

Verification of Monolithic Rotary Cutting Tool For Active Driven Rotation Machining

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Abstract

Forced rotation turning appears to be an effective machining method due to higher tool life, time efficiency and acceptable quality. Several studies have been carried out to investigate the basic characteristics of forced rotation machining. So far, tools are used whose design included several components. However, such tools may generate vibrations, which are undesirable in the process. In engineering practice, most vibration problems are solved by reducing the cutting parameters (cutting speed and feed rate), which reduces machining productivity. For this reason, a new type of monolithic rotary tool has been designed that eliminates the design complexity and high assembly accuracy requirements of current rotary tools. The presented solution fundamentally validates the new monolithic tool for forced rotation technology and defines its application for different machining materials.

1 Introduction

There is still a lot of production activity in the field of machining, and so there is need for continuous improvement in this area. Rotary tool machining is considered as one of the usable methods for the machining of the future. It can be applied in the process of milling, planing and turning of materials with enhanced mechanical properties [1], [2]. Based on the mode of rotation occurrence in a rotary tool in the machining process, we know two basic modes of rotation, namely, a tool with constrained rotation (SPRT) and tool with forced rotation (ADRT) [1], [3], [4]. Tools with constrained rotation have a rotational motion derived from the friction forces generated between the workpiece and the tool contact surfaces [5]. This type of tool does not require a separate drive for its rotation [6]. On the other hand, tools with forced rotation have rotary motion provided from an external drive [4]. The latter does not have to be part of the machine tool, especially in the case of conventional machine tools [7]. If the technology is used for CNC machines, the CNC machine can provide the tool drive. However, the machine in question must have the possibility to machine-driven tools, for example, directly or with the help of a driven tool holder. The machining productivity highly depends on the tooling material used and its cutting and working properties, especially when machining materials with increased mechanical properties [8]. Machining of refractory steels and alloys is associated with high cutting forces and considerable thermal loading of the cutting edge of the tool. In order To ensure machining efficiency, tools must meet high cutting wedge strength and resistance to thermal stresses. It should be noted that turning tools made from high-speed steel and sintered carbides may not always meet the above two requirements. An option is applying ceramic cutting inserts, which have a good service life but a high price [9]. Different designs of rotary circular tools can be a solution to these requirements due to the use of different kinematic cutting schemes (Fig. 1.). The tool is cooled to a greater extent compared to conventional methods due to the effect of its rotation [10]. The rotation of the cutting part of the tool arranges a better heat dissipation around its circumference due to the contact of only one point of the cutting edge at each time [11]. The main difference from auto-rotating tools, whose rotational motion is dependent on the machining parameters, is that in tools with forced rotation, the frequency of rotation can be controlled, and its

character can be changed with the help of an external actuator. Thus, it is realistically possible to test several options and arrange possibly better productivity than auto-rotating tools.

Some practical tests of forced-motion tools have shown that the ability to handle mechanical and thermal loads on the tool were surprisingly effective compared to conventional machining methods. Available reported records speak of up to 400 to 500% higher productivity and up to 1500 to 2000% higher tool life. According to the available test information, it has been found that radial forces decrease with increasing tool rotational speed, while axial forces increase with increasing tool speed [4]. When machining with a tool with forced rotation, two basic options of rotary tool motion can be used in the cutting process. The rotation can be carried out in clockwise and counterclockwise directions [12]. In the counterclockwise orientation, observations have shown that the tool actually moves from the location where the chip is formed to a greater extent to the location with fewer chips. More surface imperfections were observed by machining in counterclockwise rotation and by increasing the rotational speed of the tool used. Another parameter that affects the machining process by forced rotation is the angle of inclination of the cutting edge to the workpiece axis (λ_s). In forced rotation, this angle does not fundamentally affect the rotational speed of the tool, as it is provided by an external drive unit. For a correct setting, it is necessary to investigate λ_s , since at certain values, there can be a critical increase in cutting force [4]. High temperatures are generated at the cutting point when machining materials and overall high cutting forces are generated [13]. For this reason, conventional tools must be designed to have high cutting wedge strength and also cutting wedge resistance to high temperatures. However, the problem with conventional tools still remains the fact that in the machining process, the same part of the tool is always worn on the tool, which will mainly affect the machining quality and durability of the tool [10], [14] [15]. For a better understanding of the forced rotation machining process, it is necessary to know the force loads at different rotation settings. It can be assumed that the direction of rotation alone will have different results for different machined materials. Cutting tool manufacturers have very limited options for eliminating unwanted vibrations; these include cutting tool geometry, tool body material and, where appropriate, cutting tools with integrated vibration damping mechanisms. In the presented paper, the elimination of unwanted vibrations is addressed by a non-standard cutting tool geometry.

