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ABSTRACT

The process of thin films is commonly utilized to improve the surface characteristics of materials. A thin film helps to improve the absorption, depreciation, flexibility, lighting, transport, and electromagnetic efficiency of a bulk material medium. Thin film treatment can be especially helpful in nanotechnology. As a result, the current study investigates the computational process of heat relocation analysis in a thin-film MHD flow embedded in hybrid nanoparticles, which combines the spherical copper and alumina dispersed in ethylene glycol as the conventional heat transfer Newtonian fluid model over a stretching sheet. Important elements such as thermophoresis and Brownian movement are used to explain the characteristics of heat and mass transfer analysis. Nonlinear higher differential equations (ODEs) were attained by transforming partial differential equations (PDEs) into governing equations when implementing the similarity transformation technique. The resulting nonlinear ODEs have been utilized by using the homotopy analysis method (HAM). The natures of the thin-film flow and heat transfer through the various values of the pertinent parameters: unsteadiness, nanoparticle volume fraction, thin-film thickness, magnetic interaction and intensity suction/injection are deliberated. The approximate consequences for flow rate and temperature distributions and physical quantities in terms of local skin friction and Nusselt number were obtained and analysed via graphs and tables. As a consequence, the suction has a more prodigious effect on the hybrid nanofluid than on the injection fluid for all the investigated parameters. It is worth acknowledging that the existence of the nanoparticles and MHD in the viscous hybrid nanofluid tends to enhance the temperature profile but decay the particle movement in the thin-film flow. It is perceived that the velocity and temperature fields decline with increasing unsteadiness, thin-film thickness and suction/injection parameters.

Keywords: Magneto-hydrodynamic flow, Cu and Al₂O₃, Heat source; HAM solutions, Permeable stretching sheet, Ethylene glycol.

1. INTRODUCTION

In research and manufacturing processes such as wire drawing, injection moulding, deformation, and powder metallurgy, the analysis of fluid stream stretching surfaces is crucial. Crane [1] was the first to analyse and procure the similarity solution for continuous stream beyond a stretching sheet. In comparison to the elongating case, regrettably, the movement past a shrinking surface has received little attention. According to Goldstein [2], the shrinking module's flow is essentially backward. Miklavi and Wang investigated an accurate clarification of the Navier Stokes equations over a decreasing sheet in their paper [3]. Investigators observed that the flow field inside a transition zone is not restricted, and by providing sufficient

suction at the edge, a continuous flow may be achieved. A contracting sheet flow exhibits different physical processes than a stretched sheet flow, according to Fang et al. [4]

Recently, the issue of heat transfer improvement has received much attention. Thermoelectric scientists have proposed that nanotube metallic or nonmetallic materials be added to the conventional fluids to increase thermal properties since nanoparticles have a better thermal conductivity than to the base liquid. A Nanofluid is the resultant mixture that has improved physiochemical properties. Aziz [5] developed the terminology of nanofluids for the first time in 1995. Furthermore, a special type of nanofluid known as a hybrid nanofluid is studied to boost the thermal efficiency. Hybrid nanocomposites are upgraded nanofluids made up of two unique nanomaterials, whereas ordinary nanofluids are made up of a single nanoparticle that absorbs in conventional fluids. The thermal properties of hybrid nanofluids are improved, which improves the heat transmission performance.

Numerous researchers have investigated the boundary layer convection moment of hybrid nanofluids. For illustration, Devi and Devi [6, 7] studied the dynamics of a hybrid nanofluid across a stretchable sheet by contemplating Cu-Al₂O₃ nanotubes with and without electric field effects. They discovered that hybrid nanofluids outperform consistent nanofluids in terms of heat flux. Countless researchers [8-14], have recently investigated the mixed convection flow aspects of hybrid nanofluids by recognising various characteristics in publications.

The thin-film flow problem is an important aspect of the microfluidics industry, as it creates physical items with micrometre to millimetre dimensions. Electrical equipment with ferromagnetic metals that enable electric current to flow and diagnostic implants are using synthetic films to impede bacterial activity are commercial examples of that use thin layers flows. As a result of these practices, researchers were inspired to investigate and examine the different effects of thin film flow through transferring aligned, lateral, and sloped flat sheets on heat exchange. Furthermore, the primary applications of these thin-film flows are draining, encapsulating, hydrating, microbiological, and photovoltaic cells as pointed out by Bertozzi [15], Roy et al. [16], Dutta et al. [17], Taherzadeh [18], Liu et al. [19], Kreder et al. [20], Girtan [21, 22] and Thiele [23]. It is investigated through the "Thin-Film Decomposition" algorithm, which involves putting a thin-film to a surface to be covered [24].

