhongliang wrote the main manuscript. All authors reviewed the manuscript.

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Figures

Figure 1

Sketch (side view) of the two-section MLL.

Figure 2

Schematic diagram of the MLL measurement setup

Figure 3

L-I and V-I curves of the laser with the absorber section bias (V_a) varied from +1 to -3V at room temperature.

Figure 4

(a) Frequency spectrum of the MLL under the bias condition ($I_g = 180mA$, $V_a = -0.9V$). (b) pulse trains under the same bias condition.

Figure 5

Spectrum of the MLLs when PW=1.1ps.

Figure 6

The spectra measured from the InGaAs/GaAs DQW MLL at different V_a (a: $V_a = +1V$; b: $V_a = 0V$; c: $V_a = -1V$; d: $V_a = -2V$; e: $V_a = -3V$).

Figure 7

Net modal gain spectra of InGaAs/GaAs DQW lasers at bias V_a (a: $V_a=0V$; b: $V_a=-3V$)

Figure 8

Peak net modal gain versus gain section current under t +1V, 0V, -1V, -2V, and -3V, respectively.

Figure 9

(a) V_a -dependent threshold gain spectra of the MLL from +1 to -3V. (b) Net modal gain bandwidth (Black square and polynomial fitting line) and peak net gain (blue circle and polynomial fitting line) of the MLL versus bias voltage, respectively.

Figure 10

Photocurrent versus bias voltage under different I_g .