2 Cutting Tool

2.1 Design of the rotary tool

In the scientific studies carried out, tools were used whose cutting part consisted of a standard available replaceable cutting insert (Fig. 2) [1], [2], [4], [12], [14]. It should be noted that these cutting inserts are not designed for machining with active rotation, and their clamping system corresponds to this. When using a replaceable cutting insert of circular shape, high precision of the insert fitting to the clamping part is necessary. If the conditions of high precision are not met, misalignment can occur (Fig. 3), which can result in unwanted vibrations during the machining process.

Strict requirements for accuracy of fit can be met by the use of clamping screws whose head has a negative shape of the cutting insert hole. With tapered shapes, partial concentricity of fit can be achieved (Fig. 4). Such a solution is costly because every single type of cutting insert must have a specially manufactured clamping screw.

2.2. Monolithic rotary tool

When turning with circular interchangeable cutting inserts, a cutting force is generated that requires stable holder clamping, clearance definition and sufficient rigidity. Standard clamping systems require a clamping taper with a rounded hole, and the clamping screw must be in line with the axis of the cutting insert and tool holder. With this design, vibrations in the machining process may occur due to incorrect positioning of the cutting insert due to the concentricity of the insert and tool holder. For this reason, a new monolithic cutting tool (Figure 5) was designed to eliminate the shortcomings of the cutting insert mounting. The cutting portion of the tool was dimensioned to 19 mm and the tool geometry was defined based on previous experimental findings. The design of the presented monolithic tool was filed in 2020 at the Industrial Property Office of the Slovak Republic as a patent solution.

The monolithic rotary turning tool is made of sintered carbide with a 10% cobalt content content for high tool life and the ability to machine relatively hard and difficult to machine materials. The tool must maintain cutting edge sharpness even at high speeds and should also be able to withstand multiple experimental settings of machining parameters. The tapered shank of the monolithic tool is designed for better knife alignment capability with respect to the workpiece and to prevent unwanted excessive friction of the tool rotary surface against the workpiece surface during machining. In order to experimentally validate the monolithic rotary tool in the machining process, six tools with identical geometry and material composition were fabricated (Figure 6).

3 Materials

Identification of the applicability of the monolithic tool was carried out on several types of materials with different mechanical properties. The aim was to determine materials that would represent a group of tough and difficult to machine materials.

3.1. Material to be machined – tool steel

90MnCrV8 is a cold-forming tool steel with high form stability in heat treatment, very high cracking resistance, high machinability, medium toughness and wear resistance. Its chemical composition is given Table 1 [16].

Table 1
Chemical Composition 90MnCrV8 (wt%)

C	Si	Mn	P	S	Cr	V
0,85-0,95	0,1-0,4	1,9-2,1	0,03 max	0,03 max	0,2-0,5	0,05-0,15

After hardening a hardness of 63 to 65 HRC can be achieved. In addition, tempering to a different temperature provides a wide range of possible workpiece hardness: from 38 HRC with tempering at 600°C to 63 HRC, tempering at 100°C. [16] For the experiment, the workpiece was heat treated to the desired hardness of 58 HRC. This material is predominantly used in the manufacture of machine components such as press moulds, cold shear tools, screw taps, reamers, springs, plastic moulds, measuring and inspection tools and gauges [17].

3.2. Material to be machined – aluminium alloy

AlZn5.5MgCu is one of the strongest aluminium alloys with a tensile strength of up to 600 Mpa (often referred to as aerospace duralumin), has the highest strength and hardness of all alloys and is also characterised by excellent polishability [18]. It is mainly used where a combination of high strength and low weight is important and for highly stressed structural parts. Its chemical composition is given in Table 2.

Table 2
Chemical composition AlZn5.5MgCu (wt%)

Cr	Cu	Fe	Mg	Mn	Si	Ti	Zn
0,18-0,28	1,2-2	0,3 max	2,1-2,9	0,3 max	0,4 max	0,2 max	5,1-6,1

This material is applied in a cured state. It has reduced corrosion resistance, is well machinable, short chips are produced during machining. It achieves a hardness of approx. 135 to 161 HBW. Welding is very difficult, or even impossible, also not suitable for anodising. In technical practice, it is used wherever a combination of low weight and high strength is desired, i.e. mainly in the aerospace and automotive industries, for injection moulds and moulding of plastics, gears, shafts and control valve parts.

3.3. Material to be machined – refractory steel alloy

42CrMo4 belongs to the group of heat-resistant low-alloy steel. It is widely used in the engineering industry. It has high fatigue strength, abrasion resistance, toughness and torsional strength. It can be heat treated in many ways to provide a combination of desired properties. It is suitable for quench hardening and tempering.. After quench hardening, it forms a rigid martensitic structure due to the elements Cr and Mo, which also increase the mechanical properties of the steel such as strength, ductility and toughness [19].