Wang [25] investigated the first problem of this phenomenon without taking into account heat transmission. This study was conducted for Newtonian fluids, which was prompted by the work of Sakiadis [26], Crane [27], and Carragher and Crane [28], who investigated a conceptual technique for solving heat/mass transfer through elongating surfaces. The study discovered that the Navier-Stokes unsteady problem requires a remarkably precise exact solutions and an examination of integration. As a result, Andersson et al. [29] began an investigation on the basis of Wang's [25] solution towards the hemodynamic heat transport problem and introduced the similarity transformations for the thermal radiation equation.

The demand for characterised gadgets with the finest performances and optimum functionality is rising as science and technology progress. As a result, the researcher explored nanofluids to describe a new category of fluids made up of nanoparticles. Choi [30] hypothesized that in a fluid, metallic or nonmetallic atoms with in height current conductivity enhance the quality of heat transport. Because of their unique features, the presence of nanoparticles in a system can increase the

efficiency of heat and working fluid parameters. When nanoparticles and base fluid are combined, the simmering performance is reduced and deterioration is increased. Most notably, it smooths the surface of nucleate sites, resulting in significant thermophysical coefficient degradation. Khan and Pop [31], Yirga and Shankar [32], Pourmehran et al. [33], Jahan et al. [34], Hafidz et al. [35], and Gangadhar et al. [36] are some of the scholars and scientists who have reported the MHD movement and analysis of heat in a steady porous medium under the influence of viscous dissipation and chemical reaction. The similarity equations were solved by implementing the Keller-box scheme.

Krishna and Chamkha [37, 38], and Chamkha et al. [39] investigated nanofluid MHD regarding suction/injection effects for various geometries. According to these studies, the suction effect increases the heat transmission of the nanofluid. Hazarika et al. [40] examined the thermal characteristics and viscous dissipation of magnetohydrodynamic nanofluids through a permeable stretched surface. The authors mention the copper, Argentum and forum (III) oxide as the nanoparticles. Chamkha et al. [41] used the numerical method to investigate the phenomenon of nanostructures in natural convection flow. Dogonchi et al. [42] used a similar strategy to solve the mathematical modelling of magnetohydrodynamic nanofluids in permeable media regarding Brownian motion. Furthermore, Dogonchi et al. [43] suggested that enhancing the suction constraint causes a rise in moment but a decrease in nanofluid temperature.

Moreover, while employing the 90:10 ratio concentration of water, the numerical model for thermal conductivity was compared with experimental data reported by Waini et al. [44]. Various volume fraction nanoparticles, such as 0.1 percent, 0.33 percent, 0.75 percent, 1 percent, and 2 percent, provide excellent agreement with the experimental findings during this research. An increase in the nanoparticle volume fraction from 0.005 to 0.06 improves the temperature field, causing overshoot the heat transfer of the fluid. Despite this, the velocity profile and wall shear stress were both delayed. Waini et al. [45, 46] investigated similar combinations of nanoparticles with different effects on stretchable sheets. Furthermore, Ghalambaz et al. [47] reported that the existence of the hybrid nanomaterial has an optimistic consequence on the heat transfer of a hybrid nanofluid. Tayebi and Chamkha [48] conducted a numerical analysis of the steady MHD ordinary convective rate of heat transfer and stream on hybrid nanofluids, alumina and copper dissolved in water as a Newtonian fluid model.

Furthermore, various factors such as the prevalence of MHD and eating sources in fluids, drew the attention of industry, particularly engineering, who wanted to learn more about fluid flow and innovation in varied geometries. Veera et al. [49, 50] investigated second-grade fluid using MHD and Hall effects in a permeable material between two vertical plates. Krishna et al. [51] examined the features of heat transmission on magnetic field boundary layer movement of second grade fluid with the permeable channel subjected to a perpendicular stretchable sheet. Veera et al. [52] examined the properties of MHD, ion slip, and the porosity parameter on an unsteady generating/absorbing second-grade fluid.

After examining the literature, we were inspired to use the Tiwari and Das [53] nanofluid framework to explore the behaviour of hybrid nanofluid heat/mass transfer via a transparent stretching/shrinking surface subject to a thin-film MHD flow. Copper and alumina nanoparticles are used in this study. The nanoparticles are then immersed in ethylene glycol, resulting in a hybrid nanofluid. The current analytical results are validated by comparing them to previously published data.

2. MATHEMATICAL FORMULATION

The MHD flow of thin-films with hybrid nanofluids over a stretching surface of a laminar boundary layer with porous medium is considered. Two-dimensional flow is considered in this study. The stretching sheet at the x -axis with velocity $U_w = \frac{bx}{(1-\alpha t)}$ and y is normal to the sheet leading to the fluid flow in the thin-film

with uniform thin-film thickness $h(t)$. The sheet is supposed to have a mass transport parameter with velocity of the suction/injection velocity $V_w = \frac{(V_w)_0}{(1-\alpha t)^{\frac{1}{2}}}$, and sheet

temperature $T_w = T_0 - T_{ref} \left(\frac{bx^2}{2\nu} \right) (1-\alpha t)^{-\frac{3}{2}}$ fluctuates with length x along with sheet.

Here, $(V_w)_0$ it corresponds to the initial velocity suction/injection parameter, T_0 stands for the variable of slit temperature and T_{ref} is the reference temperature. Furthermore, $\alpha > 0$ and $b > 0$ are taken for the following analyses and are valid only for a time $t < \alpha^{-1}$. The geometry of the present work is portrayed in figure 1.

Figure 1 Geometry of the model

The governing equations for electrically conducting viscous hybrid nanofluids with the breadth of the Tiwari and Das [53] framework for hybrid nanofluids can be stated as

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad (1)$$

$$\left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right) = \frac{\mu_{hnf}}{\rho_{hnf}} \frac{\partial^2 u}{\partial y^2} + \frac{\sigma_{hnf}}{\rho_{hnf}} B^2(t) u, \quad (2)$$

$$\left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) = \frac{k_{hnf}}{(\rho c_p)_{hnf}} \frac{\partial^2 T}{\partial y^2}, \quad (3)$$

Subject to [16]:

$$u = U_w, v = V_w, T = T_w; \text{ at } y = 0, \text{ and } \frac{\partial u}{\partial y} = \frac{\partial T}{\partial y} = 0, v = \frac{dh}{dt}, \text{ at } y = h. \quad (4)$$

Here, u, v are the velocity components along the x and y directions, k_{hnf} is the thermal conductivity of the hybrid nanofluid, ρ_{hnf} is the density, $(C_p)_{hnf}$ is the energy, μ_{hnf} is the dynamic viscosity, σ_{hnf} is the electrical conductivity of the hybrid nanofluid, and T and t explore the temperature and time. The effect of the Lorentz force is negligible. The polarization of charges on an electric field is taken to be zero.

The $B(t)$ for the flow under this investigation will be taken as $B(t) = B_0(1 - \alpha t)^{\frac{1}{2}}$.

Table 1 is used to estimate the thermophysical properties of nanofluids and hybrid nanofluids as reported by Tiwari and Das [53] and Oztop and Abu-Nada [54]. Similarly, as described by Oztop and Abu-Nada [54], Table 2 lists the physical parameters of the nanoparticles and the base fluid with 30% ethylene glycol.

Table 1. Thermo-physical properties [53, 54].

PROPERTIES	NANOFLUID	HYBRID NANOFLUID
DENSITY	$(\rho C_p)_{nf} = (1 - \phi_1)(\rho C_p)_f + \phi_1(\rho C_p)_{s_1}$	$\sigma_{nf} = \left[\frac{\sigma_{s_1} + 2\sigma_{nf} - 2\phi_1(\sigma_{nf} - \sigma_{s_1})}{\sigma_{s_1} + 2\sigma_{nf} + \phi_1(\sigma_{nf} - \sigma_{s_1})} \right] \sigma_{nf}$
HEAT CAPACITY	$\rho_{nf} = (1 - \phi_1)(\rho)_f + \phi_1(\rho)_{s_1}$	$(\rho C_p)_{hnf} = (1 - \phi_2)(1 - \phi_1)(\rho C_p)_f + \phi_1(1 - \phi_2)(\rho C_p)_{s_1} + \phi_2(\rho C_p)_{s_2}$
VISCOSITY	$\mu_{nf} = \frac{\mu_f}{[1 - \phi_1]^{2.5}}$	$\mu_{hnf} = \frac{\mu_f}{[(1 - \phi_1)(1 - \phi_2)]^{2.5}}$
THERMAL CONDUCTIVITY	$K_{nf} = \left[\frac{k_{s_1} + 2k_f - 2\phi_1(k_f - k_{s_1})}{k_{s_1} + 2k_f + \phi_1(k_f - k_{s_1})} \right] K_f$	$K_{hnf} = \left[\frac{k_{s_2} + 2k_{nf} - 2\phi_2(k_{nf} - k_{s_2})}{k_{s_2} + 2k_{nf} + \phi_2(k_{nf} - k_{s_2})} \right] K_{nf}$ where $K_{nf} = \left[\frac{k_{s_1} + 2k_f - 2\phi_1(k_f - k_{s_1})}{k_{s_1} + 2k_f + \phi_1(k_f - k_{s_1})} \right]$