Table 3
Chemical composition 42CrMo4 (wt%)

C	Mn	Si	P	S	Cr	Mo	Cu
0,38-0,45	0,6-0,9	0,1-0,4	0,025 max	0,035 max	0,9-1,2	0,15-0,3	0,4 max

This material is slightly corrosion resistant due to its low chromium content. In the annealed state, it is well machinable [20]. After heat treatment, machining is most often limited to finish grinding. It is conditionally weldable due to its high susceptibility to cracks. It is ductile in the annealed state [21], but more force is required in forming because the steel is harder than conventional carbon steel. In

engineering practice, it is widely used for its good mechanical properties, especially for the manufacture of statically and dynamically stressed components. In the automotive and aerospace industries, it is used for the manufacture of gears, crankshafts [19], also in the oil and gas industry and in the manufacture of large machinery and machine parts, for the manufacture of fasteners, shafts, steel couplings and for the manufacture of ejectors.

4 Experimental Part

The core of the presented paper is the investigation of the cutting force. Generally speaking, cutting force, in particular, gives reliable information about the total amount of generated process heat, and from an energy point of view, it is one of the most sensitive indicators of machining performance. The knowledge of the magnitude of the cutting force and its behaviour during the cutting process enables follow-up final economic-optimisation analyses of production processes, technologies and the choice of cutting tools, machine tools and cutting conditions. The presented paper also deals with the research of the generated surface because the dynamic loading of the machine-tool-workpiece system by the cutting forces also has a major influence on the stability of the cutting process, i.e. on the accuracy of the workpiece, and finally, on the quality and integrity of the machined surface.

4.1. Experiment setup

The monitoring of the machining process with a monolithic rotary tool for turning with forced rotation (Fig. 7) was carried out on a Hurco VMX 30 T machine, in which the tool is clamped in the spindle and can be positioned in the x-, y-, z-axis. The given machine does not allow tilting of the knife inclination and thus does not create the possibility for testing the angle λ_s . The monolithic knife is clamped in the controlled spindle of the machine, and the workpiece rotates by means of a KITAGAWA rotary table, located on the worktable of the machine tool.

The spindle of the KITAGAWA table did not allow the use of higher workpiece speeds than 25 min^{-1} , which does not allow a more comprehensive verification of the potential of the knife technology in the experimental work. The workpieces of the materials in question should initially test the suitability of introducing this technology using a monolithic knife in the area of further research.

4.2. Selection of cutting parameters

On the basis of a pilot verification of the forced rotation machining process, the basic cutting parameters were determined. The experiments were carried out at the specified cutting parameters so that every single material was machined and then evaluated. For every single material, at constant feed parameters and depth of cut, the design cutting speed was varied, as shown in Table 4.

Table 4. Cutting parameters used for selected materials

Material	tool cutting speed v_T [m×min ⁻¹]	workpiece rotation speed v_w [m×min ⁻¹]	depth of cut a_p [mm]	displacement f [mm]
42CrMo4	100	10	0,2	0,1
	300			
	500			
90MnCrV8	100	10	0,2	0,1
	300			
	500			
AlZn5,5MgCu	100	10	0,2	0,1
	300			
	500			

4.3. Measurement of cutting forces

During the machining process, three perpendicular components of the cutting force were measured using a stationary dynamometer. This is a measuring device designed for chip machining processes. It basically works on the principle of the piezoelectric effect, where the mechanical load on the piezoelectric sensor generates an electrical charge. The dynamometer is equipped with four sensors. Each sensor is piezoelectric and has three components, compressive and tensile forces in the F_z direction, positive and negative shear forces in the F_x and F_y directions, while the orthogonal force components are recorded simultaneously. For the 3-component measurement during machining, eight signals leading to the hub amplifiers are obtained. These contain a capacitor, and by changing its range, the range of the measured force is changed. The amplified charge signal is converted to a voltage signal which is then evaluated. The magnitude of the charge or electrical voltage is proportional to the magnitude of the applied force [22]

Table 5
Basic technical data for the three-component piezoelectric dynamometer

Property	Numerical value
Measuring range in the direction of <i>x</i> -axis	-20 to + 20kN
Measuring range in the direction of <i>y</i> -axis	-20 to + 20kN
Measuring range in the direction of <i>z</i> -axis	10 to 40 kN
Allowed operating temperature	0 to 70 °C
Actual frequency	3 kHz
Relative measurement uncertainty	1%
Measurement sensitivity	8 pC N ⁻¹

A Kistler 9255A stationary piezoelectric dynamometer was used to measure the cutting force components during turning with powered tools. The dynamometer was mounted on the table of the used machine tool. A rotary head with a chuck (Fig. 8) was mounted on the dynamometer, in which the collet with the workpiece was clamped. The monolithic tool was clamped in the spindle of the machine tool and can be positioned in *x*, *y*, *z* axes.