Table 2 Thermo-physical properties of the base fluid and nanoparticles [53, 54]

Physical properties	Water plus 30% ethylene glycol	Cu	Al ₂ O ₃
C_p (Jkg ⁻¹ K ⁻¹)	3714	385	765
ρ (kgm ⁻³)	1038	8933	3970
k (Wm ⁻¹ K ⁻¹)	0.484	400	400
σ (s/m)	0.00276	5.96×10^6	35×10^6

Following Tiwari and Das [53], we look for a similarity solution of equations (1) -(4) by using the following similarity variables:

$$\psi = \left[\nu b (1 - \alpha t)^{-1} \right]^{\frac{1}{2}} x \xi f(\eta), \quad \eta = \left(\frac{\nu}{b} \right) (1 - \alpha t)^{-\frac{1}{2}} \xi^{-1} y,$$

$$T = T_0 - T_{ref} \left(\frac{bx^2}{2\nu} \right) (1 - \alpha t)^{-\frac{3}{2}} \theta(\eta), \quad (5)$$

where the stream function defined by ψ with $u = \frac{\partial \psi}{\partial y}$ and $v = -\frac{\partial \psi}{\partial x}$ satisfies (1)

identically, therefore, we have

$$u = \frac{bx}{(1 - \alpha t)} f', \quad v = -\left(\frac{\nu b}{1 - \alpha t} \right)^{\frac{1}{2}} \xi f. \quad (6)$$

Equation (5) into equations (2) and (3), we obtain similarity equations in ordinary differential form:

$$\left(\frac{1}{[1 - (\phi_1 + \phi_2)]^{2.5}} \right) f''' + \left[\frac{(1 - \phi_2) \phi_1 \frac{\rho_{s_1}}{\rho_{nf}} + \phi_2 \frac{\rho_{s_2}}{\rho_{nf}} + (1 - \phi + \phi_1 \phi_2)}{\rho_{nf}} \right] f'' +$$

$$\lambda \left[\begin{aligned} &ff'' - f'^2 - S \left(f' + \frac{1}{2} \eta f'' \right) \\ &- \left(\frac{[(1 - \phi_2) \phi_1 \frac{\rho_{s_1}}{\rho_{nf}} + \phi_2 \frac{\rho_{s_2}}{\rho_{nf}} + (1 - \phi + \phi_1 \phi_2)]}{\left[\frac{\sigma_{s_2} + 2\sigma_{nf} - 2\phi_2(\sigma_{nf} - \sigma_{s_2})}{\sigma_{s_2} + 2\sigma_{nf} + \phi_2(\sigma_{nf} - \sigma_{s_2})} \right] \left[\frac{\sigma_{s_1} + 2\sigma_{nf} - 2\phi_1(\sigma_{nf} - \sigma_{s_1})}{\sigma_{s_1} + 2\sigma_{nf} + \phi_1(\sigma_{nf} - \sigma_{s_1})} \right]} \right) Mf' \end{aligned} \right] = 0, \quad (7)$$

$$\left(\frac{\left[\frac{k_{s_2} + 2k_{nf} - 2\phi_2(k_{nf} - k_{s_2})}{k_{s_2} + 2k_{nf} + \phi_2(k_{nf} - k_{s_2})} \right] \left[\frac{k_{s_1} + 2k_{nf} - 2\phi_1(k_{nf} - k_{s_1})}{k_{s_1} + 2k_{nf} + \phi_1(k_{nf} - k_{s_1})} \right]}{\left[(1-\phi_2)\phi_1 \frac{(\rho c_p)_{s_1}}{(\rho c_p)_{bf}} + \phi_2 \frac{(\rho c_p)_{s_2}}{(\rho c_p)_{bf}} + (1-\phi + \phi_1\phi_2) \right]}, \Pr^{-1} \theta'' \right) + \lambda \left[-S \left(\frac{3}{2} \theta + \frac{1}{2} \eta \theta' \right) - 2f'\theta + f\theta' \right] = 0.$$

Subject to:

$$f'(0)=1, \quad f(0)=w, \quad \theta(0)=1; \quad \text{at } \eta=0, \quad (8)$$

$$f''(1)=0, \quad \theta'(1)=0, \quad f(1)=\frac{S}{2}; \quad \text{at } \eta=1.$$