4.4. Surface measurement

The Alicona InfiniteFocus optical system was used to evaluate the surface of the machined surfaces. This measurement system allows microscopic measurement of the coordinates and roughness of the scanned surfaces. For the purpose of roughness measurement, measurement with sufficiently high accuracy and repeatability can be applied. The measured workpiece sample was first set up on the instrument workbench under the confocal microscope (Figure 9). After the alignment and proper illumination of the measured sample, a scan of the sample surface was performed. The scanned surface of the part was then flattened using the system, and the roughness parameters R_a , R_z , R_q were evaluated from the scanned data.

Under the defined conditions, the surface roughness was measured on the evaluated length of 4 mm for the machined surface. There were five basic length measurements for determining the roughness parameters with a length of 0.8 mm. Surface measurements were performed for all materials (tool steel, duralumin steel, quenched steel) and all cutting speeds used (100 m·min⁻¹, 300 m·min⁻¹, 500 m·min⁻¹). The cutting parameters of the depth of cut $a_p = 0.2$ mm and feed values $f = 0.1$ mm were maintained for all materials.

5 Results

The results of the measurement of cutting force components during machining are presented, the resulting cutting forces and machined surfaces are compared and the influence of cutting parameters is assessed.

5.1 Components of cutting force in machining

Figure 10 illustrates the directly measured cutting force components F_x , F_y , F_z for the machined material AlZn5.5MgCu. The sampling frequency of the dynamometer was 5000 Hz. The total cutting force F was calculated from these measured data, the values of which are then exported using Matlab.

As shown in Figure 10, the measurement itself captures the entire machining process from the first tool-workpiece contact to the completion of chip cutting. For this reason, only a slice of the measurement record that presents the chip machining itself was analysed.

In the case of the measurement of the cutting force components for the machined materials 90MnCrV8 and 42CrMo4, the procedure was identical.

5.2 Comparison of the resulting cutting forces

Based on the obtained cutting force data from the machining process, a graphical comparison of the resulting cutting force in the machining process for each material and cutting speed was created. The results of the experiment are shown in Figure 11.

The achieved cutting forces at the individual tool rotation speeds for machining AlZn5.5MgCu were in the low range up to 50 N. When the rotation speed of the monolithic tool was increased, the cutting force decreased up to 35 N at a tool rotation speed of $500 \text{ m}\cdot\text{min}^{-1}$.

The mean cutting force values in the individual machining experiments for 42CrMo4 were very similar. The visible difference of the individual tool rotation speed settings is in the variance of the measured force values. For a tool rotation speed of $300 \text{ m}\cdot\text{min}^{-1}$, it ranges from 35 N to 77 N. This variance of values is the highest of the experimental measurements performed.

When machining the hardest material, which was 90MnCrV8, the values of the total cutting force were in the range of $90 \text{ N} \pm 5 \%$ at a tool cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$. Higher values of the total cutting force and also a dispersion of values were observed when machining at lower tool rotation speeds. Based on these data, we can assume that the monolithic tool can be used for machining materials with enhanced mechanical properties under properly specified cutting conditions.

5.3 Comparison of the machined surface

In the image of the enlarged surface of AlZn5.5MgCu, square and hexagonal tool marks can be seen after machining under the given conditions. These marks and their character are determined by the resulting direction of the main cutting motion. The surface formed at a cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$ was different from the other cutting speeds and had a hexagonal structure. The hexagonal features are distributed over

the entire surface of the machined material and can be formed by the worn part of the tool. During rotary turning of 42CrMo4 at a cutting speed of $100 \text{ m}\cdot\text{min}^{-1}$, the surface showed diamond-shaped machining marks, in which elliptical traces of the circular cutting edge of the tool appeared on the colour map. The resulting cutting motion vector gives the overall orientation direction of these traces. For a steel workpiece machined with a rotary tool at a cutting speed of $300 \text{ m}\cdot\text{min}^{-1}$, the tool marks have a striped character with fine rectangular shapes. The direction recorded by the colour map shows the vector of the resulting cutting motion. In the images of the surface machined at a cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$, the layered tool marks of the rotary tool can be seen after high-speed machining. At the high cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$, the shape of the machining marks is different for steel compared to the other two lower cutting speeds. This effect was evident in the machining of AlZn5.5MgCu. For the 90MnCrV8 material machined at a cutting speed of $100 \text{ m}\cdot\text{min}^{-1}$, rectangular strip formations appear on the surface, the direction of which is also determined by the vector of the resulting cutting motion. The width of the strip is defined by the knife geometry and the feed rate. Images of the machined surface at a cutting speed of $300 \text{ m}\cdot\text{min}^{-1}$ show finely textured rectangular layers. Their direction is determined by the resulting main cutting motion vector. The structure is finer but similar for identical parameters of 42CrMo4 steel.

From the recorded surfaces (Figure 12) and their roughness (Figure 13), it can be concluded that the monolithic knife and the overall technology is suitable for the implementation of high-speed machining. The machined surfaces generally have relatively low roughness values using the given parameters. By improving the overall technological system of a given process (such as increasing the frequency of rotation of the workpiece), the roughness values could be improved for the technology used.

5.4 Influence of cutting machining parameters

In order to determine the cutting parameters, a pilot experiment was carried out to obtain basic data on the cutting force in the forced rotation machining process. The cutting parameters used were chosen within the ranges shown in Table 6 due to the system and machine stiffness. In this experiment, the effect of the rotation direction of the tool with respect to the workpiece was also investigated, where negative rotation speeds indicate a counterclockwise orientation, and positive speeds present a clockwise rotation orientation.

Table 6
Selected cutting parameters with respect to the system and machine stiffness

$v_w \text{ (m}\cdot\text{min}^{-1})$	$v_T \text{ (m}\cdot\text{min}^{-1})$	$a_p \text{ (mm)}$	$f \text{ (mm)}$
100 - 200	50 - 200	0.25 - 0.75	0.05 - 0.15

The effects of the factors v_w , v_b , f , and a_p were analysed by the response surface method. The aim was to intensify the individual parameters and their dependence on the magnitude of the cutting force F . After the experiments were completed, the experimental data were subjected to statistical processing (Table 7).

The analysis of variance (Table 7) of the total cutting force F shows that the most significant effect is achieved by the depth of cut a_p , which directly influences the size of the material removed during machining. According to the linear model, the influence of a_p size on cutting force F reaches 24.55%. The workpiece rotation speed v_w has the smallest influence on the F size of cutting force (0.20%). Also, the feed size f cannot be considered statistically significant as its influence on the change of cutting force F reaches the value of 0.64%. The accuracy of the mathematical model reaches 90.60% with a prediction coefficient of 85.09%. From the above data, it is possible to construct the response surface equation F (1):

$$F = 583 - 0.09 v_w + 0.088 v_t - 1715 a_p - 1710 f - 0.00103 v_w^2 + 0.005289 v_t^2 + 2187 a_p^2 + 10450 f^2 + 0.00007 v_w \cdot v_t - 0.297 v_t \cdot a_p - 2.27 v_t \cdot f \quad (1)$$

Table 7. Analysis of variance output for total cutting force F

Source	DF	Contribution (%)	Adj SS	Adj MS	F-Value	P-Value
Model	11	90.60	823072	74825	38.53	0.000
Linear	4	34.21	310365	77591	39.96	0.000
v_w	1	0.20	6320	6320	3.25	0.078
v_t	1	8.83	75248	75248	38.75	0.000
a_p	1	24.55	223020	223020	114.84	0.000
f	1	0.64	5776	5776	2.97	0.092
Square	4	55.78	506762	126691	65.24	0.000
$v_w \cdot v_w$	1	5.59	32	32	0.02	0.898
$v_t \cdot v_t$	1	34.76	315782	315782	162.61	0.000
$a_p \cdot a_p$	1	15.03	99645	99645	51.31	0.000
$f \cdot f$	1	0.40	3640	3640	1.87	0.178
2-Way Interaction	3	0.61	5526	1842	0.95	0.425
$v_w \cdot v_t$	1	0.00	4	4	0.00	0.964
$v_t \cdot a_p$	1	0.18	1658	1658	0.85	0.361
$v_t \cdot f$	1	0.43	3865	3865	1.99	0.165
Error	44	9.40	85445	1942		
Total	55	100				

A graphical interaction (Fig. 14) of the selected cutting parameters was constructed from the experimentally obtained data and the subsequent mathematical model. When the graphical representation is used, the influence of the two cutting parameters on the total cutting force F can be clearly observed. One of the investigated parameters was the tool rotation v_t . For identical tool rotation speed and different rotation directions, the magnitude of the total cutting force is affected by 50N. For the parameter $a_p = 0.75$ (mm), there was an increase in the cutting force of 100N when the direction of rotation was changed. From the above, it can be seen that the direction of rotation of the tool itself has an effect on the cutting force.