Here, λ is the thin film thickness, unsteadiness of the dimensionless measure is denoted by S , $\Pr$ is the Prandtl number, suction/injection parameter is presented by w and the magnetic interaction parameter, M and are defined as

$$\lambda = \xi^2, \quad S = \frac{\alpha}{b}, \quad \Pr = \frac{(\mu c_p)_{bf}}{k_{bf}}, \quad w = -\frac{(V_w)_0}{\xi \sqrt{\nu b}}, \quad M = \frac{\sigma_{bf} B_0^2}{\rho_{bf} b}.$$

Equations (7) and (8) in simple form can be written as:

$$\left(\frac{\chi_1}{\chi_2} \right) f''' + \lambda \left[ff'' - f'^2 - S \left(f' + \frac{1}{2} \eta f'' \right) - \left(\frac{\chi_3}{\chi_4} \right) M f' \right] = 0, \quad (9)$$

$$\left(\frac{\chi_5}{\chi_6} \right) \Pr^{-1} \theta'' + \lambda \left[-S \left(\frac{3}{2} \theta + \frac{1}{2} \eta \theta' \right) - 2f'\theta + f\theta' \right] = 0. \quad (10)$$

where

$$\begin{aligned} \chi_1 &= \frac{1}{[1 - (\phi_1 + \phi_2)]^{2.5}}, \quad \chi_2 = \left[(1-\phi_2)\phi_1 \frac{\rho_{s_1}}{\rho_{nf}} + \phi_2 \frac{\rho_{s_2}}{\rho_{nf}} + (1-\phi + \phi_1\phi_2) \right], \\ \chi_3 &= \left[\frac{\sigma_{s_2} + 2\sigma_{nf} - 2\phi_2(\sigma_{nf} - \sigma_{s_2})}{\sigma_{s_2} + 2\sigma_{nf} + \phi_2(\sigma_{nf} - \sigma_{s_2})} \right] \sigma_{nf}, \quad \text{where } \sigma_{nf} = \left[\frac{\sigma_{s_1} + 2\sigma_{nf} - 2\phi_1(\sigma_{nf} - \sigma_{s_1})}{\sigma_{s_1} + 2\sigma_{nf} + \phi_1(\sigma_{nf} - \sigma_{s_1})} \right], \\ A_4 &= \frac{(1-\phi_2)[(1-\phi_1)\rho_{bf} + \phi_1\rho_{s_1}] + \phi_2\rho_{s_2}}{\rho_{bf}}, \quad \chi_5 = \left[\frac{k_{s_2} + 2k_{nf} - 2\phi_2(k_{nf} - k_{s_2})}{k_{s_2} + 2k_{nf} + \phi_2(k_{nf} - k_{s_2})} \right] K_{nf} \\ K_{nf} &= \left[\frac{k_{s_1} + 2k_{nf} - 2\phi_1(k_{nf} - k_{s_1})}{k_{s_1} + 2k_{nf} + \phi_1(k_{nf} - k_{s_1})} \right], \quad \chi_6 = \left[(1-\phi_2)\phi_1 \frac{(\rho c_p)_{s_1}}{(\rho c_p)_{bf}} + \phi_2 \frac{(\rho c_p)_{s_2}}{(\rho c_p)_{bf}} + (1-\phi + \phi_1\phi_2) \right], \end{aligned}$$

Physical quantities: Interestingly, important physical measurements such as surface drag which denotes the wall shear stress, and the rate of heat transport which denotes through the Nusselt number are defined as

$$C_f \text{Re}^{\frac{1}{2}} = \frac{1}{\delta} \left[\frac{1}{(1-\phi_1)^{2.5} + (1-\phi_2)^{2.5}} \right] f''(0), \quad (11)$$

$$Nu_x \text{Re}^{-\frac{1}{2}} = -\frac{1}{\delta} \left(\frac{k_{hmf}}{k_f} \right) \theta'(0).$$

where Reynold number, $\text{Re} = \frac{xu_w}{\nu_f}$.