With a properly selected tool rotation, it would be possible to apply cutting parameters (a_p, f) to increase machining productivity compared to productivity in the opposite direction of tool rotation.

6 Discussion

When the given results are compared, it can be concluded that the new designed monolithic tool shows a possible application for machining a wide range of materials. The prototype design of the monolithic tool eliminates possible assembly shortcomings and inaccuracies in the manufacture of complex tools consisting of multiple components. The main advantage is the absence of the clamping mechanism of the interchangeable cutting insert, thus guaranteeing the alignment of the cutting and clamping parts of the tool.

When observing the dynamics of the cutting forces, the oscillatory nature of the progress of the individual components was observed, which is influenced by several input factors. One influencing factor includes the possibility of improving the technological system, such as supporting the workpiece in the working space of the machine. This effect certainly influenced the overall quality of the machining process. The increase in the frequency of rotation of the machined material, which was limited by the mechanical equipment of the working area, would also have a positive effect. By increasing the workpiece rotation frequency, the tool rotation speed would be reduced, and the cutting conditions would be improved with respect to the cutting speed.

For AlZn5.5MgCu duralumin workpiece, the selected roughness parameters also increased with increasing speed. When the cutting speed was changed from $100 \text{ m}\cdot\text{min}^{-1}$ to $300 \text{ m}\cdot\text{min}^{-1}$, the increase in roughness parameters was low. At a cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$, the roughness value increased exponentially by about 40%. The difference in surface texture at a cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$ was also evident from the surface images (colour map of the surface – hexagonal texture). The measured parameters of the 42CrMo4 tough steel no longer increased upwards, but at a cutting speed of $300 \text{ m}\cdot\text{min}^{-1}$, the selected roughness parameters were lower than at $100 \text{ m}\cdot\text{min}^{-1}$. The highest measured roughness parameters were again found at a cutting speed of $500 \text{ m}\cdot\text{min}^{-1}$. Between the values of the cutting speed parameters of $300 \text{ m}\cdot\text{min}^{-1}$ and $500 \text{ m}\cdot\text{min}^{-1}$, there was again a step increase in the results. For hardened 90MnCrV8 steel hardened to 58 HRC, an upward increase in the evaluated roughness parameters with respect to cutting speed was observed. For this case, there was no stepwise increase in roughness. It can be concluded that the technology used is suitable for the application of machining quenched materials with respect to the roughness of the machined surface and the overall machining process. For quenched steel, better results of roughness parameters were obtained than for tough steel.

7 Conclusion

In the presented study, the suitability of the application of a new proposed monolithic tool designed for ADRT technology applications was investigated. Tools for such a kinematic scheme are currently not

commercially available. Different prototypes of clamping systems for interchangeable cutting inserts and their actual production can be time-consuming and costly. Also, setting the concentricity of the indexable cutting insert against the clamping part is demanding in terms of metrology equipment and personnel alone. This work aimed to verify a new proposed monolithic tool, which is patent pending. The given type of the proposed tool eliminates the shortcomings mentioned above of the design of tools assembled from multiple components. The identification of the applicability of the monolithic tool was carried out on three selected machined materials with different mechanical properties, representing the groups of tough and difficult to machine materials.

For the basic determination of the cutting parameters, an experiment was carried out, which took into account the stiffness of the system and the possibilities of controlling the individual cutting parameters. Based on these data, the cutting parameters were determined and subsequently applied in the machining process. Experimental verification confirmed that the monolithic tool and the proposed technology are suitable for the implementation of high-speed machining under properly set cutting conditions for the reason that the maximum cutting force achieved did not reach such values that would result in fatal damage to the tool. Changes in the total cutting force as well as in the resulting surface roughness were observed when the tool rotation speed was changed. While the magnitude of the cutting force was most affected by the material type, where there is a noticeable increase in force from the deteriorating machinability of the material. For AlZn5.5MgCu and 90MnCrV8 materials, a decrease in cutting force can be observed as the tool rotation frequency increases. Higher tool rotation speed also had a positive effect on the resulting surface roughness, where for quenched steel 90MnCrV8, lower values of surface roughness parameters were obtained at a rotation speed of 500 m.min⁻¹ compared to AlZn5.5MgCu and 42CrMo4 materials. Also, the direction of tool rotation itself affects the overall cutting force in the machining process. Thus, with a properly selected rotation direction, a reduction in cutting force can be achieved, which in practice allows other cutting parameters to be adjusted in order to increase machining productivity.

Based on the presented results, it can be assumed that the new type of monolithic tool exhibits stable properties and that its use in broader engineering practice will be successful.

Declarations

Author contribution Andrej Czán: Conceptualization and Project administration; Richard Joch: Investigation, data curation and writing – review and editing; Michal Šajgalík: Investigation and methodology; Jozef Holubják : Validation; Andrej Horák : Validation; Pavol Timko: Validation; Jan Valíček : writing – review and editing; Milena Kušnerová : writing – review and editing; Marta Harničárová : formal analysis and writing – review and editing

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Competing interests The authors reported no potential conflict of interest.

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Figures

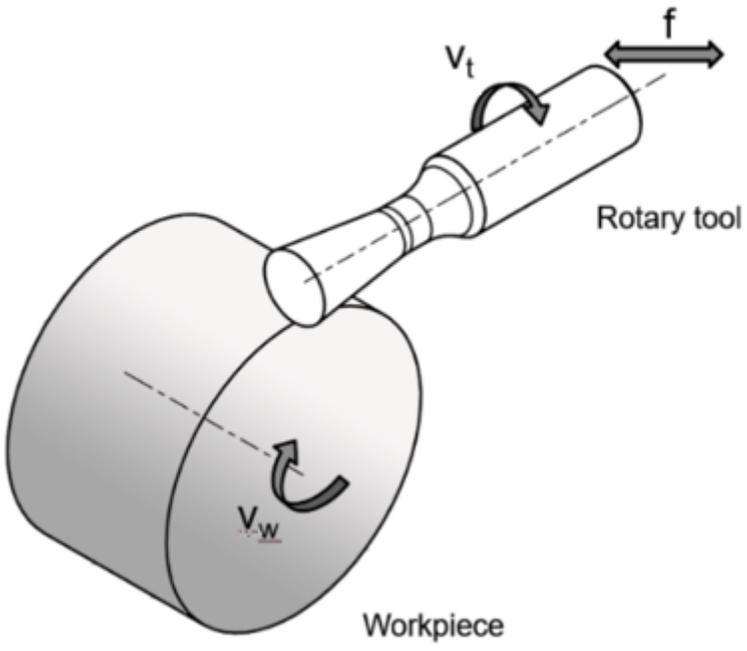


Figure 1

Kinematic diagram of ADRT

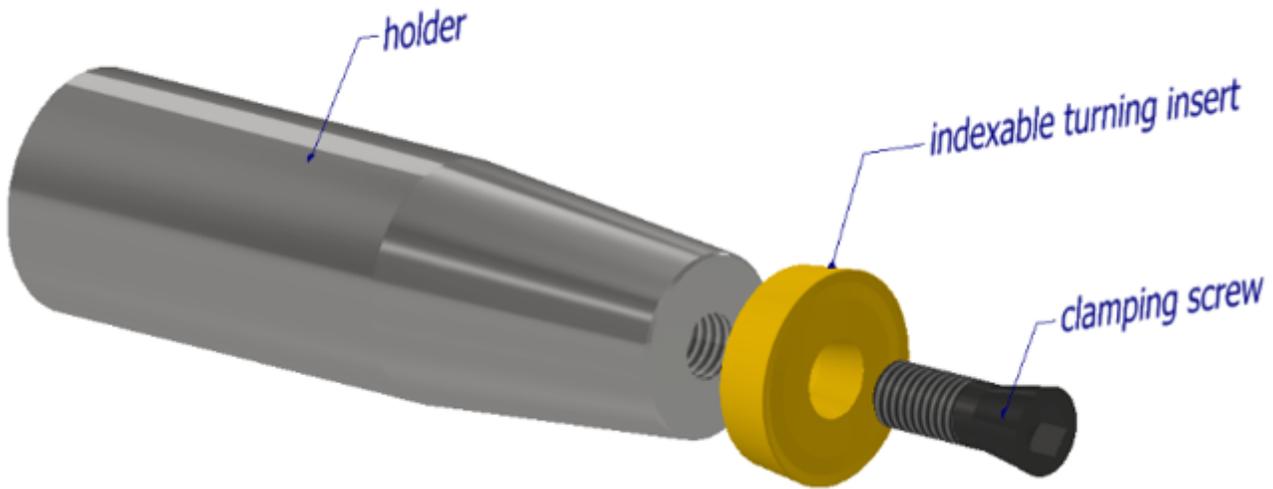


Figure 2

Design of rotary tool

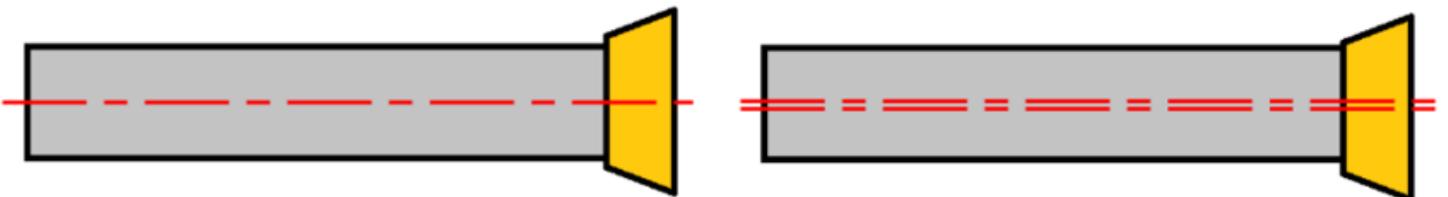


Figure 3