3. HAM SOLUTIONS

In several physical problems, the consequent differential equations are significantly nonlinear. It is challenging for investigators and scientists to compute analytical or numerical approaches to such situations. For estimating the series solution of nonlinear partial and ordinary differential equations, the homotopy analysis method (HAM) is one of the most successful computational methods. Without the use of a greater or smaller parameter, this method can be utilized to solve severely nonlinear events. This method allows you to choose and alter the confluence area and estimate rate with a great deal of freedom. The homotopy analysis technique is efficient over typical computational methods in that it avoids the rounded-off errors that are caused by the discretization procedure. This method has been used to solve a variety of nonlinear science and engineering issues [39–43]. Let us develop some reasonable assumptions about f and θ profiles.

$$f_0(\eta) = \frac{1}{4} [4w + 4\eta + (3S - 6w - 6)\eta^2 + (2 - S + 2w)\eta^3], \theta_0(\eta) = 1. \quad (12)$$

The linear operators $\varpi_f = \frac{\partial^3 f}{\partial \eta^3}$ and $\varpi_\theta = \frac{\partial^2 \theta}{\partial \eta^2}$, are represented in the expanding form as

$$\varpi_f(\omega_1 + \omega_2\eta + \omega_3\eta^2) = 0, \varpi_\theta(\omega_4 + \omega_5\eta) = 0, \quad (13)$$

By Taylor's expansion, we have

$$f(\eta; \rho) = f_0(\eta) + \sum_{x=1}^{\infty} \rho^x f_x(\eta), \quad (14)$$

$$\theta(\eta; \rho) = \theta_0(\eta) + \sum_{x=1}^{\infty} \rho^x \theta_x(\eta), \quad (15)$$

now

$$f_x(\eta) = \frac{1}{x} \cdot \left. \frac{df(\eta; \rho)}{d\rho} \right|_{\rho=0}, \theta_x(\eta) = \frac{1}{x} \cdot \left. \frac{d\theta(\eta; \rho)}{d\rho} \right|_{\rho=0}. \quad (16)$$

The scheme of equation can be expressed as

$$\begin{aligned} L_f [f_x(\eta) - N_x f_{x-1}(\eta)] &= \pi_f R_x^f(\eta), \\ L_\theta [\theta_x(\eta) - N_x \theta_{x-1}(\eta)] &= \pi_\theta R_x^\theta(\eta). \end{aligned} \quad (17)$$

Where $N_x = 0$ if $\rho \leq 1$ and if $\rho > 1$.

4. Validation of the results

The mathematical outcomes of the present investigation using Tiwari et al. [53] and Das et al. [7] are used to approve the approach and the computational procedure. Table 3 shows a comparative analysis of the numerical results with prior publications using the following parameters: nanoparticle volume fraction ($\phi_1 = \phi_2 = 0$), suction/injection ($w = 0$), Prandtl number ($Pr = 1.0$), and magnetic ($M = 0$) for numerous thin-film thicknesses λ , each of which is exposed to a various values of S . The value of local skin friction $f''(0)$ and $-\theta'(0)$, as shown in the table, is in remarkable agreement with earlier research. As a result, the code confirmation is acceptable. It also grows as λ and Pr are increasing.

Table 3 Assessment of $f''(0)$ and $-\theta'(0)$ taking $\phi_1 = \phi_2 = w = M = 0$ for numerous values of λ and Pr , respectively.

λ	$f''(0)$			Pr	$-\theta'(0)$		
	Das et al. [7]	Tiwari and Das [53]	Present		Das et al. [7]	Tiwari and Das [53]	Present
1.2	-2.1128	-2.1127	-2.11268	1.0	-0.02	-0.02	-0.02
1.6	-1.3803	-1.3802	-1.3801	2.2	-0.192061	-0.192002	-0.192062
2.2	-0.958562	-0.958560	-0.958561	2.6	-0.409006	-0.409004	-0.409003
2.6	-0.736267	-0.736265	-0.736266	3.0	-0.603009	-0.603010	-0.603008
3.5	-0.632871	-0.632870	-0.632873	4.5	-0.742955	-0.742950	-0.742951

4.2 Numerical results

To solve the Eqs. (8) -(10) analytically, the boundary value problem solver 'HAM', which means the homotopy analysis method, is used. To support this research, 0.1 solid volume fraction of Al_2O_3 (i.e. $\phi_1 = 0.1$) is included in the base fluid as recommended by Devi [7]. To create a Cu- Al_2O_3 water/ethylene glycol hybrid nanofluid, various solid volume fractions of Cu with 30% ethylene glycol were added to the mixture. We will use the Prandtl number, $Pr = 6.2$, which depicts water as the conventional fluid, as described by Oztop and Abu-Nada [54], and it will be maintained to achieve seminumerical results.

When a thin-film is stretched, the hybrid nanofluid movement and heat conduction behaviour is separated into two cases: suction($w > 0$) and injection($w < 0$) fluid through a transparent porosity sheet. Analytical solutions are derived for a variety of physical model parameters to describe the physical problems in the form of the flow pattern linked to velocity, temperature, local skin friction, and moderated Nusselt number coefficient in greater detail.