Inaccuracy of the cutting insert fit against the clamping part

Figure 4

The tapered screw clamping mechanism of the cutting insert

Figure 6

Monolithic rotary tools for forced rotation machining

Figure 7

Visualisation of the tool setup and machining process of a monolithic rotary tool

Figure 8

Schematic wiring of the cutting force component measurement assembly

Figure 9

Setting up the measured sample

Figure 10

Components of the measured cutting force in machining AlZn5.5MgCu

Figure 11

Graphical comparison of the total cutting force for each experiment

Figure 12

Record of machined surfaces

Figure 13

Graphical representation of surface roughness parameters

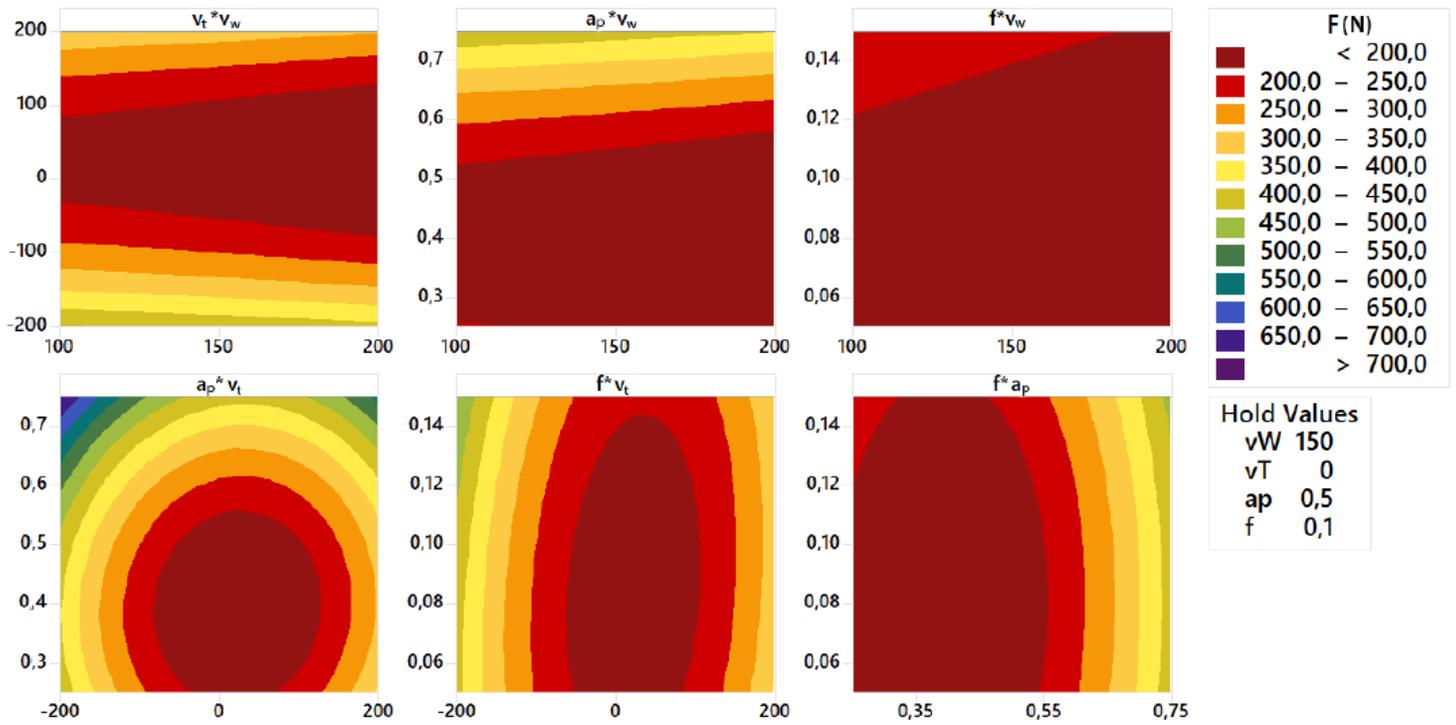


Figure 14

Graphical representation of the total cutting force in the machining process as a function of the individual cutting parameters