In all situations ($w < 0$ or $w > 0$), the fluid velocity decomposes as the M parameter is enhanced, as shown in Figure 2. The increase in M causes the stunting force uptick in the hybrid nanofluid to boost, resulting in less movement of the hybrid nanoparticles and a thinner momentum boundary layer thickness. As variable M increases, the heat transfer in Figure 3 shows the reverse pattern. Both Devi and Devi [7] and Upreti et al. [55] documented a striking similarity for both features. When M increases, the magnetic field in the liquid increases, meaning a significant Lorentz force, which causes friction in the hybrid nanofluid. It is shown in the figure that the thermal

boundary layer thickens as friction builds up under the influence of magnetism. Furthermore, the injection impacts preserve the magnetic hybrid nanofluid's lowest velocity profile and maximum heat flux more than the suction consequences. Pal [56] showed a similar pattern in the temperature gradient for suction and injection flow of fluids.

Figures 4 and 5 show the effects of parameter S on the velocity and temperature profiles for both suction and injection instances. It may be deduced that when S increases, the velocity and temperature profiles decrease. Literally, the force to flow the material in the thin-film is reduced as the rate of the original sheet extending from constricted failures increases due to the expansion of the unsteadiness parameter. This situation slows the motion of the substances and prevents the particles from absorbing heat. When S is enhanced, the thickness of the momentum and thermal boundary layers is also decreased. The velocity and temperature curves of the hybrid nanofluid under suction are smaller compared to the injection scenario, as anticipated. In the suction situation, a larger amplitude of S is believed to result in more thinning of both boundary layer thicknesses than in the injection case.

Figure 6 depicts the variation in the volume fraction of nanomaterials in relation to the velocity field of the electromagnetic hybrid nanofluid. When the volume fraction of copper nanoparticles is increased from 0.005 to 0.06, the flow rate of the hybrid nanostructured materials decreases. Furthermore, the thickness of the momentum boundary layer is reduced, slowing fluid movement. This is because when the fluid is enriched with nanomaterials, the viscosity of the fluid increases. The particles in the thin-film accelerate faster under the influence of injection amplitude than under the influence of suction. Figure 7 depicts the relationship between ϕ_2 and the altered temperature profiles. As various studies have demonstrated in the literature, increasing the parameter ϕ_2 , increases the fluid's thermal conductivity.

As a result, the temperature of the electromagnetic hybrid nanofluid rises, increasing the thickness of the thin-film flow thermal boundary layer. It is also worth noting that the temperature and thickness of the thermal boundary layer in the injection scenario are higher than those in the suction situation. The analytical conclusion of Das et al. [7] for the suction/injection of hydromagnetic nanofluids was well supported by the results of our study on velocity and temperature variations.

Figure 8 depicts the changing tendency of the hybrid nanofluid velocity according to thin-film thickness λ . A thicker thin film thickness is indicated by increasing the dimensionless parameter λ . Because the atoms in hybrid nanoparticles move slowly, the momentum barrier layer becomes thinner, resulting in a decrease in the fluid velocity field. The motion in an injection fluid is greater than that in a suction fluid, and the thickness of the momentum barrier layer is also higher.

The ambient temperature of the electromagnetic hybrid nanofluid is reduced by the thin-film thickness, as shown in Figure 9. It is clear that thicker thin-film thickness permits reduced thermal resistance from the surface sheet into the surrounding fluid, lowering the thickness of the thermal boundary layer. Figure 9 shows that the electromagnetic hybrid nanofluid in the suction situation has a cooling effect compared to the electromagnetic hybrid nanofluid in the injection scenario.

Figures 10 and 11 demonstrate the effect of the velocity and temperature field on the mass transfer parameter, and the suction/injection parameter. By adopting the injection severity, hybrid nanofluid materials are added to the thin-film, shrinking the velocity and temperature characteristics. Furthermore, identical results are produced when the hybrid nanofluid particles are removed from the thin film via suction

effects through a permeable stretching surface. The figures show that as the parameter w is increased, the momentum and thermal boundary layer thickness of the fluid decreases. As seen in Figures 10 and 11, the suction of the solvent leads to reduction in motion, and the heat capacity in the particulate matter is higher than that under the injection fluid.

Figure 2 Velocity field by M .

Figure 3 Temperature field by M .

Figure 4 Velocity field by S .

Figure 5 Temperature field by S .

Figure 6 Velocity field by ϕ_2 .

Figure 7 Temperature field by ϕ_2 .

Figure 8 Velocity field by λ .

Figure 9 Temperature field by λ .

Figure 10 Velocity field by w .

Figure 11 Temperature field by w .

The inspirations of the innumerable values of the governing constraints M, S, ϕ_2 and λ on $C_f \text{Re}_x^{\frac{1}{2}}$ and $Nu_x \text{Re}_x^{-\frac{1}{2}}$ are mapped in Table 4. An addition in the values of magnetic parameter M unveils a slumping effect on $C_f \text{Re}_x^{\frac{1}{2}}$ an equivalent behaviour in $Nu_x \text{Re}_x^{-\frac{1}{2}}$. Sandeep et al. [57] also noticed this characteristic, who considered an unsteady MHD nanofluid flow embedded with nanoparticles in a thin-film. The increase in the unsteadiness parameter S and λ curtail the local skin friction, thereby decreasing the magnitude of the wall shear stress. However, the heat transfer rate and the Nusselt number showed greater rates for higher parameters S and λ respectively. Thus, due to the Nusselt number escalation, the convective heat transfer constantly increased. Furthermore, the wall shear stress and the heat transmission rate slightly decline with the growth of ϕ_2 for the magnetic hybrid nanofluid. Similarly, the impact of the parameter w is tabulated in Table 5, and the

values of $C_f \text{Re}_x^{\frac{1}{2}}$ is decrease when the volume fraction is improved, but the opposite tendency is observed for $Nu_x \text{Re}_x^{-\frac{1}{2}}$.

Table 4. Impact of M, S, ϕ_2 and λ on $C_f \text{Re}_x^{\frac{1}{2}}$ and $Nu_x \text{Re}_x^{-\frac{1}{2}}$ for $w > 0$ and $w < 0$.

M	S	ϕ_2	λ	$C_f \text{Re}_x^{\frac{1}{2}}$		$Nu_x \text{Re}_x^{-\frac{1}{2}}$	
				Suction, $w > 0$	Injection, $w < 0$	Suction, $w > 0$	Injection, $w < 0$
0.1				-11.2485	-5.6177	15.8105	6.7508
0.3				-12.2670	-6.67678	15.6806	6.7143
0.7				-13.1728	-7.6204	15.6657	6.5192
1.2				-14.0080	-8.5810	15.5343	6.5082
	2.0			-13.4764	-5.1252	13.5266	6.7409
	2.5			-13.5920	-5.3760	13.8330	6.9367
	3.0			-13.4259	-5.5617	16.1327	9.6927
	3.5			-13.5371	-5.8854	16.4234	9.8276
		0.002		-7.6341	-3.9383	8.4734	5.9109
		0.08		-8.4530	-5.2385	11.3465	5.5362
		0.04		-8.8952	-5.7368	9.8790	5.3276
		0.07		-9.4667	-6.8438	9.1321	5.1383
			0.5	-6.4526	-4.3754	7.4147	5.9965
			1.0	-7.3830	-6.8525	9.5656	8.6579
			1.8	-10.0144	-7.0254	12.6749	9.8136
			2.4	-11.1552	-7.8153	12.7384	10.7398

Table 5. Impact of w on $C_f \text{Re}_x^{\frac{1}{2}}$ and $Nu_x \text{Re}_x^{-\frac{1}{2}}$.

w	$C_f \text{Re}_x^{\frac{1}{2}}$	$Nu_x \text{Re}_x^{-\frac{1}{2}}$
-0.2	-4.32743	5.20142
-0.1	-5.87231	6.55920
0.0	-8.10927	10.2045
1.2	-10.4563	12.5474
2.0	-15.00917	17.1348

4. CONCLUSION

The flow and heat transport of a magnetic hybrid nanofluid via a transparent stretchable surface under initial and boundary conditions were investigated in this article by taking ethylene glycol as a base fluid. Suction/injection has a significant effect on boundary layer flow and heat transfer in the magnetohydrodynamic thin-film hybrid nanofluid, according to the quantitative simulation. When the values of parameters M and ϕ_2 were increased, the velocity and temperature fields exhibited the opposite behaviour. As the dimensionless parameters S , λ and w increase, the molecule movement decreases and the viscous hybrid nanofluid cools down. Due to the overshoot of the metrics M and ϕ_2 , the physical quantities $C_f Re_x^{\frac{1}{2}}$ and $Nu_x Re_x^{-\frac{1}{2}}$ decreased. The Nusselt number of the magnetic hybrid nanofluid shows a truncation and retrograde tendency as S , λ and w increase.

CONFLICT OF INTEREST

The authors declare no conflicts of interest.

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